



CAPITAL

CANADA'S WINE

Town of Oliver



February 2023

Project No. 306-088-010

ENGINEERING ■ PLANNING ■ URBAN DESIGN ■ LAND SURVEYING

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Revision Log

Revision #	Revised by	Date	Issue / Revision Description

Report Submission

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List of Acronyms

BOD₅ cBOD₅ CPE GIS HDPE LS LWMP masl MOE MOE MSR MW MWR OC OCP PVC RIB TRUE TSS WMP WWAL WWTP	5-Day Biochemical Oxygen Demand 5-Day Carbonaceous Biochemical Oxygen Demand Chlorinated Polyethylene Geographic Information Systems High Density Polyethylene Lift Station Liquid Waste Management Plan meters above sea level Ministry of Environment Ministry of Environ and Climate Change Strategy Municipal Sewage Regulation Monitoring Well Municipal Wastewater Regulation Operational Certificate Official Community Plan Polyvinyl Chloride Rapid Infiltration Basin TRUE Consulting Total Suspended Solids Waste Management Plan Western Water Associates Ltd. Waste Water Treatment Plant
VV VV I P	waste water Treatment Plant

Units of Measure

km	kilometre
L/d	Litres per day
L/m	Litres per minute
L/s	Litres per second
lpcd	Litres per capita per day
m	metre
m³/day	cubic metre per day
mg/L	milligrams per Litre
mm	millimetre

1.0 Operational Data

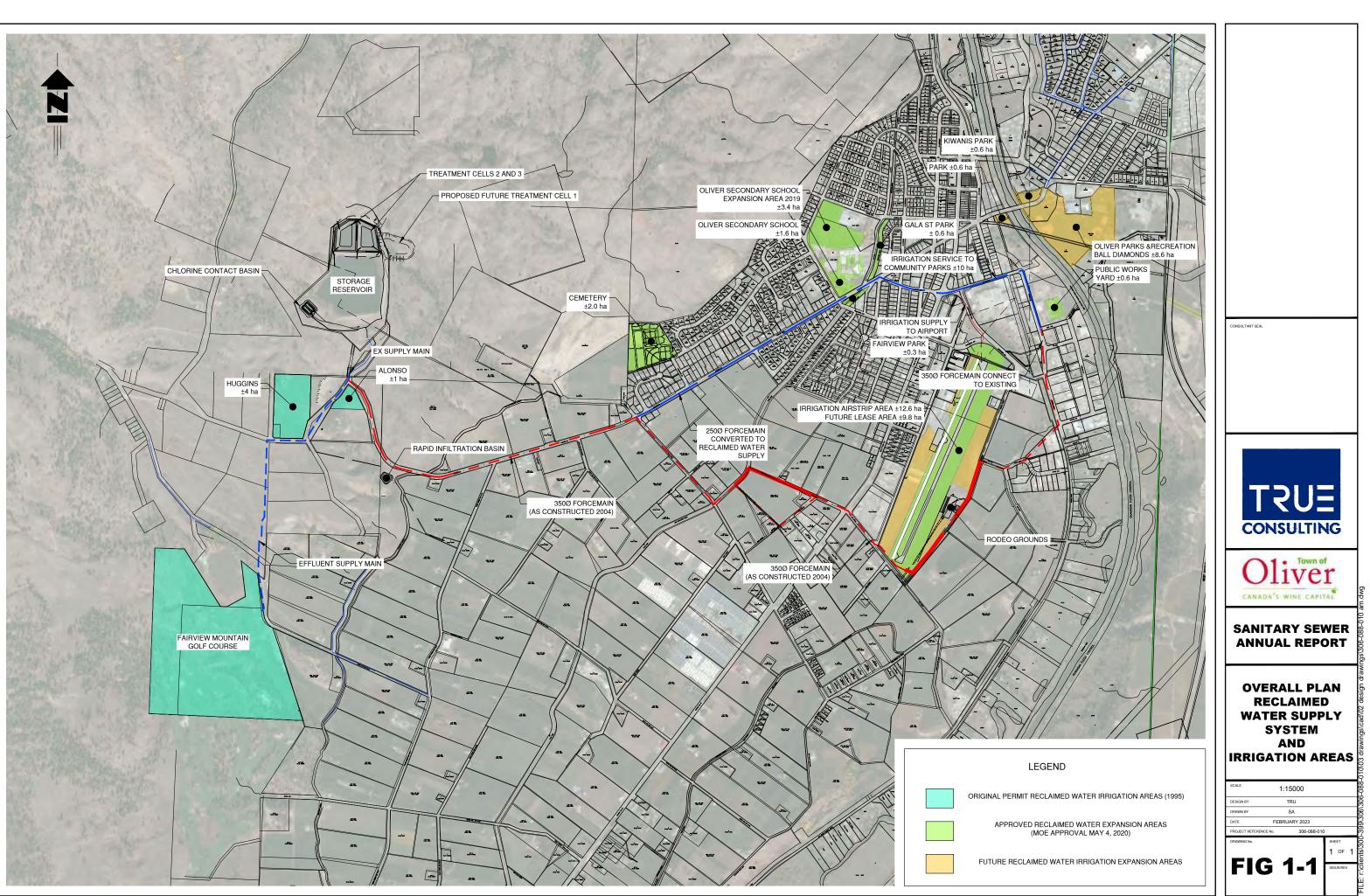
The following report summarizes the operational data for the Town of Oliver's Sanitary Sewer System for 2022. The report is formatted from collection to disposal. Appendix A contains a copy of the Operational Certificate (OC) for the system (PE 13717) issued by the Ministry of Environment (MOE) on December 14, 1995. When required, appropriate references will be made to the OC.

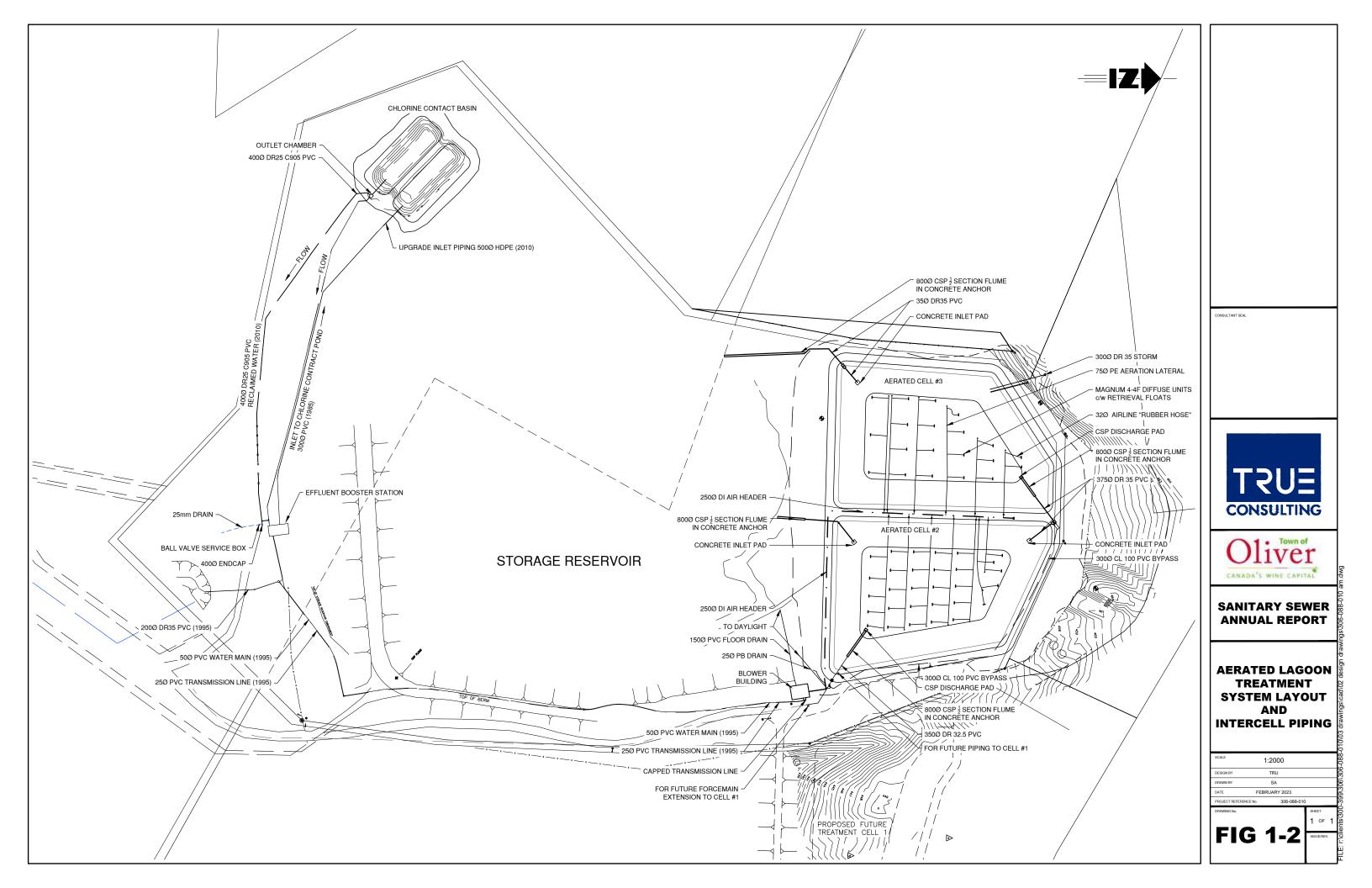
Section 1 of the OC outlines the specific authorized discharge requirements from the Town of Oliver's Wastewater Treatment Plant (WWTP) and are summarized as follows:

- The Town is authorized to discharge a maximum of 2,200m³ per day from the aerated lagoons to the reclaimed wastewater storage reservoir, averaged on a daily basis.
- There is no maximum authorized discharge rate from the storage reservoir for beneficial use as irrigation water.
- The effluent discharged from the aerated lagoons to the storage reservoir must not exceed a 5-Day Biochemical Oxygen Demand (BOD₅) of 45 mg/L, and a Total Suspended Solids (TSS) of 60 mg/L.
 - As per the BC Municipal Wastewater Regulations (MWR), BOD₅ is described as the 5-Day Carbonaceous Biochemical Oxygen Demand (cBOD₅).
- A minimum reclaimed wastewater reservoir retention time of 60 days must be met prior to discharge of the reclaimed wastewater.
- Reclaimed wastewater utilized for irrigation shall conform to the effluent irrigation guidelines developed by the BC Ministry of Health. Fecal Coliforms shall not exceed 200 MPN per 100 mL for agricultural, silvicultural, and low public use lands, and shall not exceed 2.2 MPN per 100 mL for high public use land.

To assist the reader in assessing the system operational data, the following drawings are included:

- Figure 1-1: Overall Plan Reclaimed Water Supply System and Irrigation Areas
- Figure 1-2: Aerated Lagoon Treatment System





1.1 Influent

1.1.1 Influent Works (OC 6.4.2)

Influent from the sanitary sewer collection system is pumped through influent screens and piped into a two-cell flow equalization system ("equalization basins") located at the Town's Public Works Yard at 5971 Sawmill Road. The original equalization basin was constructed in 1984 and lined with a Chlorinated Polyethylene (CPE) membrane. The second equalization basin was constructed in 2009 and lined with a 60-mil high density polyethylene (HDPE) geomembrane. These liners provide a transfer barrier for liquids from the basins to the native subsurface material. There is no piped interconnection between the Okanagan River and the equalization basins.

A detailed description of the collection system and treatment process can be found in the Town of Oliver's 2018 Sanitary Capital Plan prepared by TRUE Consulting (Appendix B). This Capital Plan includes an update to the Liquid Waste Management Plan (LWMP). Further details can be found in the Oliver WWTP Operation and Maintenance Manual prepared by TRUE Consulting in February 2021.

1.1.2 Influent Flow Data (OC 7.1.2 and 7.2.4.7)

Wastewater is pumped from the equalization basin to the aerated lagoons via the High Lift station. 2022 daily flow data for the High Lift station is presented in Appendix C. The total volume pumped to the aerated lagoons in 2022 was 622,711 m³, which equates to an average daily flow of 1,706 m³/day. This is an increase of 14,980 m³ (2.3%) as compared to 2021. A summary of total influent inflows from the period 1996 to 2022 can be seen in Table 1-1 and Figure 1-3, below.



Year	Total Influent Volume (m ³)	Average Daily Flow (m ³ /d)
1996	654,361	1,788
1997	682,480	1,870
1998	666,322	1,826
1999	688,193	1,885
2000	702,688	1,920
2001	678,052	1,858
2002	726,354	1,990
2003	751,139	2,058
2004	766,048	2,093
2005	783,947	2,148
2006	829,413	2,272
2007	823,011	2,255
2008	777,154	2,123
2009	758,308	2,078
2010	701,475	1,922
2011	693,045	1,899
2012	658,002	1,798
2013	697,377	1,911
2014	634,649	1,739
2015	679,542	1,862
2016	639,794	1,753
2017	689,098	1,888
2018	666,376	1,826
2019	625,911	1,715
2020	655,853	1,792
2021	607,731	1,665
2022	622,711	1,706

TABLE 1-1: ANNUAL TOTAL AND AVERAGE DAILY INFLUENT FLOW DATA



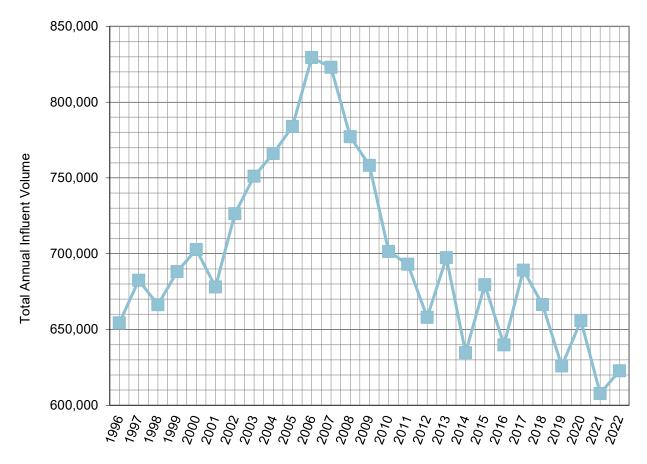


FIGURE 1-3: TOTAL ANNUAL INFLUENT SEWAGE FLOWS FOR 1996 AND 2022

1.1.3 Influent Wastewater Sampling (OC 6.1 and 7.1.2)

Influent sampling data for total phosphorus and orthophosphate concentrations are presented in Table 1-2. The average total phosphorous and orthophosphate concentrations from March and September 2022 sampling were 6.88 and 1.69 mg/L respectively. Notably, total phosphorous was not sampled during the September sampling event. This is not compliant with the OC requirements which require semi-annual sampling of total phosphorus.

The 2022 average concentrations are consistent with previous years.



Year	Date	Total Phosphorus (mg/L)	Ortho Phosphate (mg/L)
	Mar. 22	5.44	
1996	Sep. 12	5.18	
1997	Mar. 19	5.87	
	Mar. 18	5.6	
1998	Sep. 9	5.89	
	Mar. 11	6.66	
1999	Sep. 23	4.89	
2000	Mar. 23	6.48	4.69
2000	Sep. 28	8.67	3.04
2001	Mar. 22	4.57	2.3
2001	Sep. 19	4.13	1.88
2002	Mar. 19	4.53	3.84
2002	Sep. 10	4.52	2.55
	Mar. 10	3.78	3.78
2003	Sep. 30	4.48	4.38
	Mar. 16	5.23	4.76
2004	Sep. 14	5.15	3.75
	Mar. 22	5.24	4.63
2005	Oct. 5	6.74	5.58
2006	Sep. 14	7.05	5.96
	Mar. 13	5.03	6.43*
2007	Sep. 11	6.03	5.03
2008	Sep. 3	7.44	3.3
	Mar. 5	8.18	3.84
2009	Sep. 1	5.31	1.38
	Mar. 9	4.26	0.558
2010	Sep. 2	3.36	2.16
	Mar. 8	4.9	0.316
2011	Sep. 8	11.00	0.859
	Mar. 1	6.16	2.23
2012	Sep. 11	7.76	3.72
	Mar. 7	5.75	2.57
2013	Sep. 11	4.62	1.89
	Mar. 5	4.02	0.82
2014	Sep. 17	3.82	not tested
	Mar. 11	5.36	2.66
2015	Sep. 16	4.55	2.96
	Mar. 7	4.17	1.21
2016	Sep. 6	2.35	0.36*
	Mar. 7	3.77	2.42
2017	Sep. 6	4.69	2.42
	Mar. 7	5.37	1.95
2018	Sep. 4	5.89	1.95
2019	Mar. 11	5.34 5.42	1.97
	Sep. 3		2.32
2020	Mar. 2	4.97	1.89
	Sep. 1	5.45	2.09
2021	Mar. 15	6.76	1.7
	Sep.14	5.59	2.28
2022	Mar. 1	6.88	2.12
	Sept 6.	Not Tested	1.26
Average for	Period of Record	5.49	2.70

TABLE 1-2: INFLUENT SAMPLING ANALYSIS

1.2 Wastewater Treatment (OC 6.2 and 7.1.2)

Effluent sampling results from the aerated lagoon system (Cell No. 3) prior to discharging to the storage reservoir are tabulated in Table 1-3. All TSS and cBOD₅ values were compliant with regulatory criteria for all sampling events.

Date	CBOD₅ (mg/L)	TSS (mg/L)
OC Limits	45	60
Jan-10 (2022)	17.4	12.8
Feb-01 (2022)	17.4	8.7
Mar-01 (2022)	14.5	16.1
Apr-04 (2022)	18.5	18.4
May-02 (2022)	8.0	5.3
Jun-07 (2022)	<7.1	23.7
Jul-04 (2022)	<8.4	10.0
Aug-02 (2022)	7.7	16.0
Sep-06 (2022)	<7.0	13.0
Oct-03 (2022)	<6.2	<4.0
Nov-09 (2022)	10.0	14.7
Dec-5 (2022)	15.3	11.3

TABLE 1-3: CELL NO.3 - EFFLUENT BOD ₅ , CBOD ₅ AND 1	ISS

Historical data trends for BOD_5 and TSS are shown in Figure 1-4 below. Values for $cBOD_5$ have been included in lieu of BOD_5 for 2021-2022.

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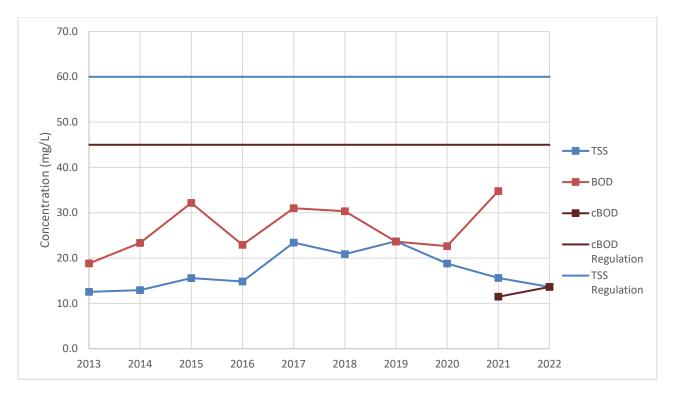


FIGURE 1-4: YEARLY AVERAGE TSS, BOD5, AND CBOD5 VALUES

As seen above, the 2022 yearly average $cBOD_5$ and TSS data values for reclaimed water are compliant with the regulatory criteria. The 2022 TSS data is consistent with historic trends. Comparing 2021-2022 $cBOD_5$ data to historic BOD_5 , shows that $cBOD_5$ concentrations are lower than historic BOD_5 .

As per PE-13717, semi-annual analysis of effluent must include:

- Total phosphorous, ortho-phosphorous, and total dissolved phosphorus (all expressed in mg/L P)
- Total nitrogen, ammonia nitrogen, nitrate, nitrite, nitrogen, and organic nitrogen (all expressed as mg/L N)

A summary of semi-annual sampling for total nitrogen, ammonia, and nitrate from 1997 – 2022 is presented in Table 1-4. The complete suite of semi-annual sampling and compliance testing requirements are included in Appendix C. It is noted that the September sampling event did not test the following parameters:

- Phosphate as P,
- Organic nitrogen as N,
- Ammonia as N and,
- Total Phosphorus.

Exclusion of these test results is not compliant with the OC criteria.



Sampling events were conducted on March 1st and September 6th, 2022. The accepted range for total nitrogen in domestic wastewater is 20 to 50 mg/L. Total nitrogen was within this range for both sampling events.

	Se	ptember/Octo	ber	March		
Year	Total Nitrogen (mg/L)	Ammonia (mg/L)	Nitrate (mg/L)	Total Nitrogen (mg/L)	Ammonia (mg/L)	Nitrate (mg/L)
1997	9.34	0.006	7.7	20.7	No Data	No Data
1998	10.8	0.005	8.89	25.1	No Data	No Data
1999	11.3	0.46	8.31	23.9	No Data	No Data
2000	No Data	0.48	9.77	29.1	No Data	No Data
2001	34.3	4.37	7.92	31.3	No Data	No Data
2002	17.7	0.013	16.3	23.6	No Data	No Data
2003	No Data	0.71	3.9	26.9	No Data	No Data
2004	9.8	8.46	0.29	17.2	No Data	No Data
2005	26.4	14.2	No Data	36.4	No Data	No Data
2006	12.1	0.78	5.97	No Data	No Data	No Data
2007	20	13.2	0.92	25.7	No Data	No Data
2008	10	9.55	0.297	24.1	No Data	No Data
2009	17	14	1	No Data	No Data	No Data
2010	16.3	8.44	3.6	27.8	No Data	No Data
2011	26	13.7	3.27	33.5	No Data	No Data
2012	5.28	1.95	2.17	32.2	No Data	No Data
2013	10.10	0.289	9.43	43.7	32.5	0.489
2014	No Data	No Data	No Data	32.8	31.2	0.046
2015	19.10	17.6	0.966	No Data	No Data	No Data
2016	12.80	1.82	5.33	33.2	31.2	1.05
2017	18.50	0.384	14.7	32	23.4	0.019
2018	11.9	0.916	8.2	32	31.1	0.282
2019	18.5	0.322	10.1	27.4	27.6	0.339
2020	21.9	15.6	2.36	35.3	25.2	1.2
2021	17.4	12.6	2.11	24.5	26	0.428
2022	5.92	No Data	4.31	33.3	30.6	0.266

TABLE 1-4: CELL NO.3 EFFLUENT - NITROGEN



From 1997 to 2002, a significant proportion of ammonia nitrogen was nitrified through the Town's aerated lagoon system. From 2003 to 2015, the Town accepted wastewater influent from Vincor (a local winemaker), which resulted in modest levels of nitrification. In January 2012, Vincor implemented a pre-treatment system, resulting in approximately a 90% reduction in BOD. This resulted in reduced loadings which in turn resulted in increased nitrification. As of July 1, 2015, Vincor has been disconnected from the Town's wastewater system.

1.3 Winter Effluent Storage Reservoir

Weekly storage reservoir level data for 2022 is presented in Appendix D. All elevations given are relative to geodetic datum. The elevation data has been converted to total volume in storage above the minimum 60-day storage level. The storage calibration curve is also included in Appendix D.

As per Section 1.1.1 of the OC, the Town is authorized to a maximum effluent discharge rate of 2,200 m³ per day from the aerated lagoon sewage treatment system to the reclaimed wastewater storage reservoir, averaged on a monthly basis. To measure this flow rate, it is assumed that the flow rate between the aerated lagoon to the storage reservoir is equal to the flow rate at the High Lift station (which pumps wastewater from the equalization basin to the aerated lagoons). This assumption is conservative because it does not account for water losses caused by evaporation and seepage. Monthly volumes are presented in Table 1-5 as follows:

	Monthly m ³	Average m³/day
January	49,176	1,586
February	39,874	1,424
March	48,657	1,570
April	50,131	1,671
Мау	51,057	1,647
June	59,316	1,977
July	66,102	2,132
August	56,953	1,837
September	52,295	1,743
October	49,800	1,606
November	47,773	1,592
December	51,577	1,664
Total	622,711	
Average		1,706

TABLE 1-5: 2022 MONTHLY EFFLUENT DISCHARGE QUANTITIES



As shown in Table 1-5, the discharge values were compliant with the regulatory criteria. Annual operating data for the storage reservoir is summarized in Table 1-6. This includes a comparative summary from 2012 to 2022.

Year		Date	Elevation (m)	Volume (m ³)
	Max.	2-May-12	445.36	338,000
2012	Min.	10-Oct-12	440.99	72,000
	End	31-Dec-12	443.46	211,000
	Max.	25-Apr-13	445.52	355,000
2013	Min.	21-Aug-13	441.67	106,000
	End	31-Dec-13	444.56	284,000
	Max.	31-Mar-14	446.06	374,000
2014	Min.	15-Sep-14	441.39	92,000
	End	29-Dec-14	443.65	223,000
	Max.	7-Apr-15	445.62	351,000
2015	Min.	7-Oct-15	441.52	101,000
	End	4-Jan-16	443.5	214,000
	Max.	4-Apr-16	445.47	343,000
2016	Min.	19-Sep-16	441.60	105,000
	End	19-Dec-16	444.02	247,000
	Max.	22-May-17	446.17	379,000
2017	Min.	16-Oct-17	442.75	167,000
	End	18-Dec-17	444.43	275,000
	Max.	2-Apr-18	446.41	391,000
2018	Min.	10-Sep-18	443.17	193,000
	End	24-Dec-18	444.63	289,000
	Max.	8-Apr-19	446.43	397,000
2019	Min.	9-Sep-19	441.91	119,000
	End	23-Dec-19	443.98	245,000
	Max.	23-Mar-20	446	370,000
2020	Min.	14-Sep-20	441.55	102,000
	End	28-Dec-20	444.01	246,000
	Max.	22-Mar-21	445.8	360,000
2021	Min.	7-Sep-21	441.6	105,000
	End	20-Dec-21	443.6	221,000
	Max.	4-Apr-22	445.76	358,000
2022	Min.	, 17-Oct-22	442.3	136,000
	End	28-Dec-22	444.05	249,000
1				,

TABLE 1-6: EFFLUENT STORAGE RESERVOIR LEVEL DATA



Winter effluent storage reservoir year-end, maximum, and minimum operating elevations for the period 2008 to 2022 are illustrated graphically in Figure 1-5. Referring to this figure:

- The maximum elevation in 2022 (445.76 masl on April 4th, 2022) is 0.04 metres below the maximum level in 2021.
- The 2022 year-end storage of 249,000 m³ is 28,000 m³ more than the available storage at the end of 2021.

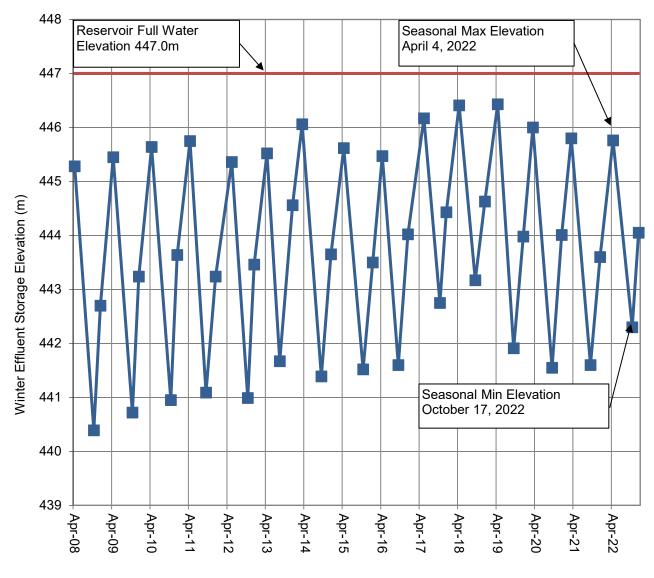


FIGURE 1-5: EFFLUENT STORAGE RESERVOIR LEVELS - 2008 TO 2022



1.4 Reclaimed Water Quantities and Quality

1.4.1 Irrigation Plan (OC 1.8)

The Town of Oliver currently provides reclaimed water to the Fairview Mountain Golf Course, Alonso Property, Higgins Property, Fairview Park, Oliver Secondary School, Public Works, the Airstrip, and Cemetery for irrigation purposes. This area has expanded since that outlined in Site Plan A of the OC.

On December 13, 2018, the Town submitted an irrigation area expansion notification to the Ministry. An updated plan was submitted to the Ministry on February 25, 2020, to include expansion to the South Okanagan Secondary School irrigation system. These expansion areas were authorized by the Director on May 24, 2020, in accordance with Clause 1.8 of OC 13717 (see Appendix E)

1.4.2 Irrigation Volumes (OC 7.2.4.2 and 6.4)

Total reclaimed water usage is measured by a flow meter in the booster station located adjacent to the reclaimed water storage reservoir. Meters are also located at the Cemetery, Gala Street Linear Park, Fairview Park, the Airport, Public Works Yard, Alonso property, Southern Okanagan Secondary School, and Huggins Property for the purposes of measuring total reclaimed water use at each location. The consumption at the Fairview Mt. Golf Course is not metered and it is calculated as total usage less all meter locations. Table 1-7 and Table 1-8 summarize the system consumption totals.



Location	2013	2014	2015	2016	2017	2018	2019	2020	2021	2022
Fairview Mt. Golf Course	248,52	316,36	346,52	322,04	311,89	281,18	329,22		356,41	352,234
Fairview Park	1	8	0	8	9	6	6	418,594 *	6	193**
Airport	185,68 7	124,89 2	115,74 3	98,511	101,78 0	99,601	69,143		32,276	28,254
Cemetery	19,160	15,996	14,354	14,843	13,400	12,651	16,986	17,499	18,291	18,336
Gala Street Linear Park	8,051	8,749	7,647	8,360	1,030*	5,928	8,858	1,245	11,676	7,896
Public Works Yard	7,086	7,393	7,380	8,095	8,341	6,261	5,940	8,320	5,388	6,103
Alonso	6,715	3,893	3,851	2,364	2,498	1,794	9,240	6,012	0	0
Huggins	1,290	0	8,554	0	0	0	4,614	0	0	0
Southern Okanagan Secondary School	0	4,874	0	0	2	0	25,744	27,420	24,694	18,545***
Infiltration Basin	0	0	0	0	23,322	38,391	16,858	11,117	2,256	3,752
Total Use	476,51 0	482,16 4	504,04 9	454,22 1	461,24 1	445,81 2	486,61 0	490,207	450,99 7	435,314

TABLE 1-7: ANNUAL RECLAIMED WATER USE BY CUSTOMER

* The Airport flow meter was not working from May to September therefore the totals were grouped.

** Fairview Park flows were partitioned based on flow meter readings.

*** In 2022, the school did not turn on the reclaimed water meter until July. Prior to this, domestic water was used for irrigation.

From flow data contained in Appendix D, reclaimed water quantities for each "user" is described as follows:

Lot 723, Plan 2361 - Fairview Mountain Golf Course

Total Usage Crop Type Irrigated Area Irrigation Application Rate Irrigation Period

Lot A, Plan 24065 - Oliver Cemetery

Total Usage Crop Type Irrigated Area Irrigation Application Rate Irrigation Period 352,234 m³ Turf and rough areas 57.6 ha 0.61 m April to October

18,336 m³ Lawn, trees & shrubs 2.3 ha 0.80 m April to October



Gala Street Linear Park

Total Usage Crop Type Irrigated Area Irrigation Application Rate Irrigation Period

Fairview Park

Total Usage Crop Type Irrigated Area Irrigation Application Rate Irrigation Period 5,898 m³ Lawn & trees 0.6 ha 1.44 m April and October

2,883 m³ Lawn & trees 0.3 ha 0.19 m April and October

Lot A, Plan 38173 – Oliver Airport

Total Usage Crop Type Irrigated Area Irrigation Application Rate Irrigation Period

28,254 m³ Forage Crops 12.6 ha 0.22 m June to September

Records were only completed between June and September.

Lot A, Plan 33094 – Oliver Public Works Yard

Total Usage	6,103 m ³
Crop Type	Lawn, landscaping, compost piles
Irrigated Area	0.6 ha
Irrigation Application Rate	N/A
Irrigation Period	April to October

The principal use of reclaimed water at the Public Works Yard is for composting operations, lawn care and landscaping. Because composting use is not separately metered, application rates for the lawn and landscaping areas cannot be calculated independently.

Lot A, Plan 37929 – Alonso (former Moir)

Total Usage Crop Type Irrigated Area Irrigation Application Rate Irrigation Period 0 m³ Vineyard approximately 1.0 ha 0 m April to October



Lot 3, Plan 5881 – Huggins

Total Usage Crop Type Irrigated Area Irrigation Application Rate Irrigation Period 0 m³ Vineyard approximately 3.7 ha 0 m April to October

South Okanagan Secondary School

Total Usage	18,545 m ³
Crop Type	Lawn and Trees
Irrigated Area	approximately 5.4 ha
Irrigation Application Rate	0.34 m
Irrigation Period	April to October

Over the years of record, reclaimed water use on the Fairview Mountain Golf Course has varied significantly on a year-to-year basis. Table 1-8 has been prepared adding seasonal precipitation to reclaimed water usage to derive an annual total. A summary of seasonal precipitation from 1992 to 2022 can be found in Appendix F. The tabulation shows that the sum of seasonal precipitation and reclaimed water use for 2022 is 0.76 m applied. This is consistent with historical usage.

Year	Total Usage (m³)	Application Rate (m)	Seasonal Precipitation (mm)	Total (m)
2012	297,875	0.66	223	0.88
2013	248,521	0.55	180	0.73
2014	316,367	0.70	175	0.88
2015	346,520	0.77	136	0.91
2016	332,048	0.74	166	0.90
2017	311,899	0.69	133	0.83
2018	281,186	0.62	210	0.83
2019	329,226	0.73	127	0.86
2020	418,594	0.73	186	0.92
2021	356,416	0.62	67.9	0.69
2022	362,234	0.63	127.5	0.76

TABLE 1-8: 10-YEAR ANNUAL TOTAL APPLICATION RATE AT THE FAIRVIEW MOUNTAIN GOLF Course

1.4.3 Rapid Infiltration

The Town infiltrates reclaimed water to the rapid infiltration basins located south of the wastewater treatment facility (see Figure 1-1). This allows the Town to lower the water level of the storage reservoirs when needed. In 2022, the Town discharged 3,752 m³ to the rapid infiltration basins.



Similar to 2021, the Town discharged minimal flows to the rapid infiltration basins as 2022 was a dry year. These flows were conveyed simply to flush the system, not to prevent reservoir overflow.

1.4.4 Hydraulic Balance (OC 7.2.4.1)

The annual overall storage reservoir hydraulic balance (January 1st to December 31st) for the period 2009 to 2022 is summarized in Table 1-9.



	2009	2010	2011	2012	2013	2014	2015
Volume in Storage on Jan. 1	167,000	200,000	223,000	197,000	211,000	284,000	223,000
(+) Total Influent	758,308	701,475	693,045	658,002	697,377	634,649	679,500
(-)Effluent Irrigation	520,530	519,803	470,917	489,241	476,510	482,164	504,049
(-)Rapid Infiltration	0	0	0	0	0	0	0
(-)Unaccounted Losses	206,778	159,672	248,128	154,761	147,867	213,485	184,451
Net Storage at Year-End (m ³)	198,000	222,000	197,000	211,000	284,000	223,000	214,000

TABLE 1-9: HYDRAULIC BALANCE DATA FOR 2009 TO 2022

2016	2017	2018	2019	2020	2021	2022
214,000	247,000	275,000	289,000	245,000	246,000	221,000
639,793	689,098	666,376	625,911	655,853	607,731	622,711
454,221	437,919	407,422	469,752	479,090	448,741	431,562
0	23,322	38,391	16,858	11,117	2,256	3,752
152,572	199,857	206,564	183,301	164,646	181,734	159,397
247,000	275,000	289,000	245,000	246,000	221,000	249,000

There is no freshwater contribution to the system. Unaccounted losses within the hydraulic balance include evaporation losses from the treatment lagoons and storage reservoir, seepage losses from both the treatment and storage cells, and flow meter inaccuracies. Unaccounted losses of 159,397 m³ were calculated for 2022.

1.4.5 Irrigation Water Quality Data (OC 5.1 and 6.3)

Effluent quality for reclaimed water prior to irrigation is presented in Table 1-10. Section 5.1 of the OC requires that fecal coliforms do not exceed 200 MPN per 200 mL for agricultural, silvicultural, and low public use lands, or exceed 2.2 MPN per 100 mL for high use public land. As seen, results for the 2022 irrigation season are compliant with the OC criteria.

To provide background data to assist with future assessment studies, the Town of Oliver continued to monitor phosphorus, nitrogen and chloride through 2022. Data for these parameters are tabulated in Table 1-10 and Table 1-11.



	Date	Fecal Coliforms	Total Coliforms	Total P	Total N	Free CL Res
OC Limit		*2.2 MPN/100 ml	n/a	n/a	n/a	n/a
Unit		MPN/100ml	MPN/100ml	mg/L	mg/L	mg/L
April	4	<1	<1	5.7	27.5	0.57
May	9	<1	<1	5.94	26.2	0.34
June	14	<1	<1	5.5	22.1	0.43
July	8	<1	<1	5.39	23.2	0.52
August	10	<1	<1	5.14	19.1	0.53
September	14	<1	<1	2.99	12.8	0.45
October	13	<1	<1	5.42	16.6	0.51

* Note: The operational permit limit for fecal coliform in reclaimed water applied to agricultural land is 200 MPN per 100mL. Most of the reclaimed water in Oliver is applied on the Fairview Mountain Golf Course, which is classified as high public use, hence the lower limit of 2.2 MPN per 100 mL.



Year	Seasonal Average Total Phosphorus (mg/L)	Seasonal Average Total Nitrogen (mg/L)	Seasonal Average Sodium (mg/L)
2000	2.92	12.5	
2001	2.46	14.1	
2002	2.75	13.4	
2003	1.2	6.8	114.3
2004	1.36	9.3	103.5
2005	2.87	11.9	94.4
2006	2.4	11.6	84.4
2007	3.91	11.9	84.2
2008	3.93	14.2	89.5
2009	3.27	12.1	93.7
2010	3.61	13.8	97.1
2011	3.88	16.9	111.2
2012	4.01	14.3	114.6
2013	4.77	19.4	112.6
2014	5.90	26.6	120.6
2015	4.04	20.3	112.3
2016	4.0	14.9	107.0
2017	4.5	16.9	108.0
2018	4.6	19.0	104.7
2019	4.6	18.6	112.5
2020	-	-	-
2021	4.1	18.5	96.9
2022	5.2	21.1	

TABLE 1-11: HISTORICAL RECLAIMED WATER QUALITY DATA

As seen in Table 1-11, the average total phosphorus and nitrogen concentration in 2022 is consistent with values seen in previous years.

In addition to the OC requirements, Section 6.8, the Soils Assessment Program, completed by Hamilton and Associates in June 2020, stipulates that "A ground assessment of any new areas to be irrigated, as shown in the "Irrigation Plan", shall be performed by a suitably qualified professional," and that the "Assessment is to include any suggested restriction or recommendations that the suitably qualified professional deems necessary." A recommendation presented in this report (see Section 4.3 Operational Considerations – Appendix J) is as follows:

"Periodic sampling (i.e. annually) and testing of reclaimed water for metals and ions (specifically sodium and chloride) should take place, with results compared to the applicable British Columbia and Canadian Water Quality Guidelines. This is in addition to testing BOD, TSS and nutrients under the OC."



The Town has historically completed testing of total phosphorus, total nitrogen, and sodium. Average seasonal values from 2000-2022 are presented in Table 1-11.

1.5 Summary of 2022 Operational Data

Operation of the Town of Oliver's wastewater collection, treatment, and reclaimed water system for 2022 is summarized as follows:

- Total influent quantities were 622,711 m³, an increase of 14,980 m³, or 2.3% as compared to 2021. The 2022 annual influent quantity is comparable to previous years.
- Wastewater effluent quality for cBOD₅ in the Town's aerated lagoons had no exceedances of the OC criteria of 45mg/L. TSS values were also well under the OC criteria of 60 mg/L.
- The maximum water level in the storage reservoir was 455.76 masl which equates to a volume of 358,000 m³.
- Reclaimed water quality prior to irrigation use complied with the OC requirements.



2.0 Supplemental Information

2.1 Facility Classification and Operator Certification (OC 3.2 and 3.3)

The Town of Oliver Wastewater Treatment Facility (Facility No. 317) is classified as a Municipal Wastewater Treatment II (MWWT-II) under the Environmental Operations Certification Program.

In compliance with OC Section 3.3 operator certifications are summarized as follows:

Operator	ECOP Certification
Hector Murillo	Wastewater Collection Level I
	Wastewater Treatment Level I
Keith Postnikoff	Wastewater Collection Level II
Ryan Seiling	Wastewater Collection Level I
	Wastewater Treatment Level I
Martin Schori	Wastewater Collection Level II
	Wastewater Treatment Level II
Adrian Zandvliet	Wastewater Collection Level I
	Wastewater Treatment Level I

TABLE 2-1: OPERATOR CERTIFICATION

2.2 Influent Waste Bylaw (OC 3.6 and 7.2.4.4)

2022 Capital Projects included:

- Cleaning and development of MW-6 as per WWAL report recommendations.
- Okanagan Street at Similkameen Avenue improvements.

Capital Projects for 2023 are expected to be deferred to 2024, with the additional 2022 projects being completed in 2023.

2023 Capital Projects include:



- Rotary Beach lift station discharge connection upgrades.
- Finish Okanagan Street at Similkameen Avenue improvements.
- Design Similkameen Avenue replacement for construction in 2024.

2.3 Influent Waste Bylaw (OC 3.6 and 7.2.4.4)

Sanitary Sewer System Use Bylaw No. 547 established regulations respecting the type, volume, and characteristics of wastewater discharged to the sanitary sewer system.

In January 2002, the Town of Oliver received an application from Vincor requesting approval to connect its winery located on the Osoyoos Indian Reserve, north of the Town boundaries, to the Town's sewerage system. This application relates to both process water and normal domestic sewage and was approved by the town.

Vincor was connected to the Town's sewerage system from October 2002 to July 01, 2015. During this period, Vincor's wastewater was sampled by the Town at least twice per month to confirm compliance with the terms and conditions of the connection agreement and for invoicing purposes. Since 2015, there has been no influent received from Vincor.

2.3.1 Infiltration, Inflow, and Cross Connection Reduction (OC 7.2.4.3 and 7.2.4.4)

The Town of Oliver has an ongoing video camera inspection program for the sewer collections system. In addition, they have prepared a 2019 Sanitary Capital Plan. Within the report, SCADA data was analyzed for possible Inflow and Infiltration (I&I) from 2015 to 2019. This I&I analysis will allow for correlations between peak rain events, surface water diversions, and failures within the pipe infrastructure.

The Town regulates provisions to identify, eliminate, and prevent cross contamination with non-potable water sources through Bylaw No. 1043.

2.4 Sludge Management Plan (OC 3.8 and 7.2.4.6)

The Town's Sludge Management Plan was updated in February 2019 and is included in Appendix G. The Plan provides an overview of the system design, sludge characterization, sludge sampling and monitoring, sludge removal, and system recommendations.

Consistent with historical practices, the Town completed sludge depth and analytical sampling in Aerated Lagoon Cell No. 2 in 2021. The analytical data is provided in Appendix G.



2.5 Groundwater Monitoring Plan

In compliance with Section 6.8 of the OC, the Town of Oliver retained the services of Golder Associates to prepare a groundwater monitoring plan in 1997. A hydrogeological review of the Town's reclaimed wastewater irrigation groundwater monitoring program, including irrigation expansion areas, was completed by Western Water Associates Ltd. (WWAL) in 2021 and is included in Appendix H.

A summary of all monitoring wells, their location, and name are provided in Table 2-2 below. Monitoring wells that were undertaken in 2021 are denoted.

Well Identification Number	Location/"Nickname"	Completion Date
Well #1	"Air Cadet"	2005
Well #2	"Rodeo Grounds"	2005
Well #3	"91A Street"	2005
MW-1	Near Higgins/Alonso Property	1997 (Inactive)
MW-2	Near Higgins/Alonso Property	1997 (Inactive)
MW-3	Near Higgins/Alonso Property	1997 (Inactive)
MW-4	"Sand Pit"	2000
MW-5	125th Street	2000
MW-6	Fairview Golf Course	2000
MW-7	Road No. 5	2000
		(Abandoned)
	South Side of Town Public Works	
MW-8	Yard	4-May-21
MW-9	South end of Oliver Cemetery	5-May-21
MW-10	Gala Street Linear Park	6-May-21
MW-11	Road No. 5	7-May-21

TABLE 2-2: SUMMARY OF MONITORING WELLS

Please note that the nomenclature of the wells has changed slightly due to the commissioning and decommissioning of monitoring wells in the area.

In May of 2021, WWAL retained Mud Bay Drilling to address the recommendations of the 2021 hydrogeological review. The following well installations were completed:

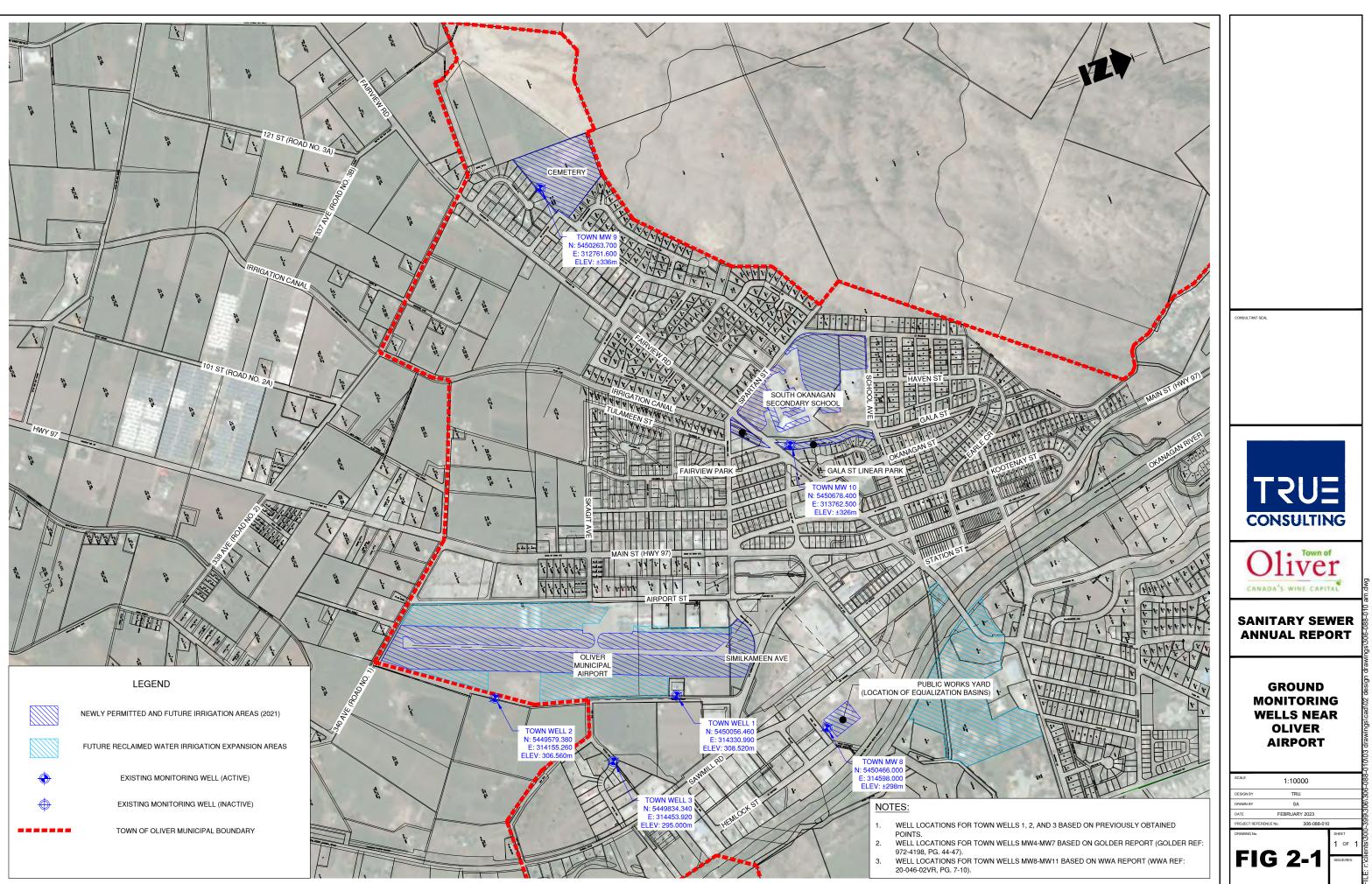
- Three new monitoring wells were installed to provide coverage for new areas receiving reclaimed wastewater for irrigation. This included: the Town Public Works Yard (MW8), Oliver cemetery (MW9), and Gala Street Linear Park (MW10).
- Well MW-11 was installed as a replacement well for Town MW7 located on Road No. 5.
 Moving forward, the MW7 replacement well is MW-11, Road No. 5.

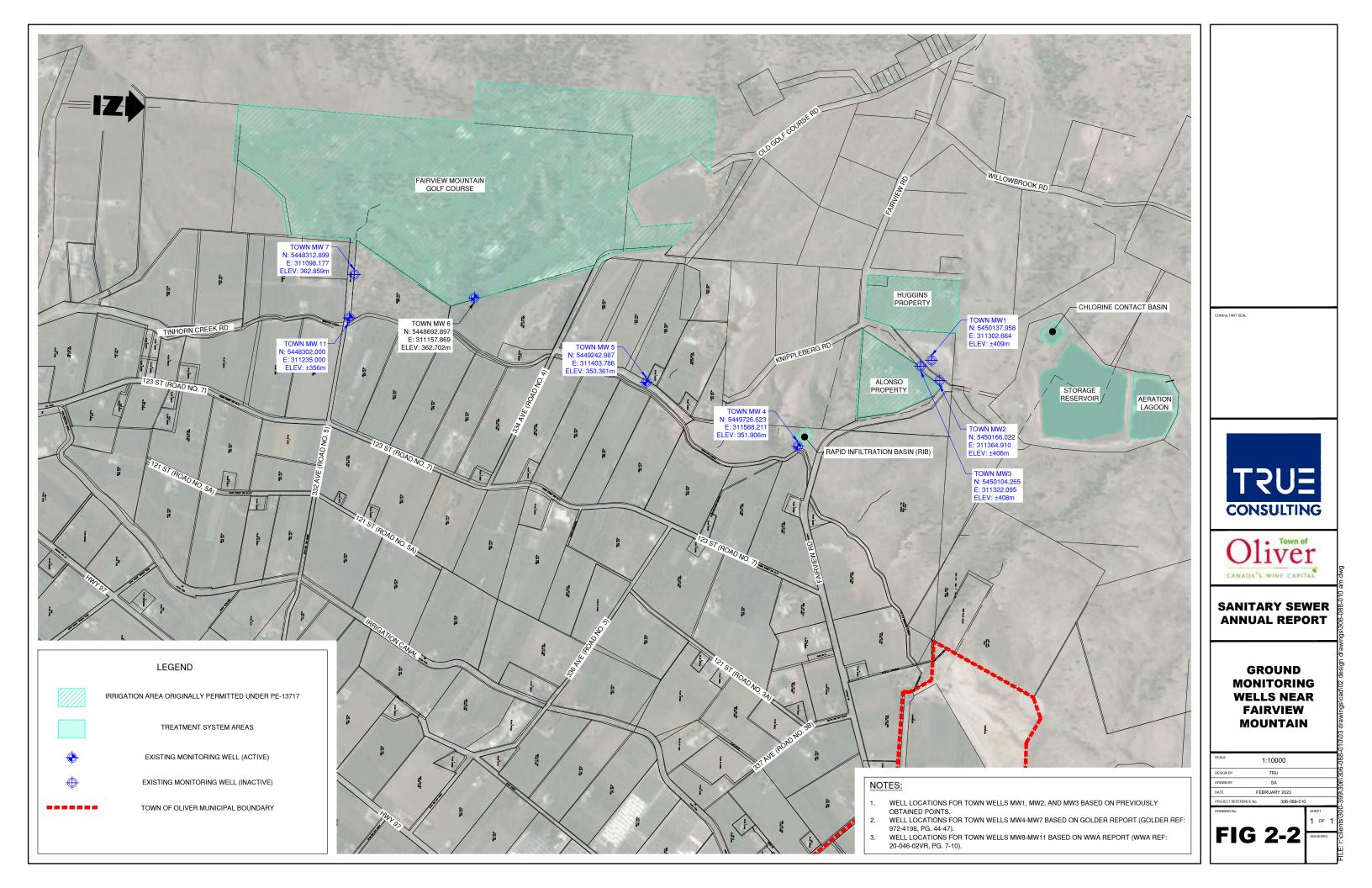


 Lastly, to address recommendations to replace MW6, WWAL attempted to re-develop MW-6 and was successful. Approximately 0.4 m of sediment was removed, and a water quality sample was obtained.

The technical memorandum detailing the installation of the new wells can be seen in Appendix H. For further detail, the Hydrogeological Review of the Town of Oliver Reclaimed Wastewater Irrigation Groundwater Monitoring Program can be viewed in Appendix H. Groundwater monitoring wells located throughout the Town are shown on Figure 2-1 and Figure 2-2.







2.5.1 Groundwater Monitoring Leading Indicators

Typical parameters tested for analyzing impacts on groundwater include chloride, ammonia, nitrate and nitrite and total hardness. Based on the chemical characteristics of each parameter, concentrations will indicate the transport and impact of reclaimed water on the groundwater system.

Chloride does not biochemically degrade and is considered a conservative ion. Its presence is indicative of the extent of anthropogenic influence. It is typically present in low concentrations in freshwater aquifer systems. Elevated chloride can be attributed to anthropogenic activities. This includes reclaimed water irrigation, wastewater effluent disposal to ground, road salting, industrial process and agricultural activity.

Ammonia is the primary form of nitrogen in raw wastewater. It is oxidized to nitrate and nitrite during the wastewater treatment process. When ammonia concentrations are high in the groundwater, it indicates the source is nearby. Anthropogenic sources include wastewater effluent, agricultural activities, urban development, and industrial activities.

Nitrate is seldom present in natural water systems. Concentrations above 3 mg/L are considered by the Province to reflect human impact. Common sources include agricultural activities, wastewater disposal to ground and industrial/mining processes. Nitrite is an unstable ion and rapidly oxidizes to nitrate or nitrogen gas.

Water hardness is a measure of the dissolved mineral content in water, predominantly dissolved ions of calcium and magnesium. It does not have a maximum allowable concentration of aesthetic objective according to the Guidelines for Canadian Drinking Water Quality.

2.5.2 Airport Monitoring Wells No. 1 to 3

There are three monitoring wells proximate to the airport site (Well #1, Well #2, Well #3). These wells are located down gradient from the reclaimed water use area.

In 2011, the Town renamed streets. For clarity, historic street names are referenced in parenthesis in Figure 2-1 and Figure 2-2.

Ten-year groundwater level and analytical data for these wells are summarized in Table 2-3 and Table 2-4. For complete historical data sets and trends, see Appendix I.

As seen, the average groundwater table elevation in Wells #1, #2 and #3 were on average higher than previous years. Notably, Wells #1 and #2 maximum level values were the greatest in the corresponding data set.

The 2022 water quality in these wells was generally within the expected values for the parameters measured. Below is a summary of 2022 water quality observations.

Chloride:



- Chloride in Well #1 was higher than in 2021. The September 7, 2022, concentration was 2.4 mg/L lower than the peak concentration in 2007.
- Chloride concentrations in Wells #2 and #3 were consistent with past concentrations.
- Ammonia:
 - Ammonia concentrations in Well #3 were approximately 0.1 mg/L above historic values, which is not considered significant.
 - Ammonia in the other wells were consistent with historic concentrations.
- Nitrate and Nitrite
 - Nitrate and nitrite concentrations in Well #3 were lower than past concentrations, which corresponds to higher-than-average ammonia concentrations during this period.
 - Nitrate and nitrite concentrations in other wells were consistent with previous values.
- Total Hardness:
 - Values for Well #1 were consistent with historic trends.
 - Total hardness in Well #2 during the September 7, 2022 sample event was 2,980 mg/L. This is the highest concentration measures since 2007. Comparatively in September 2007, May 2018, September 2018, and October 2019, concentrations ≥ 2000 mg/L were observed.
 - An elevated total hardness concentration of 1,260 mg/L was measured in Well #3 on September 7, 2022. The 2022 values were below historic peak concentrations between 2007 - 2013, but above historic concentrations between 2014 - 2020 which were consistently below 500 mg/L.
- Sodium:
 - 2022 sodium concentrations in Wells #2 and #3 appear to be trending up slightly, but they are still within the historic range measured at these wells.
 - Values for Well #1 are consistent with historic values.



Monitoring Well	Year	Minimum Level (mbtoc)	Maximum Level (mbtoc)	Average Level* (mbtoc)	Level Range (m)
	2012	9.84	10.78	10.50	0.94
	2013	9.78	10.44	10.11	0.66
	2014	9.98	10.58	10.33	0.60
	2015	10.01	10.51	10.28	0.50
	2016	10.21	10.5	10.36	0.29
Well #1 Air Cadet	2017	9.9	10.59	10.32	0.69
All Gadet	2018	9.65	10.29	10.03	0.64
	2019	9.72	10.62	10.26	0.9
	2020	9.62	10.51	10.22	0.89
	2021	9.24	10.4	9.8	1.16
	2022	10.16	10.85	10.51	0.69
	2012	5.84	6.54	6.20	0.70
Well #2 Rodeo Grounds	2013	5.62	6.24	5.91	0.62
	2014	5.84	6.27	6.08	0.43
	2015	5.69	6.66	6.08	0.97
	2016	5.66	5.97	5.82	0.31
	2017	5.98	6.3	6.16	0.32
	2018	5.81	6.24	5.99	0.43
	2019	6.18	6.96	6.61	0.78
	2020	7.07	7.46	7.27	0.39
	2021	7.48	7.78	7.62	0.3
	2022	7.79	8.10	7.94	0.31
	2012	1.38	1.54	1.46	0.16
	2013	1.20	1.39	1.27	0.19
	2014	1.11	1.65	1.37	0.54
	2015	1.21	1.66	1.41	0.45
	2016	1.13	1.43	1.28	0.30
Well #3 91A Street	2017	1.06	1.38	1.23	0.32
	2018	0.87	1.51	1.2	0.64
	2019	1.24	1.78	1.45	0.54
	2020	1.18	1.72	1.44	0.54
	2021	1.2	2.1	1.7	0.9
*Donth indiantas the	2022	1.51	2.16	1.73	0.65

TABLE 2-3: 10-YEAR HISTORICAL SUMMARY OF GROUNDWATER DEPTHS FOR AIRPORT MONITORING WELLS

*Depth indicates the measurement from the top of casing to the water level.



Water quality analysis of these wells can be seen in Table 2-4.

Monitoring Well	Sample Date	Chloride	Ammonia	Nitrate + Nitrite	Total Hardness	Sodium
	24-Apr-2012	16.4	0.04	7.59	464	20.0
	16-Oct-2012		0.034	9.7	481	19.8
	9-Apr-2013		0.034	10.1	384	18.5
	9-Sep-2013		< 0.020	20.2	383	17
	16-Apr-2014		0.027	21.6	542	18.1
	4-Sep-2014	19.8	< 0.020	23.9	402	19.5
	14-Apr-2015	20.7	0.102	24.4	485	20.5
	16-Sep-2015	15.9	0.079	20.5	590	23.5
	-	-	-	-	-	-
Well #1	13-Sep-2016	13.7	0.032	15	386	19.1
Air Cadet	10-Apr-2017	14.2	0.033	12	388	19.5
	11-Sep-2017	10.4	<0.020	6.97	392	18
	14-May-2018	11.9	0.025	6.75	363	19.1
	10-Sep-2018	9.92	<0.020	7.97	344	16.8
	28-Oct-2019	9.77	0.023	12.6	388	19.6
	6-Apr-2020	10.3	<0.050	13	331	18.8
	1-Sep-2020	9.31	<0.050	11.1	378	19.4
	22-Apr-2021	8.83	<0.050	11	316	17.1
	13-Sep-2021	12.1	0.094	9.67	303	17.6
	11-Apr-2022	16.9	<0.050	9027*	319	17.6
	7-Sep-2022	22.2	<0.050	8.3	320	18.6
	24-Apr-2012	10.6	0.01	0.749	572	17.4
	16-Oct-2012		0.021	0.263	661	17.8
	9-Apr-2013		0.047	0.121	384	18.4
	9-Sep-2013		0.023	0.115	889	18
	16-Apr-2014		0.024	0.123	392	15.9
	4-Sep-2014	8.47	0.02	0.584	370	15.9
	14-Apr-2015	9.05	0.094	0.865	494	18.5
Well #2	16-Sep-2015	6.56	0.037	0.3	1120	31.6
Rodeo	-	-	-	-	-	-
Grounds	13-Sep-2016	6.54	0.032	0.628	1110	19.2
	10-Apr-2017	7.6	0.072	0.343	914	20.4
	11-Sep-2017	6.1	0.02	0.124	959	17.1
	14-May-2018	7.2	0.1	0.122	2550	20.3
	10-Sep-2018	7.07	0.037	0.138	2090	18.9
	28-Oct-2019	6.55	0.103	0.385	2440	20.8
	6-Apr-2020	6.44	0.101	0.212	394	17.2
	1-Sep-2020	6.86	0.081	0.173	1540	18.9

TABLE 2-4: 10-YEAR HISTORICAL WATER QUALITY DATA FOR AIRPORT MONITORING WELLS



	22-Apr-2021	6.78	0.102	0.312	1410	17.5
	21-Sep-2021	9.24	0.081	0.045	1740	20.4
	11-Apr-2022	7.14	0.068	0.324	1970	20.5
	7-Sep-2022	7.51	<0.050	0.872	2980	23.6
	24-Apr-2012	18.4	0.09	0.270	1470	36.9
	16-Oct-2012		0.04	0.033	924	31.6
	9-Apr-2013		0.049	0.074	834	23.9
	9-Sep-2013		0.07	0.101	1430	24.6
	16-Apr-2014		0.028	0.058	399	16.9
	4-Sep-2014	125	0.023	0.032	438	21.8
	14-Apr-2015	8.99	0.086	0.106	631	18.9
	16-Sep-2015	7.59	0.047	0.035	496	18.5
	-	-	-	-	-	-
Well #3	13-Sep-2016	8.01	0.032	0.214	389	17.2
91A Street	10-Apr-2017	8.07	0.059	0.334	366	16.7
	11-Sep-2017	7.64	<0.020	0.042	346	15.2
	14-May-2018	8.31	0.024	0.0507	381	15.4
	10-Sep-2018	8.05	0.031	0.739	355	14.4
	28-Oct-2019	7.87	0.121	0.349	360	16
	6-Apr-2020	8.03	0.095	0.315	371	16.3
	1-Sep-2020	8.47	<0.050	0.0929	443	16.5
	22-Apr-2021	8.68	<0.050	0.25	356	15.2
	21-Sep-2021	7.77	0.15	0.307	1120	15.1
	11-Apr-2022	8.48	0.191	<0.0200	559	15.7
* Overested error	7-Sep-2022	9.04	0.141	0.0886	1260	19

* Suspected error.

2.5.3 Fairview Monitoring Wells

The Town of Oliver has seven groundwater monitoring wells downgradient of the Fairview area. Refer to Figure 2-1 and Figure 2-2 for their locations. Notes specific to well sampling in this area are as follows:

- MW-1, MW-2, and MW-3 were not included in the 2022 data collection. These wells were
 installed in 1997 as part of hydrogeological investigation supporting the design and
 commissioning of a rapid infiltration basin (RIB), which is no longer in use. As such, these
 wells are no longer monitored.
- The newly drilled monitoring well at the south end of the Cemetery (MW-9) was dry during the sampling event, therefore there is no water quality data available for this year.



Ten years of historical data for groundwater level monitoring is presented in Table 2-5. The depths of all wells were comparable to previous years. For complete historic data sets and trends, see Appendix I.

Ten years of historical data for groundwater quality analysis is presented in Table 2-6. The 2022 water quality in these wells was generally within the expected concentrations for the parameters measured. For complete historic data sets and trends, see Appendix I.

Below is a list summarizing water quality observations for the 2022 sampling period. A detailed review was completed by WWA and will be issued as an addendum to this report.

- Chloride:
 - 2022 chloride concentrations at MW4 are consistent with historic trends. Historically high chloride at this location is associated with its proximity to the RIB and surrounding agricultural activity.
 - Chloride concentrations at MW6 and MW11 are slightly below those at MW4. These concentrations are influenced by reclaimed water infiltration at the Fairview Gulf Course.
 - MW5 experiences the lowest chloride values which is expected given its further proximity from an irrigation source. This is used as a background well.
 - Values at MW8 and MW10 are similar and in the mid-range of chloride concentrations. The irrigation sources for these two locations smaller footprint and irrigate less then half of the volume of sources located upstream of MW6, and MW11.
- Ammonia:
 - Ammonia concentrations for all monitoring locations, excluding MW8, are below detectable limits.
 - The only ammonia concentrations above the detection limit was experienced at MW8 which is located at the Public Works Yard.
- Nitrate and Nitrite:
 - All ammonia monitoring well samples were below the detectable limit.
 - All concentrations of nitrate and nitrite were below 5 mg/L. Notably, MW5 experienced the lowest concentration which is attributed to its location as a background well.
- Total Hardness:
 - Elevated total hardness is experienced at MW4 with the September sampling event values being 1,610 mg/L. This value is above the MW4 historic average.
 - All other total hardness concentrations were similar to the historic range experienced at MW5.



Monitoring Well	Year	Minimum Level (mbtoc)	Maximum Level (mbtoc)	Average Level* (mbtoc)	Level Range (m)
	2012	8.48	10.85	9.79	2.37
	2013	8.21	10.64	8.89	2.43
	2014	7.43	9.62	8.57	2.19
	2015	8.08	10.20	8.92	2.12
	2016	7.79	8.98	8.38	1.19
Monitoring Well #4 Sand Pit	2017	6.24	8.33	7.71	2.09
Sand Fit	2018	1.99	8.13	6.75	6.14
	2019	7.81	9.4	8.47	1.59
	2020	7.8	10.43	9.03	2.63
	2021	8.35	10.75	9.30	2.40
	2022	9.03	10.62	9.51	1.59
	2012	6.41	9.54	8.48	3.13
	2013	5.59	9.23	7.95	3.64
	2014	8.13	9.77	9.04	1.64
	2015	-	-	-	-
	2016	4.57	9.90	7.70	5.33
Monitoring Well #5 125th Street	2017	4.56	10.57	7.93	6.01
	2018	5.28	9.09	7.78	3.81
	2019	7.89	9.66	9.01	1.77
	2020	7.36	10.1	9	2.74
	2021	7.1	9.6	8.8	2.5
	2022	7.61	10.13	8.96	2.52
Monitoring Well #6	2012-2019		13.92	(Dry)	
Fairview Golf Course	2021	12.38	12.75	12.58	0.37
	2022	12.87	13.21	13.12	0.34
Test Well # 7 (Road No. 5)	2012-2019			(Dry)	
ABANDONED	2021			doned	
	2022			doned	
Monitoring Well #8	2021	2.76	3.01	2.91	0.25
Public Works Yard	2022	2.00	3.35	2.79	1.35
Monitoring Well #9	2021	21.50	21.1 (dry)	21.20	0.40
Cemetery	2022	21.05	21.44	21.10	0.39
Monitoring Well #10	2021	25.80	27.70	26.40	1.90
Gala Linear Park	2022	25.69	26.59	26.10	0.90
Monitoring Well #11	2021	24.40	30.50	27.00	6.10
Road No. 5	2022	24.55	24.84	24.73	0.29

TABLE 2-5: HISTORICAL SUMMARY OF GROUNDWATER DEPTHS FOR FAIRVIEW MONITORING WELLS



Monitoring Well	Sample Date	Chloride	Ammonia	Nitrate + Nitrite	Total Hardness	Sodium
	24-Apr-2012	130	0.04	2.39	1110	101
	16-Oct-2012		0.034	0.691	1420	119
	9-Apr-2013		0.091	1.78	1070	118
	9-Sep-2013		0.156	2.06	1350	146
	16-Apr-2014		0.073	3.02	1050	115
	4-Sep-2014	125		1.68		127
	Apr. 14, 2015	141		3.56		120
	16-Sep-2015	135	0.023	1.53	1440	127
	-	-	-	-	-	-
•••••	13-Sep-2016	129	0.021	1.63	1700	19.2
Monitoring Well #4 Sand Pit	10-Apr-2017	121	0.084	10.2	820	108
ound in	11-Sep-2017	110	<0.020	3.05	387	11.5
	14-May-2018	111	0.035	4.12	725	100
	10-Sep-2018	96	0.043	2.99	838	87.1
	28-Oct-2019	103	0.222	16.9	704	93
	6-Apr-2020	119	0.091	8.03	659	92.2
	1-Sep-2020	101	0.072	1.11	1120	86.9
	22-Apr-2021	125	<0.050	4.19	782	81.7
	21-Sep-2021	101	0.073	0.967	2020	97.1
	11-Apr-2022	119	<0.050	3.51	991	81.2
	7-Sep-2022	121	<0.050	1.35	1610	92
	24-Apr-2012	48.8	1.9	3.19	460	22.4
	16-Oct-2012		0.025	2.94	446	19.3
	9-Apr-2013		0.036	1.11	381	15.9
	9-Sep-2013		0.071	0.652	398	12.4
	16-Apr-2014		0.022	0.577	465	13.1
	4-Sep-2014	14.7		0.683		14
	14-Apr-2015	16.7		1.31		14.7
Monitoring Well #5	16-Sep-2015	27.7	< 0.020	0.794	456	31.6
125th Street	-	-	-	-	-	-
125th Street	13-Sep-2016	23.9	0.022	1.11	960	20.4
	10-Apr-2017	17	0.052	1.21	481	14.1
	11-Sep-2017	16.5	0.089	1.11	917	88.4
	14-May-2018	16	0.058	0.569	400	12.8
	10-Sep-2018	15.6	0.066	1.59	348	10.3
	28-Oct-2019	16.1	0.774	2.18	415	13.6
	6-Apr-2020	16.7	<0.050	1.6	409	14
	1-Sep-2020	17.7	<0.050	2.28	419	17.7

TABLE 2-6: HISTORICAL WATER QUALITY FOR FAIRVIEW MONITORING WELLS



	22-Apr-2021	17.5	<0.050	1.69	386	16.5
	21-Sep-2021	16.4	0.073	1.6	374	15.1
	11-Apr-2022	13.5	<0.050	0.796	292	9.87
	7-Sep-2022	16.1	<0.050	1.17	442	15.9
	21-Sep-2021	95.6	<0.050	2.33	396	96.9
Monitoring Well #6 Fairview Golf Course	11-Apr-2022	95.2	<0.050	2.76	369	94.5
	7-Sep-2022	95.7	<0.050	2.81	395	102
	21-Sep-2021	45.5	<0.050	2.28	311	35.7
Monitoring Well #8 Public Works Yard	11-Apr-2022	48.7	<0.050	2.58	278	30.4
	7-Sep-2022	87.8	0.737	1.47	353	48.2
	21-Sep-2021	165	<0.050	5.89	317	67.1
Monitoring Well #10 Gala Linear Park	11-Apr-2022	37.9	<0.050	3.18	312	22.4
	7-Sep-2022	85.1	<0.050	3.94	674	62.8
	21-Sep-2021	97.7	<0.050	3.21	493	18.4
Monitoring Well #11 Road No. 5	11-Apr-2022	114	<0.050	4.13	470	17.8
	7-Sep-2022	115	<0.050	4.34	498	18.3

2.5.4 Groundwater Monitoring Plan Recommendations

Groundwater levels and water quality were generally consistent with previous years. To improve the groundwater monitoring program, the following recommendations are made:

- Purge MW-6 and then sample the following day with a bailer. This can be included in the monthly groundwater level and semi-annual water quality sampling programme.
- Include MW-1, MW-2, and MW-3 in the monthly groundwater level and semi-annual water quality sampling.
- Obtain monthly groundwater quality data at MW-4 for 1 year.
- Capture MW-4 transducer readings.

Additional commentary and analysis of 2022 hydrogeological data will be provided WWA by issuance of an independent addendum for annual reporting purposes.



2.6 Soils Assessment (OC 5.4, 5.5, and 6.9)

In accordance with Section 6.9 of the OC, a soils assessment of the irrigated areas was completed in June 2020 and is summarized herein. Soils were identified using a detailed soil survey of the central and southern Okanagan and Lower Similkameen Valley. This information was published in the MOE Technical Report 18 Soils of the Okanagan and Similkameen Valleys, 1986.

The conclusions found in the 2020 report prepared by Hugh Hamilton Associates are as follows.

- The schoolvard, cemetery, and park sites are all suitable for irrigation with reclaimed wastewater subject to the regulatory water quality requirements for reclaimed water.
- The airport lands east of the existing irrigated area will require special management.
 - This area has a limited irrigation season (June 15 to September 10).
 - Apply approximately ¹/₂ the rate outlined in the BC Agriculture Water Calculator.
 - Once vegetative cover improves and a layer of organic litter develops, the irrigation rates may be re-evaluated.
- Overall, the irrigation areas are capable of accepting reclaimed water for irrigation purposes.

For full report details please refer to Appendix J.

A summary of the soil classifications, characteristics, physical properties, and drainage for the reclaimed water irrigation areas is presented in Table 2-7. Detailed individual profile descriptions and an overview map of the soil parent materials is provided in Appendix J. As seen, all irrigated areas are well to rapidly drained except for the Public Works Yard. At this location, reclaimed water is used for compost operations and landscape irrigation, therefore it does not present an issue with respect to surface runoff or surfacing of reclaimed water.

Irrigation Location	Soil Name	Soil Texture	Drainage	Coarse Fragment	Parent Material	
Cemetery ^{1,2}	Ponderosa	Sandy Loam	Well-drained	65	FLUV	
Oliver Secondary School ^{1,2}	Rutland	Sandy Loam	Rapidly-drained	63	GLFL	
High School Park ¹	Rutland	Sandy Loam	Rapidly-drained	63	GLFL	
Public Works Yard ^{1,2}	Cawston	Silt Loam	Rapidly-drained	15	FLUV	
Airport ¹	Rutland	Sandy Loam	Rapidly-drained	63	GLFL	
Oliver Community Park ³	Kinney	Sandy Loam	Imperfect	-	FLUV	
Alonso	Approved in Operational Certificate PE-13717					
Huggins	Approved in Operational Certificate PE-13717					
Fairview Mountain Golf Course	Approved in	Operational Certif	icate PE-13717			

TABLE 2-7: SOILS OVERVIEW – RECLAIMED WATER IRRIGATION AREAS

¹Approved in Principle by the Ministry in August 2022

²Previously irrigated with freshwater, simple replacement

³Area considered for future reclaimed water irrigation



2.6.1 Soil Descriptions (OC 6.9)

Soil descriptions for each soil type are as follows:

Ponderosa Soils

Ponderosa soils only occur in the vicinity of Oliver. They have developed in a gravelly, moderately coarse textured fluvial veneer between 10 to 50 cm thick, overlying gravelly coarse textured fluvial fan deposits. Surface and subsurface textured are gravelly or very gravelly sandy loam or gravelly loam. Subsoils are very gravelly loamy sand. The soil drainage class is well to rapid.

Rutland Soils

Rutland soils occupy significant areas throughout the Okanagan Valley. The parent material is a moderately coarse textured veneer between 10 and 25cm thick, which overlies gravelly and stony, very coarse textured glaciofluvial deposits. Surface soil textures are dominantly sandy loam or loamy sand. Subsurface materials are gravelly sand or gravelly loamy sand. The soil drainage class is rapid.

Cawston Soils

Cawston soils occur on the Okanagan River floodplain. They have developed in medium textured recent fluvial deposits generally between 50 to 100 cm thick, overlying moderately coarse textured materials. Surface and subsurface textures are silt loam or loam. Subsoil textures are gravelly sandy loam or gravelly loamy sand. They are moderately pervious, have a high water holding capacity and slow surface runoff. The soil drainage class is dominantly poor, ranging to imperfect.

Kinney Soils

Kinney soils occur on the Okanagan River floodplain between Penticton and Osoyoos Lake. They have developed in a loamy fluvial veneer, usually between 30 and 80 cm thick, that overlies sandy floodplain deposits. Surface and subsurface textures are loam or sandy loam with a subsoil that is loamy sand or sand, occasionally containing thin silty lenses. They are imperfectly drained, moderately pervious and have moderate to low water holding capacity.

2.6.2 Surface Runoff (OC 5.4)

To date, the Town has not observed surface water runoff generated from reclaimed water irrigation use. As outlined in the soil profiles, the parent material at each irrigation area is generally well-drained. Runoff has also not been an operational issue due to the arid climate.

2.6.3 Surfacing Reclaimed Wastewater (OC 5.5)

The irrigation system is designed and managed to ensure that there is no surfacing of irrigation tail water downslope of the point of irrigation. A hydrogeological study of the rapid infiltration basin was completed by Golder Associated in 1998. The system capacity of 355 m³/day was derived



on the basis of the natural discharge capacity of the subsurface soils such that surfacing of effluent will not occur within 150m of the site.

3.0 Analytic Recommendations

As per OC Section 6.6, Sampling and Analytical Requirements, 6.6.5 "The permittee is required to follow the terms of the Quality Assurance Regulation (EQDA). Ten percent of the samples collected shall be duplicated to provide data quality assurance." Currently, duplicate sampling is not being conducted. For this reason, it is recommended that duplicate testing be carried out in 2023. Furthermore, it is recommended that duplicates be distributed throughout the monitoring programs to improve the quality of this analysis.



APPENDIX A

Operational Certificate for PE 13717



Province of British Columbia

MINISTRY OF

ENVIRONMENT,

LANDS AND PARKS



Environmental Protection #201-3547 Skaha Lake Rd. Penticton, British Columbia V2A 7K2 Telephone: (604) 490-8200 Fax: (604) 492-1314

Date: December 14, 1995

File: 76750-40/PE-13717 (01)

REGISTERED MAIL

The Corporation of the Town of Oliver PO Box 638 Oliver BC VOH 1TO

Attention: Tom Szalay, Administrator

Enclosed is a copy of the Operational Certificate No. PE-13717 issued under the provisions of the Waste Management Act. This Operational Certificate supersedes Permit PE-00102 which is cancelled in accordance with Section 16(13) of the Waste Management Act. Your attention is respectfully directed to the terms and conditions outlined in the Operational Certificate. An annual Permit fee will be determined according to the Waste Management Permit Fee Regulation.

This Operational Certificate does not authorize entry upon, crossing over, or use for any purpose of private or Crown lands or works, unless and except as authorized by the owner of such lands or works. The responsibility for obtaining such authority shall rest with the Operational Certificate holder.

This Operational Certificate is issued pursuant to the provisions of the Waste Management Act to ensure compliance with Section 34(3) of that statute, which makes it an offence to discharge waste without proper authorization. It remains the responsibility of the Operational Certificate holder to ensure that all activities conducted under this authorization comply with any other applicable legislation which may be in force from time to time.

The administration of this Operational Certificate will be carried out by staff from our Regional Office located in Penticton, (telephone 490-8200). Plans, data and reports pertinent to the Operational Certificate are to be submitted to the Environmental Protection office, Suite 201, 3547 Skaha Lake Road, Penticton, British Columbia, V2A 7K2. - 30th Street, Vernon, British Columbia, V1T 9G3.

This decision may be appealed by any person(s) who considers themselves aggrieved by this decision, in accordance with Part 5 of the Waste Management Act. Written notice of intent to appeal must be received by the Regional Waste Manager within twenty-one (21) days of the date of notification of this decision.

Yours truly,

T.R. Forty, P.Eng. Assistant Regional Waste Manager Okanagan Sub-Region

Enclosure



Environmental Protection #201 - 3547 Skaha Lake Road Penticton British Columbia, V2A 7K2 Telephone: (604) 490-8200

MINISTRY OF ENVIRONMENT, LANDS AND PARKS

OPERATIONAL CERTIFICATE

PE 13717

Under the Provisions of the Waste Management Act

TOWN OF OLIVER

P.O. Box 638

Oliver, British Columbia

V0E 1T0

is authorized to discharge reclaimed wastewater to the ground by irrigation, from a municipal sewage collection and aerated lagoon sewage treatment facility located at Oliver, British Columbia, subject to the conditions listed below. Contravention of any of these conditions is a violation of the Waste Management Act and may result in prosecution.

1. SPECIFIC AUTHORIZED DISCHARGES AND RELATED REQUIREMENTS

The discharge of effluent to which this sub-section is applicable is from a municipal sewage treatment facility located approximately as shown on the attached Site Plan A and Site Plan B. The reference number (S.E.A.M. site number) for this discharge is E222150.

1.1 Discharge Quantity

- 1.1.1 The maximum authorized rate of effluent to be discharged from the aerated lagoon sewage treatment system to the reclaimed wastewater storage reservoir, averaged on a monthly basis:
 - 1995 1950 m³ per day 1996 - 2000 m³ per day 1997 - 2050 m³ per day 1998 - 2100 m³ per day 1999 - 2150 m³ per day 2000 - 2200 m³ per day

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1.1.2 There is no maximum authorized rate of reclaimed wastewater to be discharged from the storage reservoir for beneficial use as irrigation water.

1.2 Discharge Quality

1.2.1 It is recommended that to ensure reclaimed wastewater is adequately renovated prior to irrigation, the characteristics of the effluent discharged from the aerated lagoon treatment system to the reclaimed wastewater storage reservoir not exceed:

5 Day Biochemical Oxygen Demand, 45 mg/L; and

Total Suspended Solids - 60 mg/L.

1.3 Permit Fee Calculations for Reclaimed Wastewater Discharge to Land

1.3.1 The characteristics of the reclaimed wastewater discharged from the storage reservoir and beneficially used for irrigation, for the purposes of permit fee calculations, the following discharge factors have been assumed:

5 Day Biochemical Oxygen Demand, 10 mg/L; and

Total Suspended Solids - 10 mg/L.

1.4 Authorized Works

The works authorized are: sewage collection system, sewage treatment plant concrete tankage for emergency containment, influent screen, flow equalization basin, pumping station, pressure forcemain to aerated lagoons, aerated lagoon treatment system, reclaimed wastewater storage reservoir sized to provide a minimum retention time of 60 days prior to spray irrigation, post storage chlorination, pressure forcemain to the golf course and related irrigation supply mains and sprinkler irrigation equipment, infiltration basin, and other related appurtenances, approximately as shown on the attached Site Plan A.

1.5 Source of Discharge

The source of discharge and sewage collection system services the Town of Oliver and surrounding area.

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1.6 Location of Works

The location of the sewage collection, flow equalization basin and effluent pumping station is: Block 47 of District Lot 2450s, Similkameen Division of Yale District.

The location of the effluent aerated lagoon treatment facilities, reclaimed wastewater storage reservoir, chlorination and withdrawal facilities is: District Lot 763s, and Block B, District Lot 682s, Similkameen Division of Yale District. The location of the potential infiltration basin sites: Block K, Plan 1789 (Town Sand Pit) and Lot 2, Plan 5881 (Town Gravel Pit).

1.7 Location of Discharge

The location where reclaimed wastewater may be irrigated is described generally as Oliver and the surrounding area.

1.8 Irrigation Plan

Submit for review, and obtain written authorization from the Regional Waste Manager, an "Irrigation Plan" of all new areas of land to be irrigated prior to commencement of irrigation with reclaimed wastewater. Areas for effluent irrigation are as indicated in the Oliver Waste Management Plan and as indicated on Site Plan A.

2. <u>GENERAL REQUIREMENTS</u>

2.1 Maintenance of Works, Emergency Procedures and Noncompliance Reporting

Inspect the pollution control works regularly and maintain them in good working order. In the event of an emergency or any condition which prevents continuing operation of the approved method of pollution control or results in noncompliance with the terms and conditions of this Operational Certificate, immediately notify the Regional Waste Manager and take appropriate remedial action.

2.2 Bypasses

The discharge of effluent which has bypassed the designated treatment works is prohibited, unless the consent of the Regional Waste Manager is obtained and confirmed in writing.

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2.3 **Process Modifications**

Notify the Regional Waste Manager, and his written consent obtained, prior to implementing changes to any process that may affect the quality and/or quantity of the discharge.

2.4 Alternate Water Supply

Provide alternate water supplies if any privately owned well is adversely affected by the land disposal scheme as determined by the Regional Waste Manager.

2.5 Plans - New Works

- 2.5.1 Plans of modifications and/or extensions to the existing works shall be signed and sealed by a Professional Engineer licensed to practise in the Province of British Columbia.
- 2.5.2 Copies of all "as-built" plans and drawings for the effluent treatment system, signed and sealed by a Professional Engineer licensed to practise in the Province of British Columbia, shall be submitted to the Regional Waste Manager on completion of construction.
- 2.5.3 Plans and specifications of any proposed new works, modifications or additions to the works authorized in this Operational Certificate, including the infiltration basin plans, and with the exception of the sewage collection system, shall be submitted to the Regional Waste Manager, and his written consent obtained before construction commences. The works shall be constructed in accordance with such plans.
- 2.5.4 Retain a copy of all "as-built", plans of modifications and/or extensions to the sewage collection system for perusal by the Regional Waste Manager, or his designate, upon request.
- 2.5.5 Plans for modifications of, and/or extensions to, the existing reclaimed wastewater irrigation system shall be approved by a person qualified in the design of irrigation systems.
- 2.5.6 Design and construct the irrigation works in accordance with best current agricultural practice and:

The "Pollution Control Guidelines for Municipal Effluent Application to Land", dated January 1983, and any amendments thereto, issued by the Ministry of Environment of British Columbia.

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The "B.C. Sprinkler Irrigation Manual" 1989 issue, prepared by the B.C. Ministry of Agriculture and Fisheries.

The "Health and Safety Criteria for the Use of Reclaimed Wastewater", 1991, developed by the Ministry of Health and the Ministry of Environment.

3. GENERAL REQUIREMENTS - ALL DISCHARGES

3.1 Operation and Maintenance

Develop and maintain both an Operational and Maintenance Manual for the sewage collection, sewage treatment and reclaimed wastewater utilization. A copy of the Operational and Maintenance Manuals shall be retained at the treatment facility for inspection by the Regional Waste Manager or their designate.

3.2 Facility Classification

Maintain the wastewater treatment facility classification as authorized in Section 1.4 with the "British Columbia Water and Wastewater Operators Certification Program Society" (BCWWOCPS). The new aerated lagoon treatment facility is presently classified as a Level II facility.

3.3 Operator Certification

- 3.3.1 All operators in training (OIT) working at this Level II facility classified by the BCWWOCPS shall be required to successfully pass an OIT examination within three (3) months of commencement of employment at the facility. The OIT certificate shall be valid for fifteen (15) months from the date of issue. Prior to the expiry date of the OIT certificate, but not sooner than twelve (12) months from the date when the OIT commenced facility operation, the OIT shall successfully complete a Class I certification examination in order to continue to operate at the facility.
- 3.3.2 The facility is currently classified by the BCWWOCPS at Level II. Designate at least one operator to be the "Chief Operator" of the facility by **December 1, 1996**. The "Chief Operator" shall be certified at a Class II level, at a minimum.

After December 1, 1996, no person shall have "Direct Responsible Charge", as defined by the BCWWOCPS, of a municipal wastewater

T.R. Forty, P.Eng Assistant Regional Waste Manager

Date issued: December 14, 1995 Amendment Date: (most recent) Page: 5 of 18 treatment facility classified at Level II or higher unless they possess a valid operator's certificate not more than one level below the classification level of the facility. "Direct Responsible Charge" is the "Chief Operator" of the facility, the identifiable senior person who is in charge of the plant.

- 3.3.3 Should the facility be reclassified by the BCWWOCPS at Level III, designate a "Chief Operator", certified at a Class III level by **December 1, 1998**.
- 3.3.4 Should the facility be reclassified by the BCWWOCPS at Level IV, designate a "Chief Operator", certified at a Class IV level by December 1, 1998.

3.4 Water Conservation

Establish a water conservation program to encourage a reduction in the volume of domestic and industrial wastewaters discharged to the sewage collection system.

3.5 Sewage Collection System - Groundwater Infiltration, Inflow and Cross Connections

Inspect and maintain the sewage collection system works so as to minimize the possibility of cross connections between the storm sewer and the sanitary sewer systems, to minimize infiltration of groundwater, to minimize inflow of water from basement sump pumps and roof drains, and minimize exfiltration of the collected sewage from the sewage collection system to the ground.

3.6 Influent Wastes Bylaw

Subject to being declared a Sewage Control Area under Section 17 of the Waste Management Act, and in order to minimize the potential effect of heavy metals or other toxic materials in the effluent and/or sludge, prepare, implement and/or amend an Influent Wastes Bylaw, Building Bylaw, or other similar bylaws, to regulate the input of such wastes to the sewage collection system. Devices to process household putrescible waste for disposal to the sewage collection system shall be prohibited.

3.7 Contingency Plan

Prepare a Contingency Plan that will address the appropriate course of action to be taken in any particular preconceived emergency situation. The Contingency Plan shall include chlorine leaks and any potential point of concern in the collection, treatment and disposal systems. Attention is to be given to public

T.R. Forty, P.Eng. Assistant Regional Waste Manager

Date Issued: December 14, 1995 Amendment Date: (most recent) Page: 6 of 18 safety and the protection of the environment. The Contingency Plan is to be continually updated as necessary to reflect the current operation. A copy of the Contingency Plan shall be forwarded to the Regional Waste Manager on or before December 31, 1997.

3.8 Sludge Management Plan

The rationale of sludge management, including frequency of withdrawal of sludge from the sewage treatment plant and the location(s) used for disposal and/or utilization shall be developed into a Sludge Management Plan. The Sludge Management Plan shall be prepared and submitted to the Regional Waste Manager for approval on or before December 31, 1996.

3.9 Odours

Should odours become objectionable, additional works shall be provided when so directed in writing by the Regional Waste Manager.

3.10 Fencing

Erect a fence around the sewage treatment facility, storage reservoir and such other areas as required by the Regional Waste Manager. The height and type of fencing shall meet the approval of the Regional Waste Manager.

3.11 Surface Water Diversionary Works

Surface water shall be intercepted and diverted away from the effluent treatment facilities to the greatest extent possible.

3.12 Signage

- 3.12.1 A suitable sign erected at the main entrance to the site shall have the appropriate emergency phone numbers for use by the general public and others.
- 3.12.2 Prominent "NO TRESPASSING", signs shall be erected around agricultural and silvicultural sites irrigated with reclaimed wastewater, warning persons of the possible health hazard during the irrigation season and advising that the water used for irrigation is NOT POTABLE. The wording shall be in language or symbols readily comprehensible by the general public. eg. "NO TRESPASSING - RECLAIMED WASTEWATER - DO NOT DRINK"

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4. <u>GENERAL REQUIREMENTS - EFFLUENT STORAGE RESERVOIR</u>

4.1 Leakage

Operate and maintain the reclaimed wastewater storage reservoir to minimize fluid leakage. Leakage shall not aggravate or produce soil or bedrock instability or erosion elsewhere or contaminate ground or surface water.

5. GENERAL REQUIREMENTS - EFFLUENT IRRIGATION

5.1 Disinfection - Chlorination

- 5.1.1 Adequate chlorination shall be maintained and provide not less than one hour's contact time at average flow rates in the reclaimed wastewater discharging from the chlorination facility to the irrigation system.
- 5.1.2 Reclaimed wastewater utilized for irrigation shall conform to the effluent irrigation guidelines developed by the B.C. Ministry of Health. Fecal coliforms shall not exceed 200 MPN per 100 mL for agricultural, silvicultural and low public use lands, or exceed 2.2 MPN per 100 mL for high public use lands.

5.2 Annual Irrigation

- 5.2.1 The authorized discharge period for irrigation is during the period March 15 to October 31, inclusive.
- 5.2.2 With the written authorization of the Regional Waste Manager, the irrigation schedule may be extended on a weekly basis beyond these limits. Any extension will be considered only upon receipt of a substantiated written request.

5.3 Buffer Zones

- 5.3.1 The requirement for formal buffer zones surrounding lands irrigated with reclaimed wastewater is no longer in effect, however, a buffer zone may be specified by the Regional Waste Manager.
- 5.3.2 Reclaimed wastewater applied by irrigation shall not be applied to the ground any closer than 15 metres from the edge of flowing streams or bodies of water.
- 5.3.3 There shall be no reclaimed wastewater irrigated within 30 metres of any well or inground reservoir for domestic supply.

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5.4 Surface Runoff

There shall be no surface runoff of irrigated reclaimed wastewater from the irrigated lands.

5.5 Surfacing Reclaimed Wastewater

Irrigation shall be managed in such a fashion as to preclude surfacing of irrigation tail water down slope of the point of irrigation.

5.6 Spray Irrigation Drift

The reclaimed wastewater irrigation system shall be managed in such a fashion as to preclude aerosol drift from leaving the irrigated lands.

5.7 Irrigation Rates

- 5.7.1 Irrigation rates shall not exceed the rates given in "B.C. Sprinkler Irrigation Manual", dated 1989, prepared by the B.C. Ministry of Agriculture and Fisheries.
- 5.7.2 Soils of the irrigated lands shall be monitored to prevent saturation, erosion, and instability.

5.8 Agricultural Products Lag Time

- 5.8.1 A three day lag time is required before uninspected livestock intended for human consumption are permitted on areas irrigated with reclaimed wastewater. No lag time is required if livestock are subjected to the federal meat inspection program.
- 5.8.2 A six day lag time is required before dairy cattle are permitted in areas irrigated with reclaimed wastewater.
- 5.8.3 A three day lag time, after irrigation has ceased, is required before a crop intended for animal feed is harvested.

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6. MONITORING REQUIREMENTS

6.1 Influent Sampling Program - (Equalization Basin)

- 6.1.1 Install and maintain a suitable sampling facility at the equalization basin outlet, (S.E.A.M. site number E222152), and obtain a grab sample of the plant influent semi-annually (a proportional continuous sampler may be used).
- 6.1.2 Obtain analyses of the influent sample for the following:

total phosphorus and ortho phosphorus, expressed as P in mg/L;

6.2 Effluent Sampling Program - (Cell #3, prior to storage reservoir)

- 6.2.1 Install and maintain a suitable sampling facility on the outlet of the aerated treatment lagoon, Cell #3, (S.E.A.M. site number E222151), and obtain a grab sample of the effluent before it is discharged to the storage reservoir, for analysis by a suitably accredited laboratory, a proportional continuous sampler may be used, provided that prior written approval has been obtained from the Regional Waste Manager.
- 6.2.2 Obtain analyses of the effluent sample for the following:

total suspended solids (non-filterable residue), (monthly analysis), mg/L;

5-day biochemical oxygen demand, (monthly analysis), mg/L;

total phosphorus, ortho phosphorus and total dissolved phosphorus, (quarterly analysis during 1996, and semi-annually analysis, thereafter), all expressed as mg/L P; and

total nitrogen, ammonia nitrogen, nitrate nitrogen, nitrite nitrogen, and organic nitrogen, (quarterly analysis during 1996, and semiannually analysis thereafter), all expressed as mg/L N.

6.2.3 Occasional full chemical analysis of the main cations and anions and other characteristics may be required at the discretion of the Regional Waste Manager.

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6.3 Effluent Irrigation Sampling Program - (Chlorine Contact Chamber, prior to Irrigation)

- 6.3.1 Install a suitable sampling facility after the chlorine contact chamber, prior to irrigating, (S.E.A.M. site number E222150) and obtain a grab sample of the reclaimed wastewater during the irrigation season.
- 6.3.2 Obtain analyses of the sample, parameters and frequency as follows:

faecal coliforms, M.P.N./100ml, on a monthly basis;

total coliforms, M.P.N./100ml, on a monthly basis;

total phosphorus, mg/L, on a monthly basis;

total nitrogen, mg/L, on a monthly basis; and

chlorine residual, mg/L, on a weekly basis.

6.3.3 Occasional full chemical analysis of the main cations and anions and other characteristics may be required at the discretion of the Regional Waste Manager.

6.4 Effluent Irrigation Monitoring Program

- 6.4.1 Provide and maintain a suitable flow measuring device to measure total volume of reclaimed wastewater irrigated annually and record the areas where it is utilized.
- 6.4.2 Provide and maintain a suitable flow measuring device to measure the amount of fresh water make-up from Okanagan River to the equalization basin in m³/day, and totalize this make up water volume on an annual basis in m³/year.
- 6.4.3 Provide and maintain a suitable flow measuring device and record once per day the reclaimed wastewater volume irrigated over a 24-hour period. Record the flows for each calendar month and for each calendar year.

6.5 Storage Reservoir Level Monitoring Program

6.5.1 Provide a suitable staff gauge or other similar device as approved by the Regional Waste Manager in the storage reservoir and take weekly measurements of the water level in the storage reservoir on a year round basis.

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6.6 Sampling and Analytical Requirements

- 6.6.1 Proper care should be taken in sampling, storing and transporting the samples to adequately control temperature and avoid contamination, breakage, etc.
- 6.6.2 Occasional full chemical analysis of the main cations and anions and other characteristics may be required at the discretion of the Regional Waste Manager.
- 6.6.3 Analyses are to be carried out in accordance with procedures described in the second edition of "A Laboratory Manual for the Chemical Analysis of Waters, Wastewaters, Sediments and Biological Materials, (March 1994 Permittee Edition)", or by suitable alternative procedures as authorized by the Regional Waste Manager.

The above manual may be purchased from Queens Printer Publications Centre, 2nd Floor, 563 Superior Street, Victoria, B.C., V8V 4R6, 1-800-663-6105. The manual may also be reviewed at any Environmental Protection Program Office.

- 6.6.4 Sampling and flow measurement shall be carried out in accordance with the procedures described in "Field Criteria for Sampling Effluents and Receiving Waters", April 1989, 17 pp., or by other suitable alternative procedures as authorized by the Regional Waste Manager.
- 6.6.5 The Permittee is required to follow the terms and conditions of the <u>Quality Assurance Regulation</u> (EQDA). Ten percent of the samples collected shall be duplicated to provide data quality assurance. Quality control information generated by the Permittee lab while analyzing parameters required by this Permit shall also be provided with the data required to be reported.

6.7 Sludge Sampling and Monitoring Program

Develop and maintain a record keeping system for measuring and recording the depth of sludge collecting in the lagoons and volume of sludge removed from the treatment lagoons during desludging operations, the location where the sludge was discharged, and the amount of sludge discharged at each location. The Regional Waste Manager is to be notified in writing at least two weeks prior to the commencement of desludging operations. Analysis of the sludge may be required by the Regional Waste Manager.

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6.8 Groundwater Monitoring Program

A Groundwater Monitoring Program, shall be submitted to the Regional Waste Manager. The Groundwater Monitoring Program shall be designed by a Professional Engineer or a Hydrogeological Technologist licensed to practice in the Province of British Columbia, to establish with acceptable scientific accuracy, the groundwater flow pattern and nutrient removal capability of the soil to ensure reasonable notice of impending high phosphorus or nitrate levels that may adversely affect surface water, groundwater or domestic waterwells. The sampling, measurement frequency and analyses shall be conducted in accordance with the Groundwater Monitoring Program upon its written authorization by the Regional Waste Manager. The Groundwater Monitoring Program to be submitted to the Regional Waste Manager by December 31, 1997.

6.9 Soils Assessment Program

A ground assessment of any new areas to be irrigated, as shown in the "Irrigation Plan", shall be performed by a suitably qualified professional, using best current climate and soils data to substantiate that the land is capable of accepting reclaimed wastewater for irrigation purposes. This assessment is to include any suggested restrictions or recommendations that the suitably qualified professional deems necessary. This Soils Assessment shall be submitted to the Regional Waste Manager for review prior to the initial commencement of irrigation annually. Further review and ongoing soils assessments may be required by the Regional Waste Manager.

7. <u>REPORTING</u>

7.1 General Reporting

- 7.1.1 Maintain the monitoring data required in Section 6 for inspection.
- 7.1.2 The influent/effluent water quality analyses and flow data is to be submitted to the Regional Waste Manager such that they are received by the Regional Waste Manager within 30 days of the results being sent out by the testing agency.
- 7.1.3 Monitoring data shall be submitted in an electronic and/or printed format satisfactory to the Regional Waste Manager.

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7.2 Annual Reporting

- 7.2.1 Submit an Annual Report which includes a summary of the results of all sampling and monitoring programs as specified in this permit, data interpretation and trend analyses by a suitably qualified professional.
- 7.2.2 This report is to be in a format which is suitable for review by the public and/or other government agencies.
- 7.2.3 The first report is due on or before 60 days of the end of a calendar year for that year's monitoring. Raw data are to be attached as appendices to the report.
- 7.2.4 Maintain and submit records of the following as a part of the annual report:
 - 7.2.4.1 Records of reclaimed wastewater balance, that is, the flows to and from the storage reservoir. This balance, must also include the freshwater make-up.
 - 7.2.4.2 Records of the duration, intensity, property owner, acreage, location, and type of reclaimed wastewater irrigation.
 - 7.2.4.3 Records of efforts to reduce infiltration, inflow and cross connections for inspection by the Regional Waste Manager or his designate.
 - 7.2.4.4 Records of efforts to administer the Influent Wastes By-law(s) for inspection by the Regional Waste Manager or his designate. Include as an attachment, any amendments to the Influent Wastes By-law(s) that have been made during the past year.
 - 7.2.4.5 Copy of the Contingency Plan.
 - 7.2.4.6 Copy of the Sludge Management Plan.
 - 7.2.4.7 Copy of the Annual Flow Summaries.
 - 7.2.4.8 Copy of the Annual Irrigation Summaries.

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APPENDIX A

Requirements of Reclaimed Wastewater Users

The holder of this Operational Certificate (The reclaimed wastewater supplier) shall be responsible for ensuring that the contractual agreement with the Reclaimed Wastewater User is in accordance with the Operational Certificate. A copy of this Appendix is to be provided to each user prior to the commencement of irrigation <u>EACH YEAR</u>.

1 GENERAL REQUIREMENTS

1.1 Plans - New Works

- 1.1.1 Plans for modifications and/or extensions to the existing reclaimed wastewater irrigation system shall be approved by a person qualified in the design of irrigation systems.
- 1.1.2 Design and construct the irrigation works in accordance with best current agricultural practice and the "Pollution Control Guidelines for Municipal Effluent Application to Land", dated January 1983, and any amendments thereto, issued by the Ministry of Environment of British Columbia, and also in accordance with the "B.C. Sprinkler Irrigation Manual", dated 1989, prepared by the B.C. Ministry of Agriculture and Fisheries.

1.2 Construction Criteria

- 1.2.1 All reclaimed water user valves, shall be of a type or secured in a manner that permits operation by only personnel authorized by each wastewater user. All piping, valves and outlets should be marked to differentiate reclaimed wastewater from domestic water. All reclaimed wastewater controllers, valves, etc., shall be affixed with reclaimed wastewater warning signs.
- 1.2.2 Use or installation of hose-bibbs on any irrigation system presently operating, or designated to operate with reclaimed wastewater, regardless of the hose-bibb construction or identification, is not permitted.
- 1.2.3 There shall be at least a 3 metre horizontal and a 0.3 metre vertical separation (with domestic water pipeline above the reclaimed water pipeline) between all pipelines transporting reclaimed water and those transporting domestic water.

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1.2.4 There shall be no connection between a potable water supply, irrigation water or industrial well, and piping containing reclaimed wastewater, except through an air gap separation or reduced pressure principle device.

1.3 Fencing

The Reclaimed Wastewater User MAY be required by the Regional Waste Manager to erect a fence around the disposal area to restrict public access. The height and type of fencing shall meet the approval of the Regional Waste Manager.

1.4 Signage

- 1.4.1 Prominent "NO TRESPASSING", signs shall be erected around agricultural and silvicultural sites irrigated with reclaimed wastewater, warning persons of the possible health hazard during the irrigation season and advising that the water used for irrigation is NOT POTABLE. The wording shall be in language or symbols readily comprehensible by the general public. eg. "NO TRESPASSING - RECLAIMED WASTEWATER - DO NOT DRINK"
- 1.4.2 Warning signs shall be posted in sufficient numbers and size and at strategic locations to advise the public that reclaimed water is being used. Additional signage may be required as directed by the Regional Waste Manager.

2 <u>GENERAL REQUIREMENTS - RECLAIMED WASTEWATER IRRIGATION</u>

2.1 Buffer Zones

- 2.1.1 The requirement for formal buffer zones surrounding lands irrigated with reclaimed wastewater is no longer in effect, however, a buffer zone may be specified by the Regional Waste Manager.
- 2.1.2 Reclaimed wastewater applied by irrigation shall not be applied to the ground any closer than 15 metres from the edge of flowing streams or bodies of water.
- 2.1.3 There shall be no reclaimed wastewater irrigated within 30 metres of any well or inground reservoir for domestic supply.

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2.2 Surface Runoff

- 2.2.1 There shall be no surface runoff of irrigated reclaimed wastewater from the irrigated lands.
- 2.2.2 The maximum ground slope shall not exceed 20% without the written consent of the Regional Waste Manager.

2.3 Surfacing Reclaimed Wastewater

- 2.3.1 Irrigation shall be managed in such a fashion as to preclude surfacing of irrigation tail water down slope of the point of irrigation.
- 2.3.2 Irrigation shall be managed as to prevent ponding.

2.4 Spray Irrigation Drift

- 2.4.1 Reclaimed wastewater shall be confined to the area designated and approved for reclamation. The reclaimed wastewater irrigation system shall be managed in such a fashion as to prevent aerosol drift from leaving the irrigated lands.
- 2.4.2 Precautions shall be taken to ensure that reclaimed water will not have contact with any facility or area not designated for reclamation, such as passing vehicles, buildings, domestic water facilities, fruit and vegetable gardens, or food handling facilities.
- 2.4.3 Drinking water facilities shall be protected from direct or wind blown reclaimed wastewater spray.

2.5 Irrigation Rates

- 2.5.1 Irrigation rates shall not exceed the rates given in "B.C. Sprinkler Irrigation Manual", dated 1989, prepared by the B.C. Ministry of Agriculture and Fisheries.
- 2.5.2 Soils of the irrigated lands shall be monitored periodically or as otherwise directed by the Regional Waste Manager or the Town of Oliver, to prevent saturation, erosion, and instability.

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2.6 Agricultural Products Lag Time

- 2.6.1 A three day lag time is required before uninspected livestock intended for human consumption are permitted on areas irrigated with reclaimed wastewater. No lag time is required if livestock are subjected to the federal meat inspection program.
- 2.6.2 A six day lag time is required before dairy cattle are permitted in areas irrigated with reclaimed wastewater.
- 2.6.3 A three day lag time, after irrigation has ceased, is required before a crop intended for animal feed is harvested.

2.7 Insect and Vector Control

Adequate measures shall be taken to prevent the breeding of insects and other vectors of health significance, and the creation of odors, slimes or unsightly deposits.

2.8 Irrigation of Public Areas

- 2.8.1 Irrigation on golf courses or cemeteries shall only be practised when the public are not present.
- 2.8.2 Golf score cards shall indicate that reclaimed wastewater is used for irrigation on the golf course lands.

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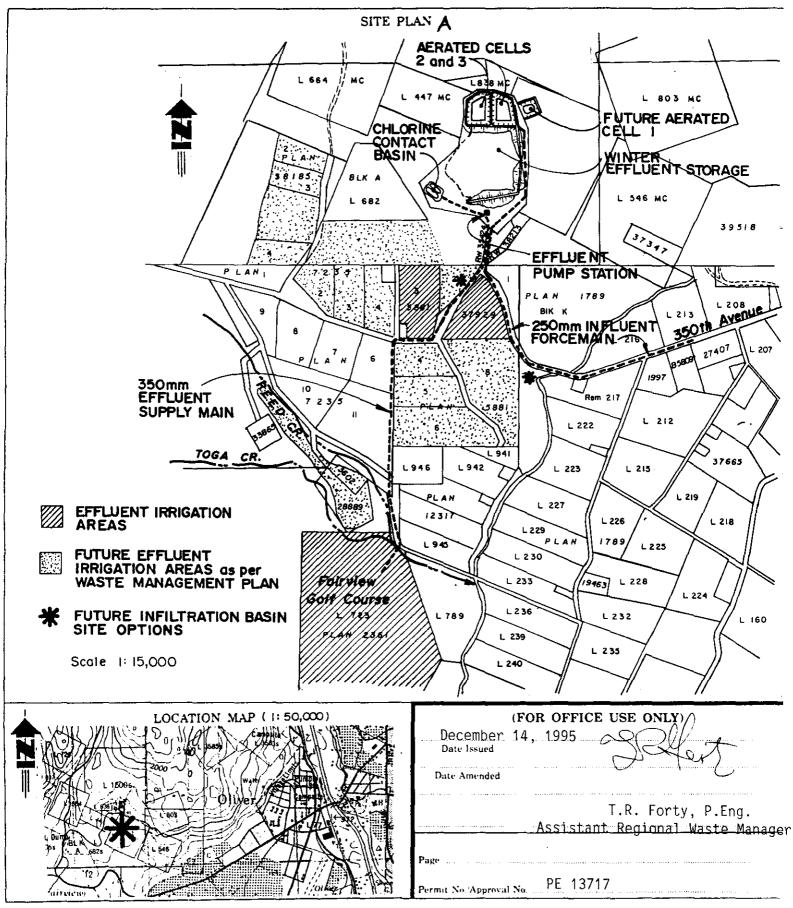
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Province of British Columbia

Ministry of Environment, Lands and Parks





BC

Environment

APPENDIX B

2018 Oliver Sanitary Capital Plan

2018 Sanitary System Capital Plan







EUST

March 2019

Project No. 306-1751

ENGINEERING ■ PLANNING ■ URBAN DESIGN ■ LAND SURVEYING



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Steve Underwood, P. Eng. Project Engineer

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List of Acronyms

AC CPE	Asbestos Cement Chlorinated Polyethylene
FLNRO	Ministry of Forests, Lands, and Natural Resource Operations
GIS	Geographic Information Systems
HDPE	High Density Polyethylene
l&l (l/l)	Inflow and Infiltration
LS	Lift Station
LWMP	Liquid Waste Management Plan
MOE	Ministry of Environment and Climate Change Strategy
MSR	Municipal Sewage Regulation
MWR	Municipal Wastewater Regulation
OC	Operational Certificate
OCP	Official Community Plan
OIB	Osoyoos Indian Band
PCSWMM	Storm Water Management Model
PVC	Polyvinyl Chloride
SCADA	Supervisory Control and Data Acquisition
TRUE	TRUE Consulting
WMP	Waste Management Plan

Units of Measure

km	kilometre
L/d	Litres per day
L/m	Litres per minute
L/s	Litres per second
lpcd	Litres per capita per day
m	metre
m³/day	cubic metre per day
mg/L	milligrams per Litre
mm	millimetre



Referenced Reports

TRUE Consulting Group (2002). *Town of Oliver 2002 Liquid Waste Management Plan Update.*

TRUE Consulting Group (2018). *Town of Oliver Wastewater Treatement System Capacity Improvements.*

Support from FCM

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1.0 Introduction

The purpose of this report is to evaluate the sanitary collection network and treatment system performance under existing and future conditions in order to develop a guide for staged system improvements and expansions. In addition, guideline recommendations from the Ministry of Environment and Climate Change (MOE) to review Liquid Waste Management Plans (LWMP) every 5 to 10 years has prompted an update to the Town's LWMP, which was most recently updated in 2002. This report serves as the 2018 LWMP Update. It includes revisions to the forecasted reclaimed water irrigation flow rates; review of all system works, summarizes upgrades to the Town's collection, treatment and reclaimed water system; and updates projected capital asset management costs.

The following general scope of work was completed:

- Reviewed the Town of Oliver's Liquid Waste Management Plan Update (2002)
- Reviewed historical population and generation rates in the Town in order to generate projected flows on a 20-year design horizon
- Developed a sanitary collection network model using PCSWMM including:
 - Reviewed record drawings and survey data to populate the model
 - Reviewed Official Community Plan (OCP) land use for existing and future conditions
- Reviewed available SCADA data for lift stations and the treatment system.
- Prepared a report to summarize the analysis and recommendations for replacement, rehabilitation, or improvements to infrastructure

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2.0 Background

The Town's sanitary system is referred to in two distinct systems: the sanitary collection network and the treatment system. The sanitary collection network consists of gravity pipe, six lift stations, and their respective forcemains. The collection network converges at the Influent Lift Station where it then begins the treatment process at the screening station. All components beyond and including the screening station comprise the treatment system.

2.1 Sanitary Collection Network

The Town's sanitary collection network consists of approximately 41.5 kilometers of gravity mains, six lift stations, and 3 kilometers of force mains. As shown on Figure 2-1, the gravity network and lift stations convey all generated flows to the Influent Lift Station which pumps into the screening station (the first step in the treatment process). The network is generally separated into six areas, each of which supplies by gravity to one of the lift stations.

- 1. Influent Lift Station
- 2. McPherson Lift Station
- 3. Rockcliffe Lift Station
- 4. Rotary Beach Lift Station
- 5. Sawmill Road Lift Station
- 6. Scott Road Lift Station

The existing sanitary collection network is generally limited to within the Municipal boundary. However, there are some parcels outside the Municipality which are serviced or planned to be serviced in the future. These parcels are primarily on Osoyoos Indian Band (OIB) land. The installation year of infrastructure within the sanitary network ranges from the 1960s to present as there is ongoing development in the Town.

2.2 Treatment System

The original wastewater treatment system consisted of an equalization basin, wastewater pump station and activated sludge treatment system. These works were constructed pre-1985 and are located on the former treatment plant site adjacent to the Town's Public Works Yard at 5971 Sawmill Road. From 1962 to 1984 treated effluent was then discharged into the Okanagan River. In the mid 1980's the Town of Oliver adopted a plan for reuse of treated effluent in the Fairview area, thereby discontinuing direct discharge of treated effluent to the Okanagan River. A summary of system improvements and expansions from 1966 to present are listed in Section 2.2.8.



The existing treatment process now consists of an influent screening station, two equalization basins, a wastewater pump station and forcemain, an aerated lagoon treatment system, reservoir storage, and reclaimed water irrigation system. These system components are described in more detail below, and an overview of the wastewater treatment system can be seen in Figure 2-2, including site plans for the overall reclaimed water supply system and aerated lagoon areas.

2.2.1 Influent Screens

The first step in the treatment process is solids removal. This is achieved by pumping influent through rotating screens. These screens were part of the initial treatment system and are located on the former treatment plant site, adjacent to the Town's Public Works Yard.

A real-time flow meter has operated at the screening station in recent years, however it only began storing historical sub-daily flow data on the SCADA system in December 2018. Sub-daily refers to data taken at shorter intervals (ie. Minutes or seconds) to record flow levels throughout the day. All other flow meters or flow totalizers in the system are located after the equalization basins, and therefore do not represent the actual sub-daily generated flows.

2.2.2 Equalization Basin

Following solids removal, effluent is piped into a two-cell flow equalization system. Construction of Cell 1 was prompted by unreliable electrical services in the South Okanagan in the early 1980's. During this time, the Town experienced numerous, short duration interruptions in their electrical service on a daily basis throughout the summer months. In 1985, a design decision was made to construct a CPE-lined equalization basin (Cell 1) to store flows during short duration power failures rather than provide standby power. Since the early 1980's, the electrical utility has undertaken major improvements to the electrical distribution system and short duration power failures are now infrequent.

Inflow to the equalization basins flows through concrete open channels that formerly comprised the aeration basins and sludge digestor. The decommissioned tankage has a total storage volume of 900 m³ and can be used as emergency storage if required. Piping systems and valves remain in place, allowing for wastewater to be diverted to this tankage and then returned to the normal wastewater system if required.

In 1995, a floating surface aeration mixer was installed in Cell 1 for odor reduction. Cell 2 was constructed in 2009 as a result of energy incentives from Fortis BC to discharge during off-peak hours. Cell 2 is comprised of a 60 mil HDPE membrane lining and aerators, comparable to Cell 1. A site plan of the equalization basin is found in Figure 2-3.

2.2.3 <u>Wastewater Pump Station and Forcemain</u>

Following the equalization basins, the effluent is pumped from the High Lift Station through 3,400 m of 350 mm diameter PVC forcemain to a two-cell aerated treatment lagoon system. Pumping at the High Lift Station generally occurs in the evenings and on weekdays to optimize energy



incentives offered by Fortis BC. The current forcemain was constructed in 2004., during which time the former 250 mm diameter forcemain was converted to a reclaimed water supply main.

2.2.4 Aerated Lagoon Treatment System

This two-cell aerated lagoon system is located off Fairview Road in the southeast area of the Town (see Figure 2-4) and was constructed in 1995 to replace the previous activated sludge plant. The aerated lagoon cells are designated as No. 2 and 3, with a third cell (No. 1) planned in the build out design (see Appendix A).

Air to the system is provided by two 40 Hp positive displacement blowers housed in a building located at the south east corner of aerated cell #2. Piping, electrical and space provisions have been made in the building for installation of two additional blower units. Figure 2-5 shows details of the Aeration Treatment System Layout and Intercell Piping.

2.2.5 <u>Reservoir Storage</u>

The winter effluent storage reservoir was constructed in 1984 and is comprised of two earth fill berms, which traverse the south and east side of a natural topographic depression. The maximum operating elevation of the reservoir is 447.0 m, at which point the surface area of the reservoir is 6.5 ha. Prior to distribution for irrigation use, effluent is pumped from reservoir storage to the chlorine contact basins.

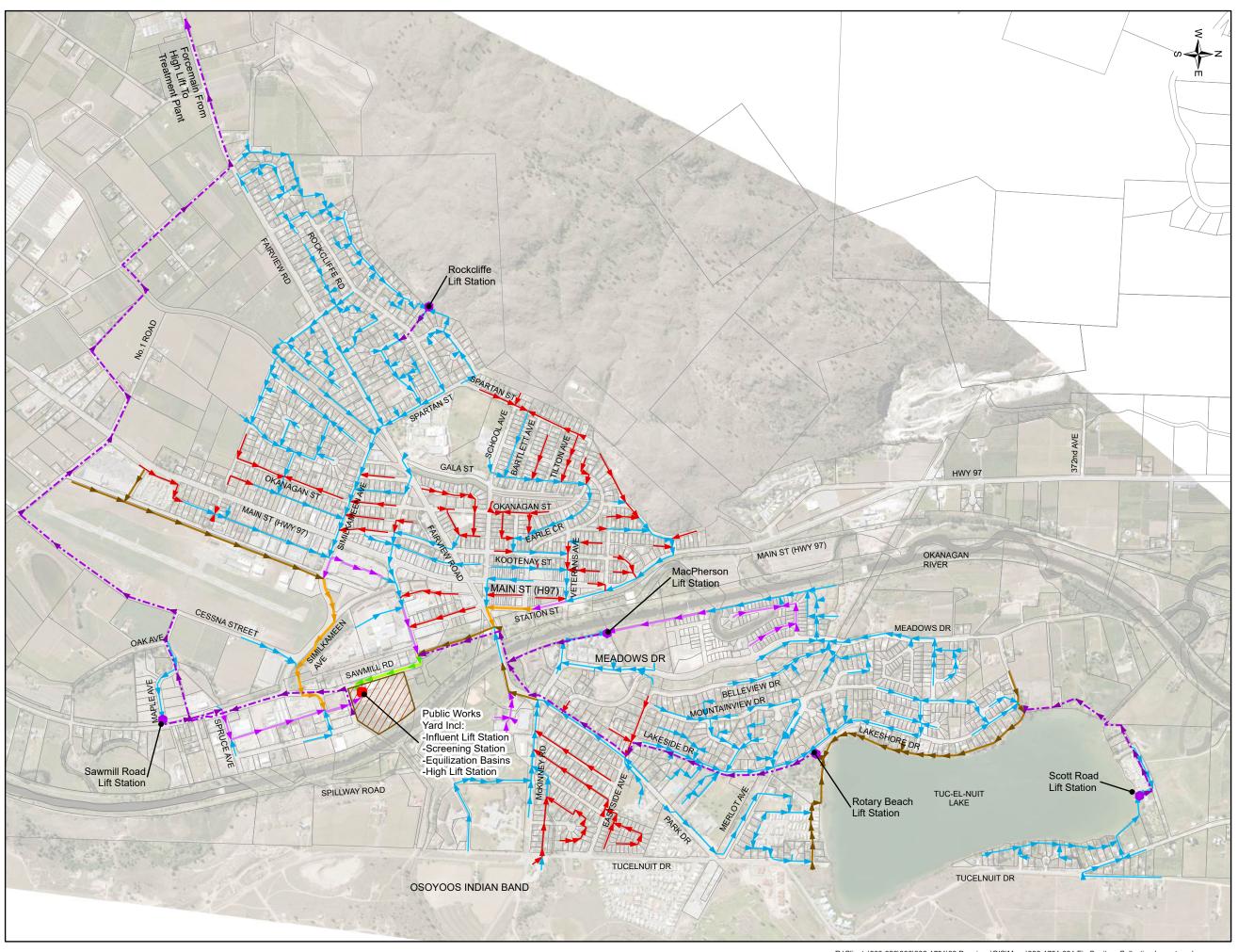
2.2.6 Chlorine Contact Chambers

Following reservoir storage, the irrigation booster station pumps effluent from the winter storage reservoir to the chlorine contact basins. The booster station is equipped with two 50 Hp horizontal split case pumps, which have a combined operating capacity of 76 to 100 L/s (depending on the effluent elevation in the storage reservoir). Space and piping provisions have been made for a third pump. The Town utilizes chlorine gas in the booster station for effluent disinfection, followed by two CPE membrane-lined chlorine contact basins, each measuring 15m x 52m with a design operating depth of 2.6 m operate in series and provide a contact volume of 2180 m³.

2.2.7 Reclaimed Water Irrigation

Reclaimed water supply and distribution was first constructed to the Fairview Mountain Golf Course in the 1980s. From 2004 to 2005, the reclaimed water distribution system was expanded to serve the seven additional sites including: the cemetery, Linear Park, Airport, Public Works Yard, Alonso, Huggins, and the Secondary School as shown on Figure 2-2. This distribution system uses the previous 250 mm diameter sanitary forcemain, now converted to reclaimed water supply. Flow meters measure reclaimed water usage at all sites except the Fairview Mountain Golf Course. Reclaimed water usage at the Fairview Mountain Golf Course has since been calculated as the total annual irrigation volume less all other metered usage.



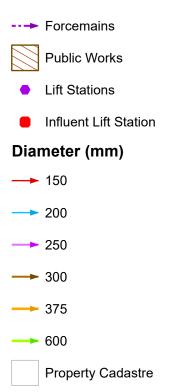


R:\Clients\300-399\306\306-1751\03 Drawings\GIS\Maps\306-1751-001 Fig Sanitary Collection Layout.mxd

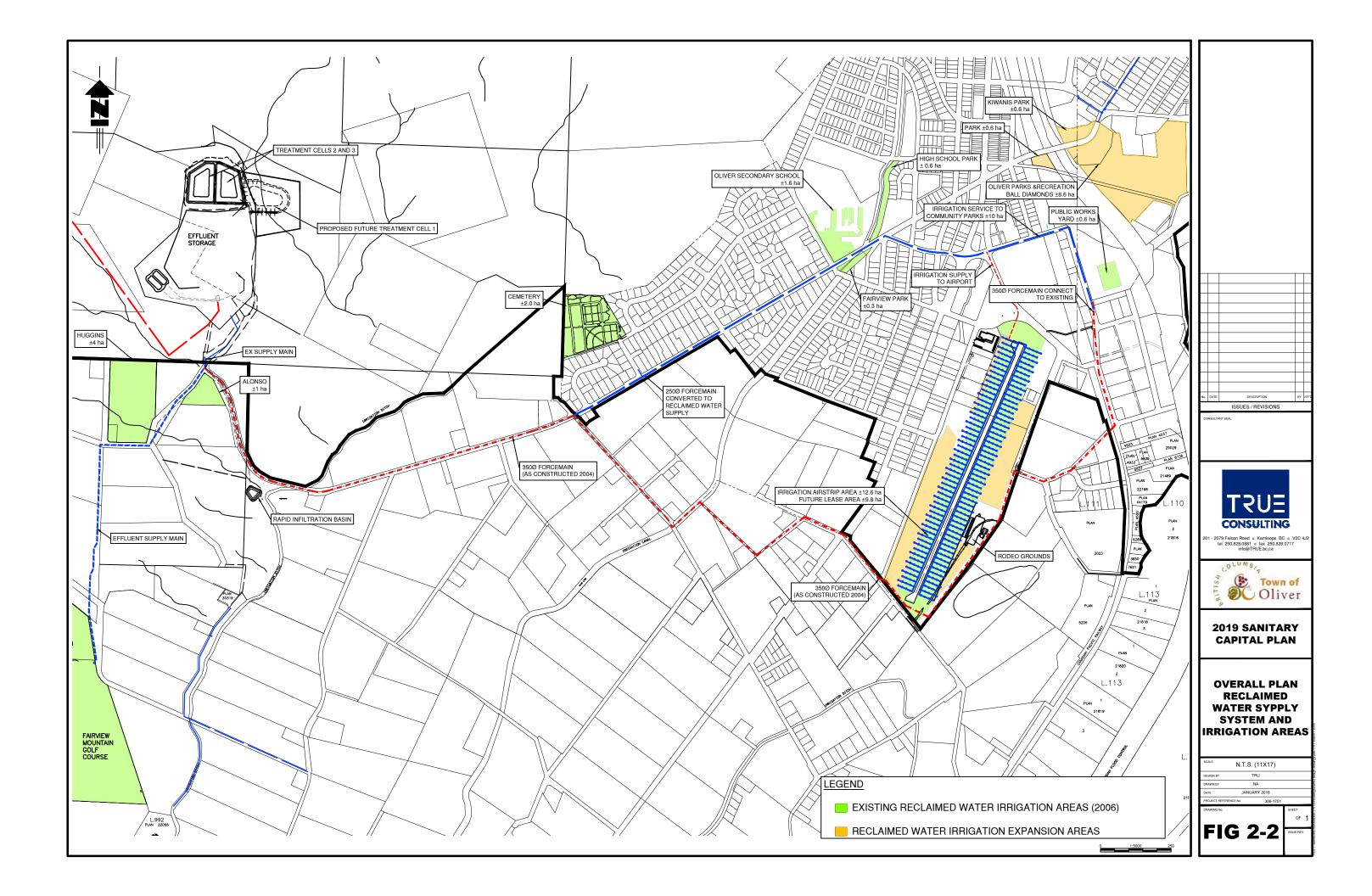


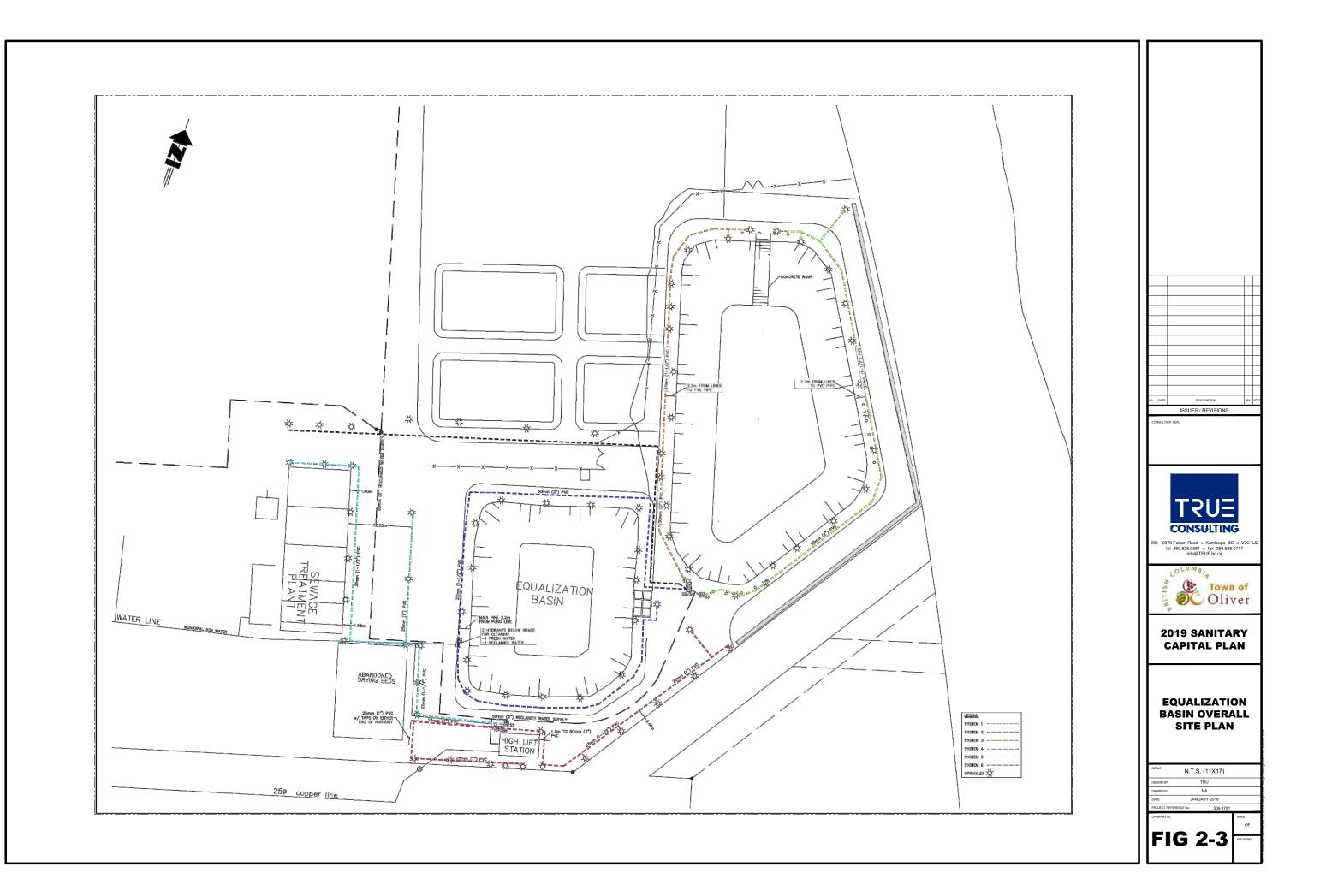
Sanitary Collection Network Layout

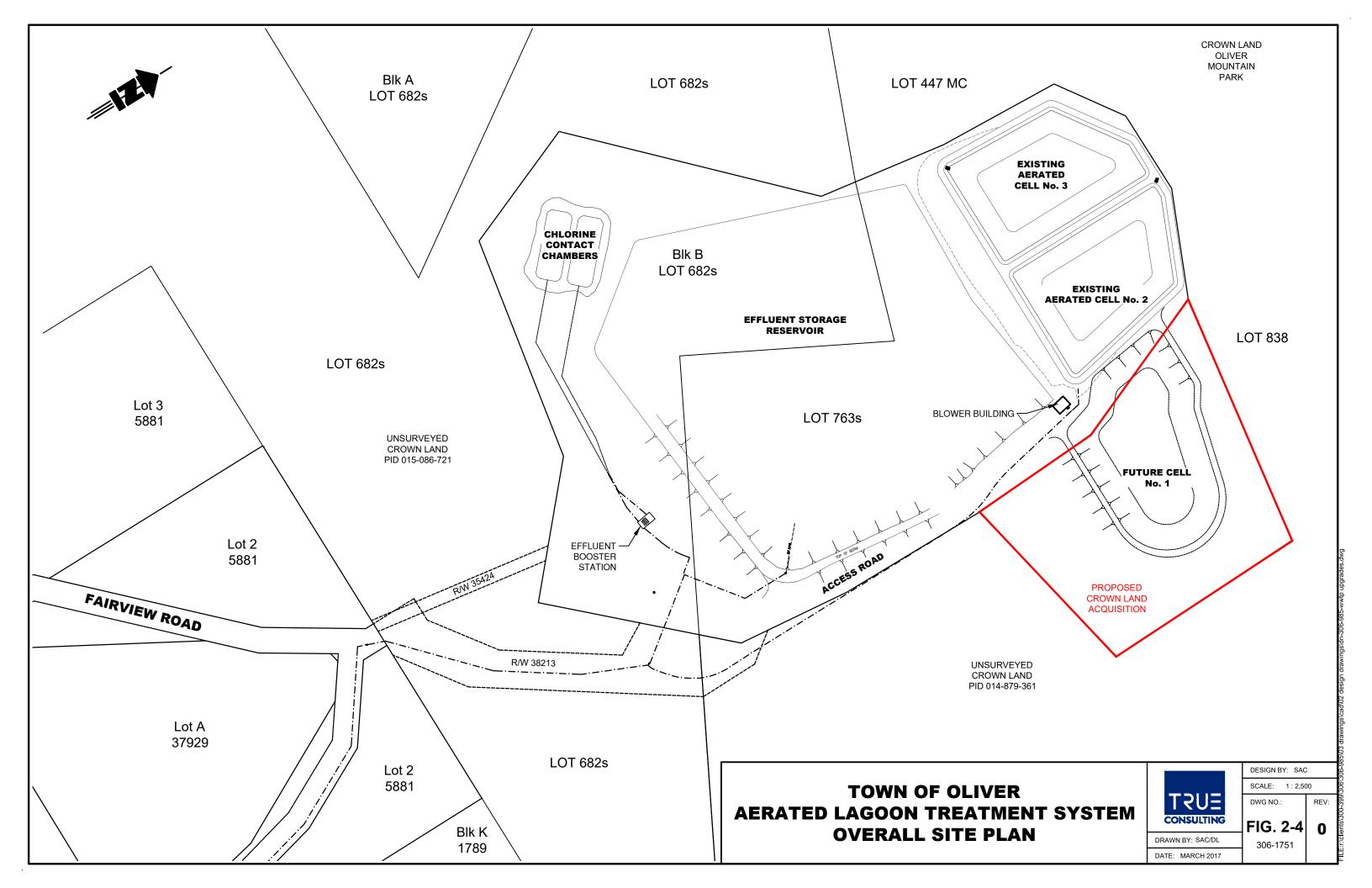
Legend

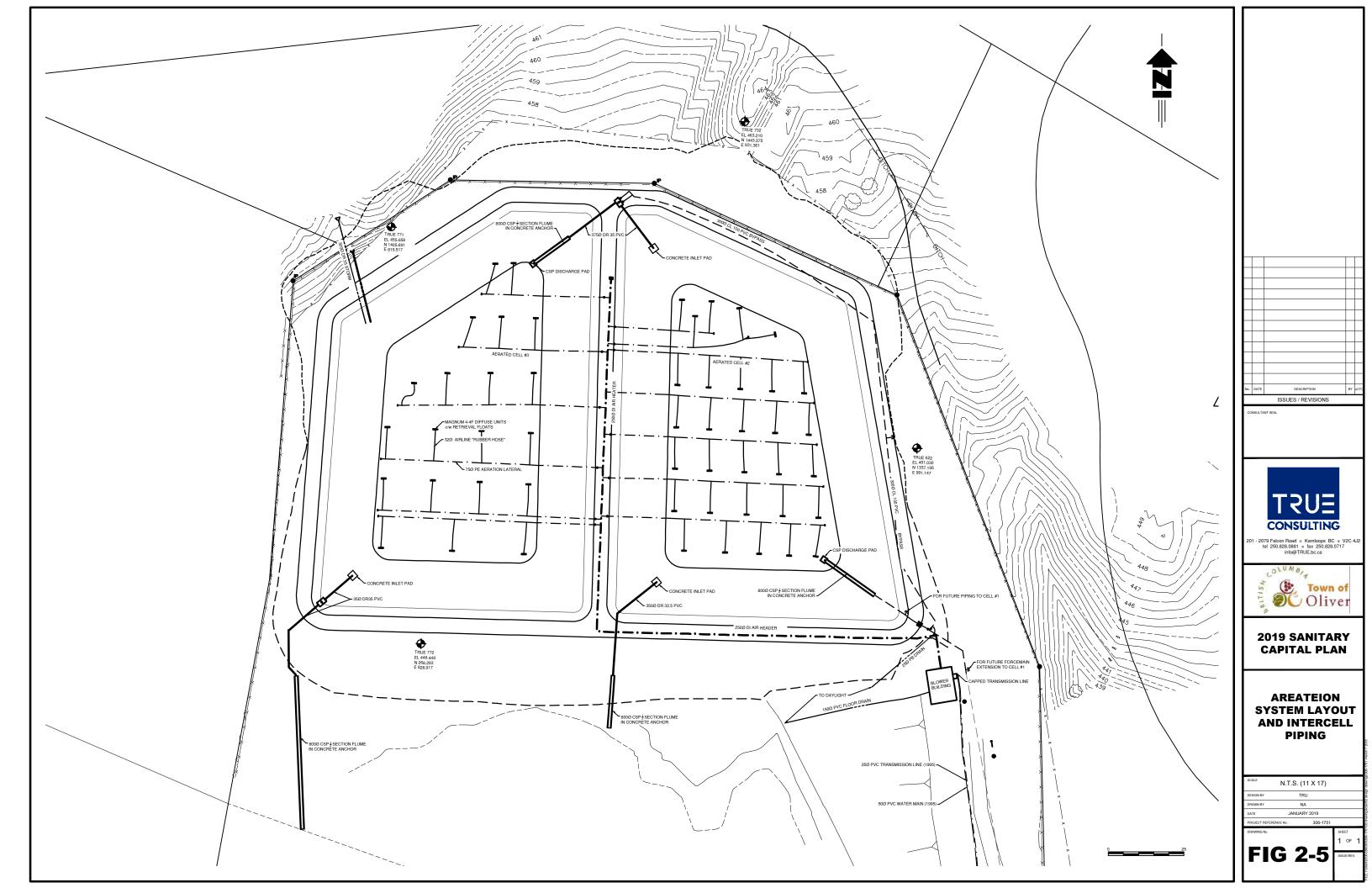


1:12,500 500 125 250 0 Meters Figure 2-1 TRUE









2.2.8 Chronological Summary of Improvements and Expansion of Sewerage Works

The Town completed their first Liquid Waste Management Plan (LWMP) in 1992, which provides a framework for collection, treatment, and disposal of wastewater. An update to the LWMP was completed in 2002, summarizing expansions and upgrades since publication of the 1992 LWMP. System improvements and expansions completed by the Town since 1966 are listed below in Table 2-1.

TABLE 2-1: CHRONOLOGICAL SUMMARY OF IMPROVEMENTS AND EXPANSIONS TO SEWERAGE WORKS

Year		IMPROVEMENTS AND EXPANSIONS				
1966		ary sewage treatment system implementation. ed effluent discharged to Okanagan River.				
1983		view Mountain Golf Course irrigation system constructed. norization Permit No.:PE-00102				
1985	- Rece - Disch	truction of winter effluent storage and land disposal systems in the Fairview area. ipt of Authorization Permit No.: PE13717 narge to Okanagan River discontinued. aimed water supply to Fairview Mountain Golf Course.				
1992		tion of Liquid Waste Management Plan ional lands suitable for irrigation identified.				
1994	- Aerat	ed lagoon earthworks.				
1995	- Blowe	tion system, Topping Lake manhole intake. er building and appurtenances. ational Certificate No. PE-13717 Amended				
1998		n initiated update of 1992 LWMP. d Infiltration Basins on Lot 2 Plan 5881.				
1999	- Town	rate irrigation on Lots 5 and 6, Plan 5881. advised that reclaimed water irrigation expansion in the Fairview area, consistent he 1992 LWMP would not be approved.				
2000		n initiated a second update of the LWMP, with the principle objective of identifying of rexpansion of the reclaimed water irrigation system.				
2001	- Rapio	d Infiltration Basins on Lots 5 and 6 Plan 5881				
2002	- LWM	P Update reviewed and accepted.				
2004	works - Recla - Press - Recla - Public - Airpo sprint - Instal	llation of 5020 metres of 350 mm ductile iron and PVC forcemain from the public s yard to the wastewater treatment site. aimed water supply main from 350 th Ave to the cemetery. sure reducing station at Oliver Secondary School. aimed water supply main from 348 th Ave to the airport. c works yard reclaimed water service construction. rt reclaimed water irrigation system construction, including: pipes, fittings, klers, control valves, etc. llation of flow meters at the airport, park adjacent to high school, cemetery and c works yard.				



Year		IMPROVEMENTS AND EXPANSIONS				
2005	-	Reclaimed water system extensions placed into service at the public works yard, Linear Park, cemetery and airport.				
2009	-	Construction of raw wastewater equalization basin #2.				
2010	-	Upgrading of the chlorine contact basins at the wastewater treatment facility and reclaimed watermain from the reclaimed water booster station to the chlorine contact basin.				
2012	-	Installation of rotary drum screen #2.				
2014	-	Construction of infiltration basin (Town sand pit).				

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3.0 Current and Projected Population

Population data has been updated since the 2002 LWMP Update. Using 2016 census information from Statistics Canada, projected growth rates for the short term and long term design horizons were revised.

3.1 Updated Population Data (1991-2016)

Updated population data is summarized in Table 3-1. This is compared to population estimates projected in the 2002 LWMP Update. To date, only agricultural properties in the North Tuc-El-Nuit Lake and 342nd area remain un-serviced by the Town's sanitary sewer system. Un-serviced properties within municipal boundaries represents approximately 2% of the Town's total population. For the purposes of this analysis, the Actual Population is derived from Statistics Canada and BC Stats.

Year	2002 LWMP ASSUMED POPULATION	ACTUAL POPULATION	ANNUAL AVERAGE POPULATION GROWTH RATE
1991		3,743	2.8%
**1996		4,285	-0.3%
**2001	4,867	4,224	0.7%
**2006	5,320	4,370	2.0%
*2011	5,687	4,824	0.4%
*2016	6,053	4,928	

*Source: Statistics Canada for Actual Population **Source: BC Stats for Actual Population

3.2 Short and Long Term Population Projections

The average population growth rate from the 2001 to 2016 census is 1% annually. While BC Stats predicts population growth within the Regional District to be at a rate of 1% to 1.5%, this is mostly occurring in the City of Penticton and may not be an appropriate representation of the Region. The Town of Oliver Official Community Plan (OCP) anticipates a growth rate between -1% to 1% annually over the next 20 years. To provide a conservative estimate for analysis of the Town's sanitary system, a growth rate of 1% annually has been used for population projections within the Town of Oliver.

As shown in Table 3-2 below, the 10-year population projection (short term design horizon) is anticipated to reach a population of 5,550 and the 20-year population projection (long term design



horizon) is expected to reach a population of 6,130. When compared to the 2002 LWMP Update, the actual 2018 population is approximately 1,200 fewer than previously projected.

YEAR	2018 POPULATION PROJECTION	2002 LWMP POPULATION PROJECTIONS
2016	4,928	6,053
2017	4,977	6,127
2018	5,027	6,200
2028 (Short Term Horizon)	5,550	
2038 (Long Term Horizon)	6,130	

TABLE 3-2: TOWN OF OLIVER SHORT TERM AND LONG TERM POPULATION PROJECTIONS

3.3 Land Use and Equivalent Population

In order to populate a hydraulic model of the collection network, parcel land-use was used to determine the generation rate of flow throughout the sanitary collection network. Detailed dwelling counts at existing conditions were not available from the town, therefore the OCP land-use and typical population densities were used to determine an equivalent population (see Table 3-3).

LAND USE	POPULATION DENSITY		
	PER HA	PER PARCEL	
AGRICULTURAL		1	
COMMERCIAL HWY	50		
COMMERCIAL TOURIST	50		
HIGH DENSITY RESIDENTIAL	80		
INDUSTRIAL	50		
INSTITUTIONAL	50		
LOW DENSITY RESIDENTIAL		1	
MEDIUM DENSITY RESIDENTIAL	40		
OTHER LOTS		1	
TOWN CENTRE	50		

TABLE 3-3: OCP LAND USE AND POPULATION DENSITY

Table 3-4 below shows the calculated equivalent populations for each land use category and the respective serviced area. Based on anticipated future development of undeveloped parcels, the same values were calculated for future conditions. The future equivalent population calculated referencing the OCP land use is consistent with the projected 20-year design horizon population at 1% annual population growth.



	EXISTING CONDITIONS		FUTURE CONDITIONS	
POPULATION DENSITY	EQUIVALENT POPULATION	Area (ha)	EQUIVALENT POPULATION	AREA (HA)
AGRICULTURAL	2	0.8	2	0.8
COMMERCIAL HWY	477	9.5	1065	21.3
COMMERCIAL TOURIST	260	5.2	260	5.2
HIGH DENSITY RESIDENTIAL	760	9.5	1339	16.7
INDUSTRIAL	1560	31.2	1562	31.2
INSTITUTIONAL	1557	31.1	1557	31.1
LOW DENSITY RESIDENTIAL	1431	141.2	1463	155.3
MEDIUM DENSITY RESIDENTIAL	949	23.7	1319	33.0
OTHER LOTS	4	52.1	4	52.1
TOWN CENTRE	406	8.1	452	9.0
Total	7406	312.5	9022	355.8

TABLE 3-4: OCP EQUIVALENT POPULATIONS



4.0 Capacity Assessment of Treatment System

A capacity assessment for each component of the Town's treatment system is described below, including review of wastewater transmission, treatment and disposal. Population growth projections were integrated into the assessment, providing information on the service population capacity of each system component. This assessment was undertaken based on the 2002 LWMP Update and the OC No. PE-13717 for the system.

4.1 Wastewater Flows

4.1.1 Average Influent Flows

A comparison table of average daily and total annual influent flows are shown in Table 4-1. This table compares projections derived in the 2002 LWMP Update to actual data recorded by the Town. As seen, the average daily flow generated from recorded data in 2017 is significantly lower than the daily flow forecasted in the 2002 LWMP Update (1,888 m³/day and 2,423 m³/day respectively).

	2	002 LWMP		ACTUAL				
Year	POPULATION*	Annual Influent Volume (m³)	Avg. Daily Flow (M³/D)	POPULATION	Annual Influent Volume (m³)	Avg. Daily FLow (M³/D)	PER CAPITA FLOW (M ³ /CAPITA/ DAY)	
2002	4,984	744,295	2,039	4,253	726,354	1,990	0.47	
2003	5,100	762,994	2,090	4,282	751,139	2,058	0.48	
2004	5,173	774,771	2,123	4,312	766,048	2,099	0.49	
2005	5,247	786,548	2,155	4,341	783,947	2,148	0.49	
2006	5,320	798,326	2,187	4,370	829,413	2,272	0.52	
2007	5,393	810,103	2,219	4,461	823,011	2,255	0.51	
2008	5,467	821,880	2,252	4,552	777,154	2,129	0.47	
2009	5,540	833,658	2,284	4,642	758,308	2,078	0.45	
2010	5,613	845,435	2,316	4,733	701,475	1,922	0.41	
2011	5,687	857,212	2,349	4,824	693,045	1,899	0.39	
2012	5,760	868,990	2,381	4,845	658,002	1,803	0.37	
2013	5,833	880,767	2,413	4,866	697,377	1,911	0.39	
2014	5,907	892,544	2,445	4,886	634,649	1,739	0.36	
2015	5,980	904,322	2,478	4,907	679,542	1,862	0.38	
2016	6,053	916,099	2,510	4,928	639,794	1,753	0.36	
2017	6,127	927,876	2,542	4,977	689,098	1,888	0.38	

TABLE 4-1: TOWN OF OLIVER SANITARY SEWER INFLUENT FLOWS FROM 2002-2017

*Assumes 1.5% population growth rate from 2002 onwards.



The decrease in per capita sewage flows observed over the past twelve years can be attributed to legislation within the province related to low flow fixture installation, greater public awareness and conservation efforts, as well as disconnection of the Vincor winery. Future wastewater flows derived herein are based on a per capita contribution of 0.38 m³/day and a population growth rate of 1% annually, as shown in Table 4-2.

Year	PROJECTED POPULATION	Annual Average Flow (m³/d)	Average Flow (L/s)
2017	4,977	1,888	21.9
2018	5,027	1,907	22.1
2023	5,283	2,004	23.2
2028	5,553	2,107	24.4
2033	5,836	2,214	25.6
2038	6,134	2,328	26.9
2043	6,446	2,446	28.3
2048	6,775	2,571	29.8
2053	7,121	2,703	31.3
2058	7,484	2,841	32.9
2063	7,866	2,986	34.6
2068	8,267	3,138	36.3
2073	8,689	3,299	38.2
2078	9,132	3,467	40.1
2083	9,598	3,644	42.2

TABLE 4-2: PROJECTED FUTURE INFLUENT FLOWS

4.1.2 Reservoir Operational Data

Effluent is stored in the Town's storage reservoir during the winter months (October to April). This equates to \pm 240 days residence time in the reservoir, including a 60-day retention time, as per the requirements of the Town's OC. Reservoir operational data from 2002-2017 is presented in Table 4-3 on Page 17. The total storage utilized per capita ranges from 37-63 m³ annually. Per capita storage from 2002 was excluded from this range, as the value appears to be a data anomaly. Variability in the rate of utilization can be attributed to climatic factors and user demand.

4.1.3 Annual Effluent Flows

The overall hydraulic balance of treated effluent from 2002 to 2017 is presented in Table 4-4 on Page 18. As seen, total influent volumes have decreased significantly since 2002 and the net effluent storage per capita has varied from year to year. Fluctuations in the reservoir storage requirements are related to seasonal weather variations and changes in user demand effecting irrigation demand. Unaccounted losses are comprised of seepage from the aerated lagoons and effluent storage reservoir, evaporative losses, and flow meter inaccuracies.



Year	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014	2015	2016	2017
Volume in Storage on Jan. 1 (m³)	82,000	90,000	213,000	272,000	205,000	197,000	170,000	167,000	200,000	223,000	197,000	211,000	284,000	223,000	214,000	247,000
Total Influent Volume (m³)	726,354	751,139	766,048	783,947	829,413	823,011	777,154	758,308	701,475	693,045	658,002	697,377	634,649	679,542	639,794	689,098
Total Irrigation Volume (m³)	433,620	401,022	329,575	620,982	636,315	649,220	606,744	520,530	519,803	470,917	489,241	476,510	482,164	504,049	454,221	437,919
Rapid Infiltration (m ³)	0	54,300	139,470	0	0	0	0	0	0	0	0	0	0	0	0	23,322
Unaccounted Losses (m³)	284,734	172,817	238,003	229,965	199,098	200,791	173,410	206,778	159,672	248,128	154,761	147,867	213,485	184,493	152,573	199,857
Net Storage at Year-End (m³)	90,000	213,000	272,000	205,000	199,000	170,000	167,000	198,000	222,000	197,000	211,000	284,000	223,000	214,000	247,000	275,000
Total Area Irrigated (m ²)	450,000	450,000	450,000	186,000	613,000	613,000	613,000	613,000	660,000	660,000	660,000	660,000	186,000	186,000	186,000	623,000
Storage Period (days)	147	153	231	189	189	177	199	180	198	168	161	118	168	183	168	147

TABLE 4-3: RESERVOIR STORAGE AND IRRIGATION SUMMARY 2002-2017



Year		Dате	ELEVATION (M)	Storage Volume (m³)	Storage Period (days)	TOTAL STORAGE USED (M ³)	Total Storage per Capita (m³/capita)
2002	Max.	22-Apr-02	443.73	228,000	147	90,000	21
2002	Min.	16-Sep-02	440.05	34,000	147	90,000	21
2003	Max	22-Apr-03	443.96	240,000	153	213,000	50
2003	Min.	22-Sep-03	440.66	59,000	155	213,000	50
2004	Max.	19-Apr-04	445.77	377,000	231	272,000	63
2004	Min.	06-Dec-04	444.22	260,500	231	272,000	03
2005	Max.	18-Apr-05	446.4	390,000	189	205.000	47
2005	Min.	24-Oct-05	441.18	81,000	109	205,000	47
2006	Max.	24-Apr-06	446.2	380,000	189	100.000	46
2006	Min.	30-Oct-06	440.81	67,000	189	199,000	40
2007	Max.	30-Mar-07	446	370,000	177	170,000	38
2007	Min.	23-Sep-07	440.34	40,000	177		
2008	Max.	13-Apr-08	445.28	445.28 339,000	199	167,000	37
2006	Min.	29-Oct-08	440.39	49,000	199		
2009	Max.	14-Apr-09	445.45	344,000	190	108 000	43
2009	Min.	11-Oct-09	440.72	61,000	180	198,000	43
2010	Max.	06-Apr-10	445.64	352,000	198	222.000	47
2010	Min.	21-Oct-10	440.95	71,000	190	222,000	47
0014	Max.	11-Apr-11	445.75	357,000	400	407.000	
2011	Min.	26-Sep-11	441.09	76,000	168	197,000	41
0040	Max.	02-May-12	445.36	338,000	404	011.000	44
2012	Min.	10-Oct-12	440.99	72,000	161	211,000	44
0040	Max.	25-Apr-13	445.52	355,000	440	004.000	50
2013	Min.	21-Aug-13	441.67	106,000	118	284,000	58
0014	Max.	31-Mar-14	446.06	374,000	400	000.000	40
2014	Min.	15-Sep-14	441.39	92,000	168	223,000	46
0045	Max.	07-Apr-15	445.62	351,000	400	011.000	4.4
2015	Min.	07-Oct-15	441.52	101,000	183	214,000	44
2010	Max.	04-Apr-16	445.47	343,000	400	047.000	50
2016	Min.	19-Sep-16	441.60	105,000	168	247,000	50
2017	Max.	22-May-17	446.17	379,000	4.47	075 000	
2017	Min.	16-Oct-17	442.75	167,000	147	275,000	55

TABLE 4-4: WINTER EFFLUENT STORAGE OPERATING DATA

Historically, reclaimed water usage has been measured by a flow meter located at the booster station (adjacent to the reclaimed water storage reservoir), the Alonso property and the Higgins property. In 2005, flow meters were installed at the cemetery, Linear Park, the airport, the school, and the public works yard. Reclaimed water usage at the Fairview Mountain Golf Course is calculated as the total annual irrigation volume less all other metered usage. Table 4-5 lists the sites currently serviced with reclaimed water irrigation and their total irrigated area.



LOCATION	AREA (M ³)
Fairview Mountain Golf Course	450,000
Cemetery	23,000
103rd Street Linear Park	8,000
Airport	126,000
Public Works Yard	6,000
Alonso2	10,000
Huggins2	37,000
Secondary School	7,000
Total	667,000

TABLE 4-5: TOWN OF OLIVER IRRIGATION AREAS

4.2 Equalization Basin

Cell 1 has a total storage volume of 1,100 m³ and was designed to include equalization storage (15% of average daily flow) and emergency storage (12 hours or 50% of average daily flow). A residence time of 0.67 days is used for storage capacity projections. This measurement is derived using a maximum storage period of 16 hours, as per peak electricity rate hours during the shoulder season (i.e. Mar.-Jun., Sept. and Oct.).

Cell 2 was constructed northeast of the existing equalization basin and provides operational storage of 2,300 m³. A residence time of 0.67 days was again assumed for capacity projections. An overview of the equalization basin Cell 2 system expansion design and pre-design brief can be found in Appendix B. The total available storage of the two equalization basins, as well as the 900 m³ of emergency storage described in Section 2.2.2, is summarized in Table 4-6.

STORAGE AREA	TOTAL STORAGE VOLUME (M ³)
Equalization Cell 1	1,100
Equalization Cell 2	2,300
Emergency Storage (in original treatment plant location)	900
Total Capacity	4,300 m³
Total Capacity excl. Emergency Storage	3,400 m³

TABLE 4-6: EQUALIZATION BASIN STORAGE CAPACITY
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The total design capacity of the two equalization basins is 3,400 m³, excluding emergency storage. Table 4-7 forecasts storage requirements for operation using a 0.67 day residence time. Under this operational design, capacity is estimated to be reached in 2090. This projection assumes a 1.3 factor of safety, 1% population growth, 0.38 m³/capita*day generation rate and 16-hour storage period. This capacity projection defines the point at which the system will no longer be able to store effluent to pump during off-peak hours.



YEAR	Population (1% Growth Rate)	FLOW (M³/D)	Storage Required (M ³)
2017	4,977	1,888	1,636
2018	5,027	1,907	1,653
2019	5,077	1,926	1,669
2020	5,128	1,945	1,686
2025	5,389	2,045	1,772
2030	5,664	2,149	1,863
2035	5,953	2,259	1,958
2040	6,257	2,374	2,058
2045	6,576	2,496	2,163
2050	6,912	2,623	2,273
2055	7,264	2,757	2,389
2060	7,635	2,898	2,512
2065	8,024	3,046	2,640
2070	8,433	3,201	2,775
2075	8,864	3,365	2,916
2080	9,316	3,537	3,065
2085	9,791	3,717	3,222
2090	10,290	3,907	3,386
2091	10,393	3,946	3,420

TABLE 4-7: EQUALIZATION BASIN STORAGE CAPACITY PROJECTION

4.3 High Lift Station

The SCADA system records the pump hours and number of starts at the High Lift Station, as well as the total daily flow using a flow totalizer. Based on this data, the operating capacity of the High Lift Station is approximately 30 L/s per pump. The Lift Station contains three pumps, one of which is reserved as a stand-by unit, meaning that the design capacity of the Lift Station is approximately 40 L/s (3,450 m³/day).

As influent is stored in the equalization basins such that pumping can be done in off-peak hours, the capacity assessment of the High Lift Station is subject to average influent flows, rather than peak daily flows. Based on Table 4-7 above, the High Lift Station configuration is anticipated to meet the average daily flow pumping requirements until 2077, well past the long term design horizon (≥ 20 years).

4.4 Treatment

The two aerated lagoons in service have a combined capacity of approximately 75,800 m³ and an operating depth of 5.3 m. Aeration is achieved through a submerged bottom fixed fine bubble diffuser system. A design summary was completed by TRUE in 2018 (see Appendix A) to establish the approximate timeline for construction of aerated lagoon No.1. Under existing



conditions with lagoons fully de-sludged, it was determined that effluent BOD will exceed permitted concentrations in 2077, with a population of 9,080 people at 1% annual growth rate.

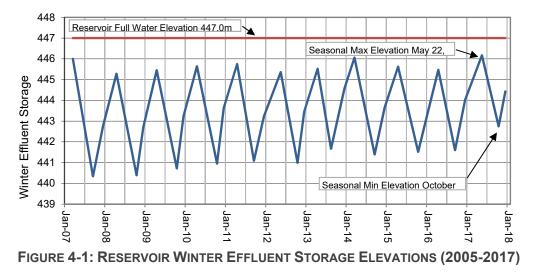
Under existing conditions where lagoons are not de-sludged, effluent BOD will exceed permitted concentrations in 2040, with a population of approximately 6,300 people. Under these assumptions, it is not anticipated that construction of the future aerated lagoon No. 1 will be required until 2040. This timeline will be dependent upon sludge accumulation, future desludging efforts and actual population growth rates.

A preliminary design for aerated lagoon No. 1 was completed by TRUE to determine the future Right of Way (ROW) area requirements for construction. In February 2017, a crown land tenure application was submitted to the Ministry of Forests, Lands, and Natural Resource Operations and Rural Development (FLNRORD) to obtain crown land necessary for the construction of aerated lagoon No.1. FLNRORD indicated the crown land tenure ROW necessary for the future construction of the lagoon could be incorporated into the Oliver Mountain assessment.

4.5 Winter Effluent Storage

The storage reservoir water elevation fluctuates between 439.00 m and 447.00 m, between which the total storage provided is estimated to be approximately 470,000 m³. The lower elevation limit was generated based on a 60-day effluent residence time prior to discharge for irrigation.

The service capacity of the storage reservoir is dependent on climatic conditions both in the preceding irrigation season and the spring following the storage period. Construction of the infiltration basin in 2014 now assists the Town in addressing climatic variability. Winter storage requirements are derived from volume and flow data. A summary of winter effluent storage volumes from 2007-2017 is provided in Figure 4-1.





A per capita storage requirement of 47 m³/capita was averaged from 2003 to 2017. A multiplication factor of 1.2 was added to allow for a conservative estimate of future requirements. A 21 m³/capita contribution provision was applied to meet the 60-day minimum retention time (as stated in the OC for PE 13717). This equates to a total requirement of 77 m³/capita.

Measured storage requirements to date and projected requirements are presented in Table 4-8. Based on the above assumptions, the reservoir is anticipated to reach its design capacity in 2037 without any upgrades to the system or expansion of the reclaimed water irrigation area.

Year	POPULATION (1% GROWTH)	Volume (m³)
2018	5027	387,083
2019	5077	390,954
2020	5128	394,863
2021	5179	398,812
2022	5231	402,800
2023	5283	406,828
2024	5336	410,896
2025	5390	415,005
2026	5444	419,155
2027	5498	423,347
2028	5553	427,581
2029	5609	431,856
2030	5665	436,175
2031	5721	440,537
2032	5778	444,942
2033	5836	449,391
2034	5895	453,885
2035	5954	458,424
2036	6013	463,008
2037	6073	467,639

 TABLE 4-8: RESERVOIR WINTER STORAGE REQUIREMENTS

4.6 Reclaimed Water Irrigation

There are five reclaimed water supply mains: the original two to Fairview Golf Course and the old forcemain to the Public Works Yard were built in 1983. The other three mains were built in 2004. It is recommended that Town Operations maintain a record of leaks, repairs, or operational concerns on the original supply mains to ensure their condition is being monitored.

An irrigation area expansion plan was submitted to the MOE in December 2018. Following submission of the 2019 Liquid Waste Management Plan Update and Sanitary Sewer Annual Report, the MOE will proceed with an amendment of the Town's OC to be consistent with current reclaimed water irrigation areas.



5.0 Collection Network Hydraulic Model Results

The following sections summarizes the development, methodology, and results of the hydraulic model of the gravity collection network.

5.1 Wastewater Flows

5.1.1 Diurnal Curve

Historical SCADA data is available from the Town of Oliver for pump hours and number of starts at each Lift Station. Unfortunately, there are no flow meters throughout the collection network until the screening station which only recently began storing data in December 2018. In order to convert the pump hours to flow rate, a system curve analysis was conducted with pump specifications provided by Town staff.

Data from 2015-2018 was analyzed to determine the actual sub-daily flows for use in the hydraulic model. The selected diurnal curve is shown in Figure 5-1 for the Influent LS, which represents the Town's entire catchment. In 2016 and 2017, there was a distinct increase in flows between dry weather and freshet conditions at the Influent LS and MacPherson LS likely due to their catchments' proximity to the Okanagan River. The increased level of the Okanagan River follows a similar trend year-to-year compared to the increase in sewage flows in the spring. Therefore, Figure 5-1 shows diurnal curves for dry weather and freshet conditions.

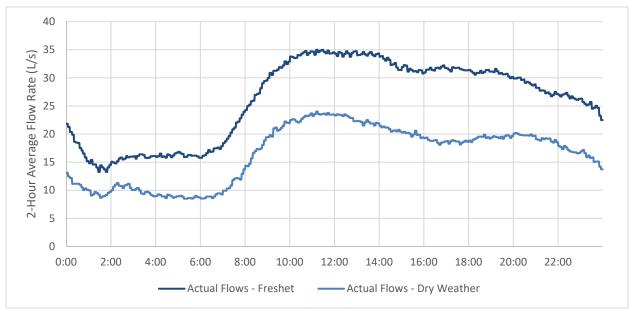


FIGURE 5-1: INFLUENT LIFT STATION DIURNAL CURVES – DRY WEATHER AND FRESHET

The average daily flow at the Influent LS has been determined as 17.5 L/s in the dry season, and 26.2 L/s during freshet. These values are consistent with the treatment facility's average annual flow of 21.9 L/s in 2017. During freshet, the Influent LS experienced 9.7 L/s of additional peak flow; while the McPherson LS experienced 1.1 L/s of additional peak flow.

5.1.2 Rain Event I&I

SCADA data was analyzed for possible Inflow and Infiltration (I&I) on all peak rain event days from 2015 to present. Peak rain events were determined using Osoyoos' daily precipitation data, which was checked against the Town of Oliver's daily recorded rainfall. This I&I analysis found no pattern of increased flows during peak rain events until two events in March 2018, in which the Influent LS experienced 16.7 L/s in additional peak flow.

This sudden change is I&I response may be the result of construction sites draining excess surface water into the sanitary system, which has been a concern for the Town in recent years. For the purpose of this analysis, a constant I&I design criteria of 8000 L/Ha/Day has been assigned.

5.1.3 Land-Use Generation Rates

Using the equivalent population from the OCP land use described in Section 3.3 and an equivalent per capita flow rate in the dry season and during freshet, a generation rate was assigned to each OCP parcel under existing and future conditions. Table 5-1 below shows the estimated amount of flow that is contributed from each land use category. Under both existing and future conditions, the primary contributors are Industrial, Institutional, and Low Density Residential.

OCP LAND USE	EXISTING – AVERAGE FLOW RATE (L/S)	FUTURE – AVERAGE FLOW RATE (L/S)
AGRICULTURAL	0.0	0.0
COMMERCIAL HWY	1.1	2.5
COMMERCIAL TOURIST	0.6	0.6
HIGH DENSITY RESIDENTIAL	1.8	3.2
INDUSTRIAL	3.7	3.7
INSTITUTIONAL	3.7	3.7
LOW DENSITY RESIDENTIAL	3.4	3.5
MEDIUM DENSITY RESIDENTIAL	2.2	3.1
OTHER LOTS	0.0	0.0
TOWN CENTRE	1.0	1.1
Total	17.5	21.3

TABLE 5-1: GENERATION BASELINE FLOWS BY OCP LAND USE



5.1.4 Lift Stations & Force Mains

Through the pump curve analysis, the operating point of each pump was calculated and presented in Table 5-2. As mentioned, each lift station is designed with a stand-by pump such that the design capacity of each station assumes that one pump is offline.

LIFT STATION	# OF PUMPS	PUMP OPERATING POINT (L/S)	LIFT STATION DESIGN CAPACITY (L/S)
Influent Lift Station	3	35	70
McPherson	2	18.5	18.5
Rockcliffe	2	5.8	5.8
Rotary Beach	2	14.9	14.9
Sawmill Road	2	25.5	25.5
Scott Road	2	15	15

 TABLE 5-2: LIFT STATION ESTIMATED OPERATING POINTS AND AVERAGE DAILY FLOWS

5.2 Model Development

A hydraulic model was developed using the latest version of PCSWMM in order to model all sanitary sewers and lift stations up to the Influent LS. The base data for the sanitary network was sourced from TRUE's GIS data of the Town's sanitary system. This GIS data included some general attributes (diameter, length, direction) of each conduit, but did not include any elevation data.

Manhole surface elevations were provided by Town staff from a survey conducted in 2018. The locations of surveyed manholes were compared to the GIS data and analyzed for data gaps. Invert elevations and other data gaps were first filled with information from record drawings as available; attributes such as diameter and direction of flow were also confirmed through record drawings. In the absence of record information, values were assumed based on surrounding information (e.g. inverts were interpolated based on available inverts nearby). All changes to the data set were tracked and coded so that staff could review and potentially update the base GIS data set.

Average daily flows were developed for all scenarios based on parcel area, generation rate, population densities and equivalent populations as detailed previously. The flows were spatially distributed through the model utilizing the spatial proximity of a parcel to the sanitary network. The model calculates the peak flow for each pipe segment by applying the diurnal curve to the average daily flow, routing the flows through the system, and applying a constant inflow for I&I and freshet flows.



5.3 Model Results

The model results have been summarized in Table 5-3 under the following four flow conditions:

CONDITIONS	Season	RAIN EVENT I&I (L/HA/DAY)	AVERAGE DAILY FLOW (L/s)	PEAK FLOW (L/S)	Total Daily Volume (m ³)
Existing	Dry Weather	N/A	17.4	23.8	1,510
Existing	Freshet	8,000	37.5	66.5	3,240
Future	Dry Weather	N/A	21.3	29.6	1,840
Future	Freshet	8,000	41.2	71.0	3,560

TABLE 5-3: COLLECTION NETWORK HYDRAULIC MODEL SCENARIOS

5.3.1 Existing Conditions

The total daily flow under existing dry weather conditions reported in the model is 1,510 m³/day, with an average daily flow of 17.4 L/s and a peak daily flow of 23.8 L/s. Existing flows were also modelled in a wet weather scenario with a baseline I&I from freshet and I&I from a rain event during peak hours; the resulting total daily flow was 3,240 m³/day, with an average daily flow of 37.5 L/s and a peak daily flow of 66.5 L/s. Figure 5-2 below shows the modelled sub-daily data for inflow to the Influent LS under these existing conditions, overlaid with the actual diurnal curves for the Influent LS.

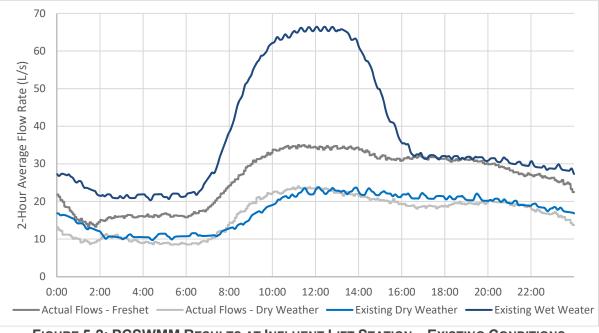
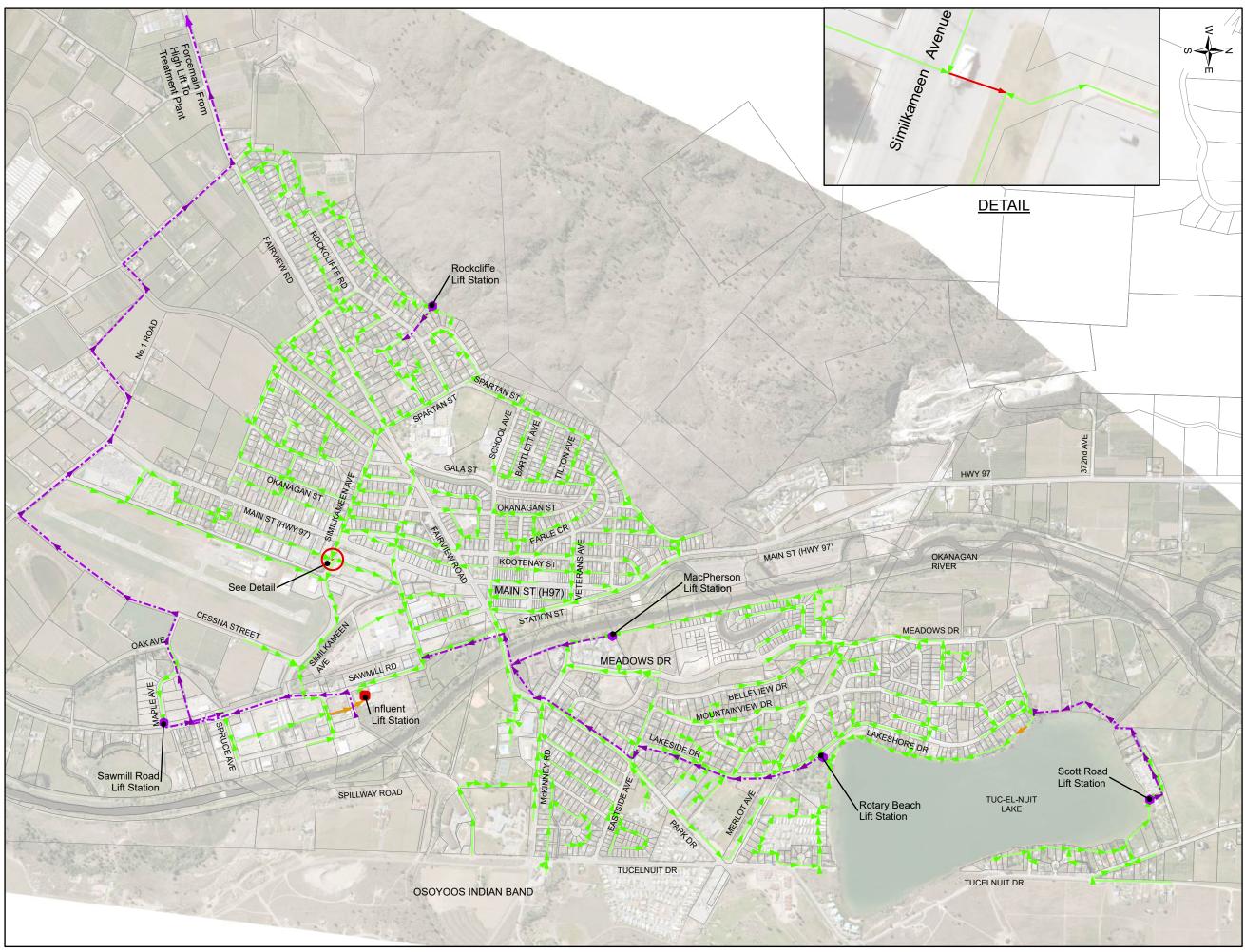


FIGURE 5-2: PCSWMM RESULTS AT INFLUENT LIFT STATION – EXISTING CONDITIONS





R:\Clients\300-399\306\306-1751\03 Drawings\GIS\Maps\306-1751-003 Fig Existing and Future Wet Conditions.mxd



Model Results-Existing and Future Wet Weather Conditions

Legend

--- Forcemains

Lift Stations

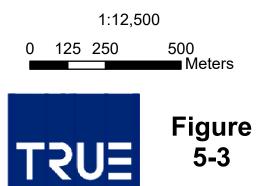
Influent Lift Station

Sanitary Mains Max Flow / Full Flow

→ < 0.50

→ > 0.66

Property Cadastre



During dry weather flows, there is no apparent surcharging of manholes or pipe, flooding, or pipe flowing above 2/3 of full flow. During wet weather conditions, there is one section of pipe operating above 2/3 of full flow, five sections above 1/2 of full flow, and no flooding or surcharging of manholes. Table 5-4 and Figure 5-3 (previous) summarize the pipe sections above 1/2 and 2/3 of full flow.

ID	Inlet Node	Outlet Node	D IAM (MM)	Slope (%)	Length (M)	MAX/FULL FLOW RATIO	Max Depth/ Diameter Ratio
C2	D-178	D-177	0.2	0. 2	8.5	1.09	0.58
C712	T-696	T-697	0.3	0.1	45.1	0.61	0.39
C12	D-152	D-101	0.25	0.6	17.6	0.57	0.57
C376	D-153	D-152	0.25	0.6	48.2	0.55	0.54
C377	D-155	D-154	0.25	0.6	11.5	0.55	0.53
C81	D-154	D-153	0.25	0.6	76.2	0.55	0.53

TARLE C A. DOOMMAN DEALS TO			
TABLE 5-4: PC5WWWW RESULTS -	- EXISTING CONDITIONS	- GRAVITY PIPE ABOVE 1/2 FULL FL	OW

5.3.2 Future Conditions

The same dry weather and wet weather conditions were modelled for future generated flows for a 20-year design horizon. The total daily flow under future dry weather conditions reported in the model is 1,840 m³/day, with an average daily flow of 21.3 L/s and a peak daily flow of 29.6 L/s. Existing flows were also modelled in a wet weather scenario with a baseline I&I from freshet and I&I from a rain event during peak hours; the resulting total daily flow was 3,560 m³/day, with an average daily flow of 341.2 L/s and a peak daily flow of 71.0 L/s. Figure 5-4 below shows the modelled sub-daily data for inflow to the Influent LS under these future conditions, overlaid with the actual diurnal curves for the Influent LS.

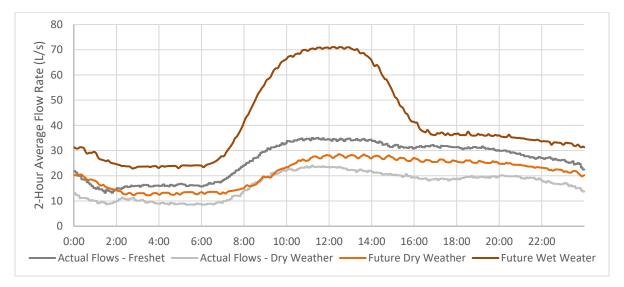


FIGURE 5-4: PCSWMM RESULTS AT INFLUENT LIFT STATION - FUTURE CONDITIONS

28

The results under future conditions are comparable to existing conditions: there is no surcharging or flooding of nodes, and the same sections of pipe operating above 1/2 and 2/3 of full flow under wet weather conditions.

5.3.3 Lift Station Performance

Table 5-5 below shows the peak inflows to each lift station under the maximum flow conditions (future wet weather), the operating capacity of each station based on the system curve analysis, and the surplus or deficit of capacity at peak flow.

LIFT STATION	LIFT STATION DESIGN CAPACITY (L/S)	Peak Inflow (L/s)	SURPLUS (+) / DEFICIT (-) IN CAPACITY (L/S)
Influent Lift Station	70	71.0	-1.0
McPherson	18.5	8.1	10.4
Rockcliffe	5.8	5.3	0.5
Rotary Beach	14.9	15.5	-0.6
Sawmill Road	25.5	1.1	24.4
Scott Road	15	1.8	13.1

TABLE 5-5: PCSWMM RESULTS - FUTURE WET WEATHER CONDITIONS - LIFT STATION CAPACITIES

Although Rotary Beach LS's capacity is exceeded in the model, Figure 5-5 below shows that the pump is able to continue pumping down the water level in the Lift Station at a slower rate. The Influent LS also has a deficit in capacity from peak flow and may not be capable of keeping up with the additional peaks in flow caused by the other lift stations.

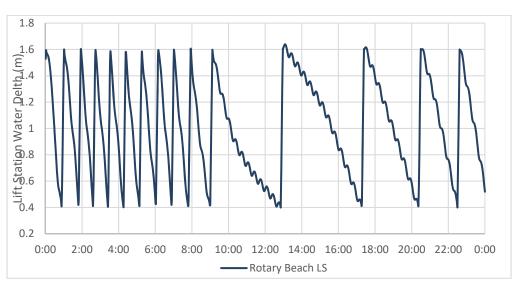


FIGURE 5-5: PCSWMM RESULTS – ROTARY BEACH LIFT STATION DEPTH



5.4 Asset Management

5.4.1 Collection Network

Developing a hydraulic model for the Town's sanitary collection network involved a systematic and in-depth review of the Town's sanitary manholes and linear assets. The data set has been improved based on the best available information and should be adopted as the Town's base data set to be maintained and improved upon over time.

The Town currently manages approximately 41.5 km of sanitary collection infrastructure including Polyvinyl Chloride (PVC), Vitrified Clay Tile (VCT), and Asbestos Cement (AC) pipe. Figure 5-6 provides a summary of the material types while Figure 5-7 provides and overview of materials for pipe segments in the system.

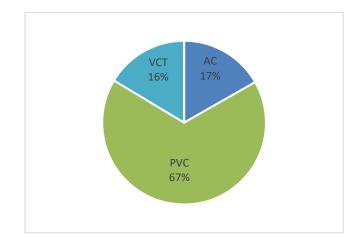


FIGURE 5-6: COLLECTION NETWORK PIPE MATERIAL PIE CHART

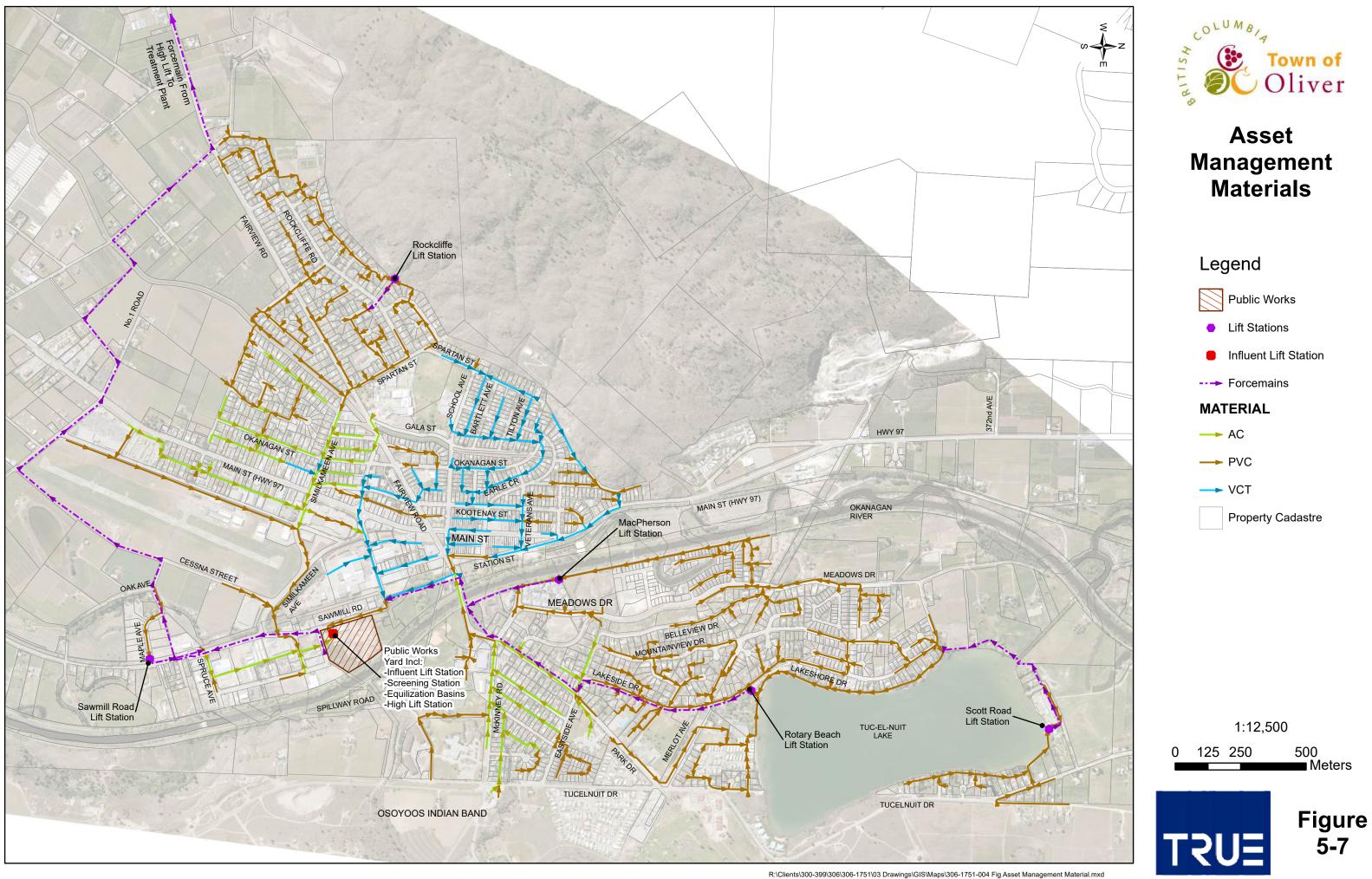
The outputs of a hydraulic model allow performance of the system to be incorporated into decision making for capital projects and assists with the prioritization of replacement projects. A simple risk model was developed to identify and prioritize replacement projects. The risk equation is:

Risk = Probability x Criticality

Probability was determined based on condition (if available) and remaining useful life which is a function of material and installation year. Condition inspections were conducted on many of the older VCT and AC pipes in 2016 and 2017. Criticality is based on size of pipe, contributing serviced area, and the max/full flow ratio from the model. In addition to compliance with the Sewerage System Regulation of BC, the Town of Oliver Subdivision and Development Servicing Standards outlines design standards for the sanitary sewer system including the maximum to full flow ratio is not to exceed 2/3 for pipe over 200 mm in diameter.

Once the risk score was determined, the assets were classified into high, medium, and low categories. Table 5-6 provides a breakdown of the risk categories.









CATEGORY	Length (m)	PERCENTAGE OF COLLECTION NETWORK
High	3,800	9%
Medium	4,700	11%
Low	33,000	80%

TABLE 5-6: COLLECTION NETWORK - SUMMARY OF RISK SCORES

The dividing line between categories is rather arbitrary and was set based on experience with other municipalities. Figure 5-8 breaks out the risk categories by pipe material.

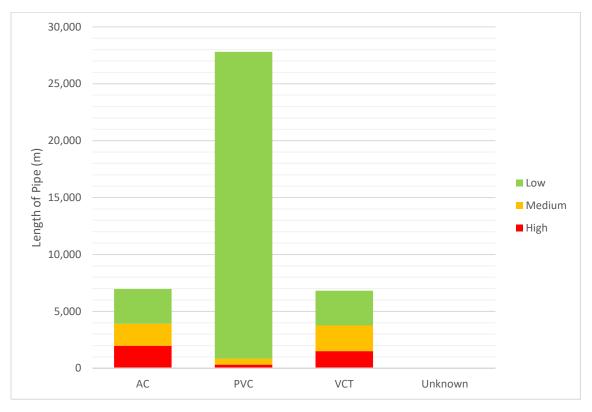


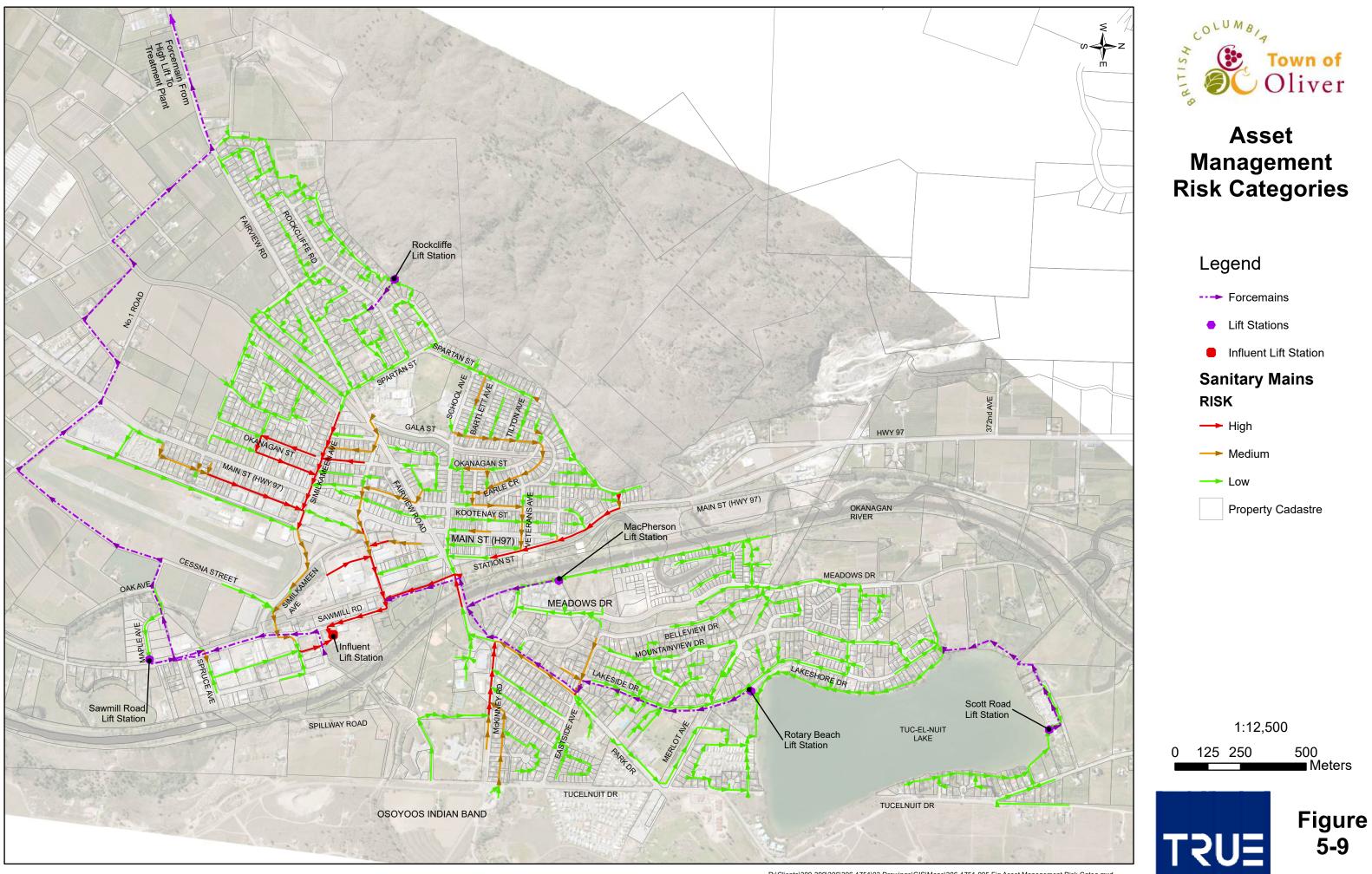
FIGURE 5-8: RISK SCORES BY PIPE MATERIAL

The AC and VCT pipe are largely classified as high and medium-risk due their age and estimated remaining useful life. However, the condition inspections from 2016 and 2017 show that some of the AC and VCT pipe is in good condition. PVC pipes are generally newer assets in the system and are classified as low risk. However, there are some segments of PVC near the Influent LS which have been flagged as high and medium risk due to their size and large contributing area. Figure 5-9 highlights the risk categories throughout the collection network.

5.4.2 Lift Stations & Forcemains

The Town keeps a record of lift station pump models and installation years as shown below in Table 5-7. Based on a 20-year useful life, three pumps should be assessed for replacement.





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LIFT STATION	Asset	MANUFACTURER	Model #	Install Year	Useful Life	USEFUL LIFE Remaining	ANTICIPATED REPLACEMENT YEAR
Dotom/ Booob	Pump 1	Flygt	3153.185	2018	20	19	2038
Rotary Beach	Pump 2	Flygt	3152.181	1993	20	-6	2013
Deelveliffe	Pump 1	Flygt	3127.180	1994	20	-5	2014
Rockcliffe	Pump 2	Flygt	3127.180	1994	20	-5	2014
Scott Road	Pump 1	Flygt	3127.181	2010	20	11	2030
Scoll Road	Pump 2	Flygt	3127.181	2010	20	11	2030
	Pump 1	Flygt	3085.183	2014	20	15	2034
Sawmill Road	Pump 2	Flygt	3085.183	2014	20	15	2034
MaaDharran	Pump 1	Flygt	3127.181HT	2013	20	14	2033
MacPherson	Pump 2	Flygt	3127.160	2017	20	18	2037
	Pump 1	Flygt	3127.181	2013	20	14	2033
Influent Lift	Pump 2	Flygt	3127.181	2012	20	13	2032
	Pump 3	Flygt	3127.160	2015	20	16	2035

TABLE 5-7: ASSET MANAGEMENT - LIFT STATION PUMPS

The forcemain asset information is summarized in Table 5-8 below. The forcemains were installed in the 1980s and 1990s using PVC.

Forcemains	Length (M)	MATERIAL	Diameter (MM)	Install Year	Useful Life	USEFUL LIFE REMAINING	ANTICIPATED REPLACEMENT YEAR
MacPherson Lift Station to 350th Ave Bridge	373	PVC	150	1983	80	44	2063
Junction by 350th Ave. Bridge to MH D-104	418	PVC	200	1983	80	44	2063
Rotary Beach Lift Station to 350th Ave Bridge	1298	PVC	150/250	1982	80	43	2062
Rockcliffe Lift Station to MH D-232	158	PVC	100	1994	80	55	2074
Scott Road Lift Station to MH T-751	720	PVC	150	1993	80	54	2073

6.0 System Upgrades

Based on these capacity assessments, a list of system upgrades has been developed for the collection network, lift stations, and treatment system. For the collection network, these projects are primarily based on available asset information; The first step in all recommended system upgrades is to verify the GIS information and determine the actual condition of these assets in order to avoid premature replacement. Alternatively, the Town may choose to undertake any of these projects outright based on its criticality to the system as risk of continued degradation may not be acceptable to the Town.

6.1 Collection Network

As discussed in Section 5.4, the risk model identified approximately 4 km of sanitary piping as high risk and therefore due for replacement or rehabilitation. The risk model is a prioritization tool to indicate which assets should be considered or investigated first.

The following list of projects has been developed assuming that all assets in the high-risk category need replacement or rehabilitation. These preliminary cost estimates will assist the Town in incorporating projects into their capital planning. Following further investigation into the high-risk assets, the Town may wish to reprioritize these projects if specific assets are found to be in satisfactory condition or the GIS information was incorrect.

ID	PROJECT	EST. CAPITAL COST	EST. DCC ELIGIBILITY
S1	Fairview to Sawmill Road	\$425,000	75%
S2	Main & Station Street (Hillside to Bank Ave)	\$583,000	69%
S3	Similkameen Avenue (Tulameen to Airport)	\$601,000	32%
S4	Okanagan Street at Similkameen	\$564,000	0%
S5	Airport Street Alley (Skagit to Similkameen)	\$313,000	0%
S6	McKinney Road (Coyote to Park)	\$117,000	0%
S7	River Crossing at Fairview Road	\$239,000	56%
S8	Co-op Road (Main to Sawmill)	\$339,000	0%
S9	Fir Avenue to Influent Lift Station	\$181,000	56%
	Total	\$3,362,000	

TABLE 6-1: SANITARY COLLECTION NETWORK - SYSTEM UPGRADES

A reasonable goal would be to replace or rehabilitate the high-risk assets within 10 years which equates to approximately 400 m of replacement each year. This replacement program covers approximately 10% of the sanitary collection network in the next 10 years. At this rate, the Town would replace the entire sanitary collection network in 100 years which exceeds the typical useful life of system components (approximately 80 years for PVC). Therefore, this program is just a



start, and development of a long term replacement program will be vital to sustainably manage the sanitary collection network.

Project sheets containing additional information and detailed cost estimates for each project can be found in Appendix C.

6.2 Lift Stations

Pump Replacement – Rockcliffe Lift Station

Both pumps at the Rockcliffe LS are beyond their estimated useful life and should be assessed for replacement. Based on the results of the capacity assessment, replacing the pumps with new models of similar capacity will be adequate for future demand.

Capacity Assessment & Pump Replacement – Rotary Beach Lift Station

One pump at Rotary Beach LS is beyond its estimated useful life and should be assessed for replacement. While the collection network capacity assessment showed that Rotary Beach LS is nearing its capacity during peak I&I conditions, it is recommended to conduct a capacity assessment of the lift station to confirm the operating capacity. There are two forcemains available for the Rotary Beach LS to pump and Town staff believe that the station is currently pumping to the smaller of the two forcemains. Part of a capacity assessment of the LS would be to confirm which of the two historical forcemains is currently being used and determine options to increase capacity at the station. This will ensure that the replacement pump is adequate for future and peak I&I demand.

6.3 Treatment System

The service capacity of each component of the wastewater treatment system is a function of the useful life of the asset and the population which it can serve. The Town prepared a Wastewater Treatment Systems Capacity Improvement Design Brief in January 2019 to outline proposed upgrading works (see Appendix D). The recommendations are based on addressing deficiencies to the existing aerated lagoon treatment system, which is the only component of the treatment system forecasted to require upgrading within the next 15-years. The upgrades listed below have a combined capital cost estimate for \$4,645,000. The detailed cost estimate can be found in Appendix D.

Middle Berm Stabilization

This project will involve stabilizing the saturated middle berm of aerated lagoons Cell No. 2 and 3. To rectify this issue, it is proposed to install two lock block walls along the length of this berm. These walls would be tied to each other with geogrid to provide stability and infilled. A secondary



benefit of this berm stabilization would be that the existing lagoon capacity would increase due to the installation of a wall structure in place of the existing 3:1 lagoon slopes.

Aeration System Upgrades

Upgrades to the aeration system would include desludging of Cell No. 2, installation of a new aeration header and lateral pipes to each lagoon, provision for a new aeration system diffuser and installation of a new blower to the existing blower building. The new blower would act as the duty blower for the aeration system.

Installation of a 50 kW Photovoltaic System

It is proposed to utilize the aerated lagoon site as a location for renewable energy production as a means to offset emissions produced by the Town of Oliver. The Photovoltaic (PV) power will be connected to the system by means of a "grid-tie" inverter and metered by FortisBC under their net metering program.

7.0 Other Recommendations

In addition to the system upgrades summarized in Section 6, there are a number of additional areas of interest or concern which the Town may wish to investigate:

Electrical Systems Review

Aside from regular maintenance, the electrical systems in the lift stations and treatment system have not been upgraded since installation in the 1980s and 1990s. It is recommended that the Town review their electrical systems and determine if upgrades are required to maintain safe and reliable operations and meet future demand. Upgrades have already been identified by Town Operations staff to increase electrical service to 600V at the Scott Road and Rockcliffe Lift Stations.

Inflow & Infiltration

In order to further investigate the suspected I&I events in 2017 and 2018, the Town may wish to install portable flow monitors throughout the collection network to narrow down the problem areas. As part of the investigation into I&I, it is important to have accurate sub-daily precipitation data in order to identify a direct correlation between rainfall and increased flow. Therefore, it is recommended that the Town install a rain gauge and data collection system which would allow them to track sub-daily precipitation.

Winter Storage Options Assessment

Based on the capacity assessment of the treatment system, winter effluent storage will be the first limiting component in future development. Capacity of the current storage reservoir is estimated to be reached by 2037. It is recommended that the Town undertake an options assessment to begin long term planning to upgrade this facility.

SCADA System Review

A detailed review of the SCADA system is recommended to ensure that the Town is recording all necessary data in the correct format and timestep and identify any gaps in the data collection system. This review may result in recommendations to change, update, or add to the existing data collection systems.



APPENDIX A

Aerated Lagoon No. 1 – Design Summary



Internal Memorandum

То:	TRUE Staff	From:	Sean Curry, P. Eng.
Attn:	Staff on Oliver LWMP Update		
Date:	December 5, 2018	File No:	306-985

RE: Aerated Lagoon No. 1 – Design Summary

This memo is written to provide a summary of preliminary design considerations relating to the future construction of Aerated Lagoon No. 1 at the Town's wastewater treatment facility in the Fairview area.

Design considerations for this lagoon are based off of the Town's LWMP Update dated January 2002 (TRUE project number 306-083). In this report, the future Aerated Lagoon No. 1 design considerations were specified as follows:

- Capacity minimum 20,000 m³
- Interior slopes 3:1
- Exterior slopes 2:1
- Liquid depth 5.25m
- Top of water level 448.30m (match existing lagoons see drawing 306-291) topographic survey indicates that Aerated Lagoon No. 2 has a liquid elevation of 448.35m
- Bottom of water level 443.00m (match existing lagoons see drawing 306-291)
- Top of berm 449.30m (i.e. 1.0m of freeboard)

In February 2017, a crown land tenure application was submitted to the Ministry of Forests, Lands, and Natural Resource Operations (MFLNRO) to obtain crown land necessary for the construction of Aerated Lagoon No. 1. This work was done in conjunction with another crown land tenure application submitted on behalf of the Town. Upon receipt, MFLNRO staff informed the author that an assessment relating to recreation and environmental protection of the Oliver Mountain area was currently being undertaken. Therefore, MFLNRO staff indicated that the required crown land tenure right-of-way necessary for the future construction of this lagoon should be incorporated into the Oliver Mountain assessment. Preliminary design for this lagoon was therefore authorized by Town staff to determine a required right-of-way area for construction of the future lagoon. This preliminary design is illustrated on the enclosed drawing 306-985-Fig 1.

It is important to note that the Town has no current plans for construction of the future Aerated Lagoon No. 1. The crown land tenure application process was started to ensure that land would be available when expansion of the wastewater treatment facility was deemed necessary. The 2002 LWMP Update indicated that construction of Aerated Lagoon No. 1 would provide service

201-2079 Falcon Road ■ Kamloops BC ■ V2C 4J2 ■ www.true.bc.ca ■ tel 250.828.0881 ■ fax 250.828.0717

capacity for a population equivalent of about 11,000 persons while the existing system (i.e. 2 aerated lagoons in service with a combined capacity of about 75,800 m³) had a capacity for a service population of about 7,000 persons. The 2016 census population for the Town of Oliver was found to be 4,928 persons. Clearly, the existing system is adequate for the Town's current service population.

Based on the above, it is also important to provide an opinion on when the treatment objectives relating to the existing treatment system will exceed permitted maximum levels of 45 mg/L BOD and 60 mg/L of TSS. The following calculations are provided to indicate when these treatment objectives will be exceeded based on existing conditions (i.e. lagoons are not desludged) and ideal conditions (i.e. lagoons are fully desludged). Note that winter conditions govern and the Town's 2016 Annual Report indicated that average flow for this system is about 1,753 m³/d.

Existing Design Conditions (i.e. lagoons are fully desludged)

- Volume: Lagoon 2 has capacity of 37,600 m³ while lagoon 3 has capacity of 38,200 m³ resulting in a total design capacity of 75,800 m³
- Detention time = 75,800 m³ divided by 1,753 m³/day = 43.2 days
- 2016 Oliver census population = 4,928 persons
- Theoretical BOD = 0.17 lb/capita or 0.077 kg/capita x 4,928 persons = 379 kg/day BOD in
- Influent BOD concentration = BOD in divided by flow = 379 kg/day divided by 1,753 m³/day = 0.216 kg/m³ x 1x10⁶ mg/kg divided by 1,000 L/m³ = 216 mg/L BOD in
- Theoretical reaction rate if wastewater temperature is assumed to be 5°C during winter conditions = 0.162 day⁻¹
- Removal efficiency = 1 / (1 + reaction rate x detention time) = 12.5% remaining
- Wastewater treatment system Effluent BOD = removal efficiency x BOD in = 12.5% x 216 mg/L = 27.0 mg/L BOD
- Use solver to determine when effluent BOD will exceed 45 mg/L during winter conditions: found to be in 2077 with a population equivalent of about 9,080 persons (assumes 1% growth rate consistent with LWMP Update dated October 2017 306-1751). Refer to R:\Clients\300-399\306\306-985\04 Design\Aerated Lagoon No 1\Calculations.xlsx

Existing Conditions (i.e. lagoons are not desludged)

- Volume: As of 2011, Lagoon 2 had a sludge accumulation of 5,000 m³ while lagoon 3 had a sludge accumulation of 5,000 m³. Sludge accumulation is based off a survey conducted by Lambourne Environmental Ltd. in December 2011. This report can be found in R:\Clients\300-399\306\306-985\02 Correspondence\Grant Applications\2016 Clean Water and Wastewater Fund\CWWF 2016-Application No. 68\E Relevant Studies and Reports\Oliver survey report 2011.pdf
- Projected sludge accumulation is based off annual sludge accumulation between 1996 and 2011.
- Detention time = about 65,000 m³ divided by 1,753 m³/day = 37.1 days for 2016 conditions
- 2016 Oliver census population = 4,928 persons

- Theoretical BOD = 0.17 lb/capita or 0.077 kg/capita x 4,928 persons = 379 kg/day BOD in
- Influent BOD concentration = BOD in divided by flow = 379 kg/day divided by 1,753 m³/day = 0.216 kg/m³ x 1x10⁶ mg/kg divided by 1,000 L/m³ = 216 mg/L BOD in
- Theoretical reaction rate if wastewater temperature is assumed to be 5°C during winter conditions = 0.162 day⁻¹
- Removal efficiency = 1 / (1 + reaction rate x detention time) = 14.3% remaining
- Wastewater treatment system Effluent BOD = removal efficiency x BOD in = 14.3% x 216 mg/L = 30.8 mg/L BOD
- Use solver to determine when effluent BOD will exceed 45 mg/L during winter conditions: found to be in 2040 with a population equivalent of about 6,300 persons (assumes 1% growth rate consistent with LWMP Update dated October 2017 306-1751). Refer to R:\Clients\300-399\306\306-985\04 Design\Aerated Lagoon No 1\Calculations.xlsx

Based on the above, it can be assumed that the existing system has adequate capacity for the existing service population. Also, construction of the future Aerated Lagoon No. 1 will not be necessary until between 2040 and 2077 (depending upon sludge accumulation and future desludging efforts). A recommendation moving forward should be to fully desludge these lagoons on a regular basis to ensure that adequate treatment capacity is maintained. Desludging will allow the Town to defer capacity upgrades in the future.

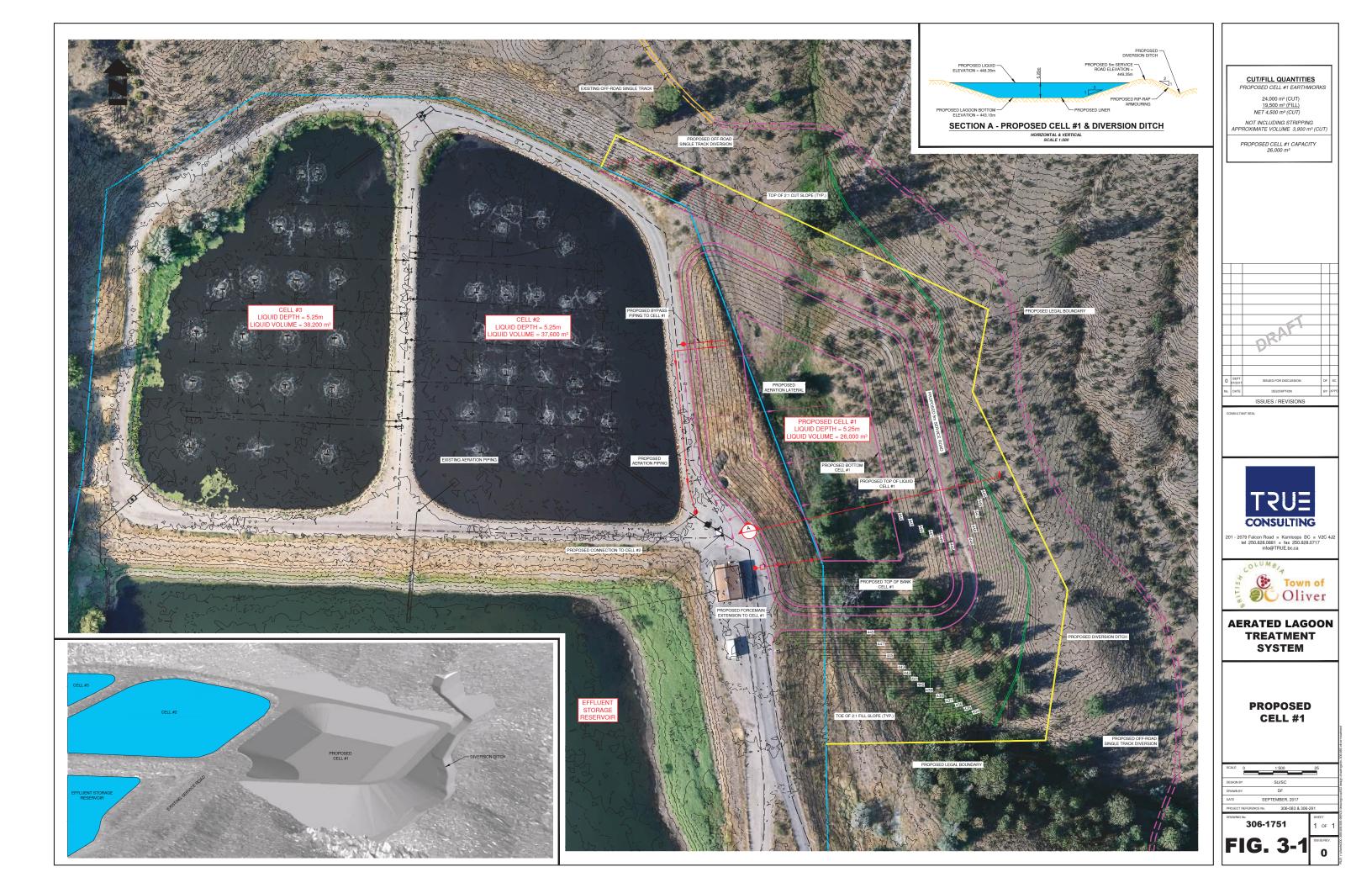
Regards,

Sean Curry, P. Eng.

SAC/slf

enclosures: hand calculations and drawing 306-985-Figure 1 showing the preliminary design and right-of-way requirements for the future Aerated Lagoon No. 1

R:\Clients\300-399\306\306-985\02 Correspondence\Outgoing\306-985-Internal Memo-Oliver Aerated Lagoon No 1 Calculations-2018-12-05.docx



APPENDIX B

Equalization Basin Expansion – Predesign Brief



Equalization Basin Expansion

Predesign Brief

Prepared by:



February 2007 Ref: 306-081

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1.1 <u>General Description – Town of Oliver Wastewater Treatment and Disposal</u> <u>Systems</u>

Up to 1985, the Town of Oliver discharged treated wastewater from a secondary modified activated sludge treatment plant to the Okanagan River. To achieve compliance with initiatives of the Provincial government to reduce phosphorus loadings to Okanagan Valley watercourses, the Town of Oliver constructed effluent storage and effluent irrigation systems in the Fairview area in 1985. *Figure 2* is an overall plan of the Town of Oliver wastewater treatment, storage and related facilities and includes areas where the Town uses reclaimed water for irrigation purposes. In 1995, the Town constructed an aerated lagoon treatment system adjacent to the winter effluent storage reservoir and at that point, abandoned the secondary treatment plant at the public works yard.

The terminus of the Town's sewage collection remains at the Public Works yard. Wastewater is pumped through a rotating screen, piped to an equalization basin from where it is pumped to the Fairview area.

1.2 <u>Waste Management Plan Update 2002</u>

In 2002 the Town of Oliver completed a major revision and update of its Waste Management Plan focusing on the identification of additional lands for irrigation with reclaimed water. This update of the Waste Management Plan assessed several directions for expansion of the Town's reclaimed water irrigation supply system and concluded that the preferred option was the construction of supply mains to make reclaimed water available for irrigation purposes at Town/Public lands including the Airport, Cemetery, Public Works Yard, South Okanagan Secondary School, etc.

Once the preferred direction for irrigation area expansion was identified, the Waste Management Plan then assessed supply alternatives. The options were:

-1-

construct new supply mains from the Fairview Area to the identified reclaimed water irrigation expansion areas.

or

construct a new forcemain from the Public Works Yard to the Fairview area and use the existing forcemain constructed in 1985 as the reclaimed water supply main.

A major advantage of a new forcemain option was the opportunity for the Town to take advantage of, at that time, proposed time of use energy cost incentives to be offered by the electrical utility. The new forcemain option was recommended as the preferred option and the forcemain was constructed in 2004. Reclaimed water for irrigation purposes has been used at the cemetery, airport and public works yard in 2005 and 2006 supplied through the original forcemain.

1.3 <u>Functional Description of the Existing Equalization Basin</u>

The Town's existing equalization basin at the Public Works yard is a lagoon type structure, lined with a hypalon membrane and has an operating capacity of about 1100 cubic meters. In the early 1980's, the electrical service in the South Okanagan was very unreliable with numerous short duration interruptions in electrical service occurring on a daily basis through the summer months. In 1985, a design decision was made to construct an equalization basin to store flows during a short duration power failure rather than provide standby power which at that time may have started and stopped numerous times on a daily basis through the summer months. Since the early 1980's the electrical utility has undertaken major improvements to the Oliver and electrical distribution system and short duration power failures are now infrequent.

Consistent with its Waste Management Plan, the Town of Oliver has modified the controls of high lift station pumps to assess the practicality of fully complying with time of use operational restrictions and thereby achieve significantly reduced costs for electrical energy. The equalization basin's primary functional use has therefore changed from a facility to be used during power interruptions to a storage facility to take advantage of energy cost incentives. On a trail basis, the Town has successfully operating its 3 - 100 HP high lift pumps on a time of use basis through 2005 and 2006. Energy cost savings realized by the Town are of the order of \$20,000 annually. The existing equalization basin is not of sufficient volume for the Town to continue to operate its high lift pumps on a time of use basis therefore the project proposal to construct a second equalization basin.

2.1 <u>Time of Use Energy Cost Incentives</u>

Time of use energy cost incentives are offered by Fortis Canada if the operation of the Town's high lift wastewater pump station can be limited to off peak periods. The off peak periods vary from summer to winter and are summarized as follows.

Winter - November, December, January, February

- > off peak Midnight to 7:00 AM 7 hours
- \blacktriangleright peak 7:00 AM to Noon 5 hours
- > off peak Noon to 4:00 PM 4 hours
- ▶ peak 4:00 PM to 10:00 PM 6 hours
- > off peak -10:00 PM to Midnight -2 hours

Winter Maximum Storage Period – 6 hours

Summer – July, August

- ▶ off peak Midnight to 10:00 AM 10 hours
- > peak -10:00 AM to 9:00 PM -11 hours
- > off peak -9:00 PM to Midnight -3 hours

Summer Maximum Storage Period – 11 hours

Shoulder Seasons - March, April, May, June , September, October

- > off peak Midnight to 6:00 AM 6 hours
- > peak 6:00 AM to 10:00 PM 16 hours
- > off peak -10:00 PM to Midnight -2 hours

Shoulder Season Maximum Storage Period – 16 hours

For the Town to take full advantage of the time of use energy incentives offered by Fortis, the design storage volume requirements to be provided in the equalization basins is determined by the shoulder season during which wastewater inflow has to be stored for a 16 hour period from 6:00 AM to 10:00 PM and pumped to the Town's treatment lagoon system over an 8 hour period from 10:00 PM to 6:00 AM.

2.2 Equalization Basin Sizing Criteria

Average daily sewage flows on a monthly basis measured at the Town's High Lift Station for the period 2003 to 2006 inclusive are presented in Table 2.1. The flow data illustrates some variation in average daily sewage flows between winter and summer with winter flows being about 93% of the annual average and summer flows being about 113% of the annual average. Higher flows during the summer months may be indicative of infiltration during freshet flows in the Okanagan River and tourism related summer period commercial uses.

Table 2.1

Town of Oliver Summary of Monthly Sewer Flows

]	2003		2004		2005		2006	
	High Lift Station							
	Total	Monthly	Total Monthly		Total Monthly		Total Monthly	
	Monthly	Average	Monthly	Average	Monthly	Average	Monthly	Average
	m3/day	m3/day	m3/day	m3/day	m3/day	m3/day	m3/day	m3/day
Jan	60226	1943	61225	1975	63969	2064	65959	2128
Feb	53430	1908	56546	1950	57824	2065	60239	2151
Mar	58878	1899	60063	1938	62488	2016	66581	2148
Apr	59758	1992	59838	1995	63396	2113	63534	2118
May	61955	1999	62370	2012	65867	2125	72354	2334
Jun	61281	2043	61728	2058	68081	2269	77483	2583
Jul	68917	2223	70059	2260	73239	2363	78623	2536
Aug	69251	2234	73069	2357	73976	2386	76326	2462
Sep	65661	2189	67545	2251	64542	2151	68481	2283
Oct	67753	2186	68490	2209	65567	2115	69071	2228
Nov	61983	2066	62127	2071	61595	2053	64857	2162
Dec	62047	2002	62988	2032	63403	2045	65905	2126
Total	751139		766048		783947		829413	
Average	2052		2093		2147		2272	

For determination of the equalization volume requirements to enable the Town to take full advantage of the Fortis time of use energy incentives, the June 2006 shoulder season average daily sewage flow of 2583 m³/day has been utilized. Equalization volume requirements are derived as follows:

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- > design shoulder season flow $-2583 \text{ m}^3 \text{day}$
- ➤ shoulder season storage period 16 hours
- → storage volume $16/24 \text{ x } 2583 \text{ m}^3 = 1722 \text{ m}^3$
- ➤ adjustment factor for flow variations 30%
- ➢ storage volume − 1722 x 130% 2238 m³

- \geq 2006 serviced population 4200
- > mid term horizon population as per the Waste Management Plan 6200
- > storage volume required to 6200 population horizon -3300 m^3

The existing equalization provides approximately 1100 m^3 of storage between normal low and high operating levels therefore the proposed expansion of the equalization basin has to provide a minimum of 2200 m³ of operating storage.

2.3 <u>Project Description</u>

Proposed equalization basin number 2 is illustrated conceptually on drawing 306-1121-SK1. Equalization basin 2 is proposed to be located northeast of the existing basin generally occupying a vacant portion of the Public Works yard site between the Okanagan River flood control dyke and the existing basin and an area formerly used for sludge drying beds. When the Town completed the aerated lagoons in the Fairview area in 1995, the activated sludge treatment plant on the Public Works site was removed from service and the drying beds ancillary to the treatment plant were no longer required.

Referring to drawing 306-1121-SK1, the proposed equalization basin and related works are briefly described as follows.

- the equalization basin is proposed as a lagoon type structure with a 60 mil HDPE membrane lining comparable to the existing basin. At the average operating level, the basin measures approximately 30 m x 50 m.
- the proposed basin will have a floor, top of berm and operating elevations the same as the existing basin. It is therefore assumed that the two basins will be operated together, i.e. inflow directed to each basin through the existing diversion structure and withdrawn simultaneously from each basin through the same diversion structure.
- inlet and outlet piping connecting to chambers in the existing diversion structure intended for future extensions to a second equalization basin.
- two surface aerator/mixers to provide circulation in the basin and thereby minimize stagnant conditions that may result in odor problems.

As illustrated in drawing 306-1121-SK1 all proposed works associated with equalization basin 2 are within the Town's Public Works Yard.

- 5 -

2.4 <u>Capital Cost Estimate</u>

A preliminary capital cost estimate for Equalization Basin 2 is presented in the tabulation follows.

Preliminary Capital Cost Estimate Equalization Cell No. 2

1.	Strip Site	4500m² @ \$2.00	\$9,000
2.	Excavation and Embankment	1000m ³ @ \$8.00	\$8,000
3.	Import Fill	4000m ³ @ \$15	\$60,000
4.	Sand Base for Liner	2800m² @ \$6.00	\$16,800
5.	60 Mil HDPE Liner	2800m² @ \$30	\$72,000
6.	Site Piping		
	6.1 Inlet Pipe	70 m @ \$200	\$14,000
	6.2 Outlet Pipe	40 m @ \$200	\$8,000
	6.3 Outlet Structure	allow	\$5,000
	6.4 375 Tee complete with Valves		\$16,000
	6.5 Modify Existing Diversion Structure		
	complete with Slide Gates		\$18,000
	6.6 Piping in Abandoned STP	allow	\$10,000
	6.7 Abandoned STP to Diversion Structure	100m @ \$250	\$25,000
7.	Mixers complete with Electrical	2 ea. @ \$35,000	\$70,000
8.	Remove and Replace Liner in Existing Basin	1600m² @ \$35	<u>\$56,000</u>
		Subtotal Construction	\$387,800
	Contingencies and E	ngineering (allow 25%)	<u>\$96,200</u>
		Total Project	\$484,000

APPENDIX C

Collection Network Upgrades – Project Sheets



Project: S1 - Fairview to Sawmill Road

Priority:	1	Type:	Replacement/Upgrade
Trigger:	Future Development	DCC:	75%

Location Map



Issue

This main is a very critical connection in the sanitary collection network, and services a corridor of future development. The 300 mm VCT pipe has surpassed its anticipated useful life.

Scope

Removal of approximately 315m of 300 mm VCT. Installation 315m of 600 mm PVC including reconnection of all existing services. New connections for future development are required.

DCC Justification

This project increases the capacity of the system for long term growth. DCC portion will be determined based on the change in cross sectional area of the upgrade:

DCC % =
$$1 - \frac{\left(\frac{\pi(D_1)^2}{4}\right)}{\left(\frac{\pi(D_2)^2}{4}\right)} = 1 - \left(\frac{D_1}{D_2}\right)^2 = 1 - \left(\frac{0.3}{0.6}\right)^2 = 75\%$$

Time Frame

1-3 years



ITEM NO.	DESCRIPTION	UNIT	EST. QUANT.	UNIT PRICE	TOTAL PRICE
S1	Fairview to Sawmill Road				
1.1	Materials 600Ø PVC Sanitary Main - Supply	~	245	¢700	¢220 500
	and Install Lined Concrete Manhole - Supply and Install	m ea	315 4	<u>\$700</u> \$8,000	\$220,500 \$32,000
1.2	Service Connections			·	
	Tie into existing	ea	2	\$5,000	\$10,000
	Reconnect existing services	ea	1	\$1,000	\$1,000
	Connect New Services	ea	2	\$2,000	\$4,000
1.3	Other Construction				
	Asphalt Restoration	m²	800	\$45	\$36,000
	Bare Land Restoration	m²	460	\$10	\$4,600
	Curb and Gutter	m	8	\$110	\$880
	Sidewalk	m	8	\$105	\$840
	Traffic Control	L.S.		\$5,000	\$5,000
				Subtotal	\$315,000
		Enginee	ring & Conting	gency (35%)	\$110,000
				TOTAL	\$425,000



Project: S2 – Main & Station Street (Hillside to Bank)

Priority:	1	Type:	Replacement/Upgrade
Trigger:	Future Development	DCC:	69%

Location Map



Issue

This main is a key connection in the sanitary collection network, and services a corridor of future development. The existing VCT pipe has surpassed its anticipated useful life.

Scope

Replacement of approximately 475 m of 200 mm VCT and 25 m of 250 mm VCT with 500 m of 300 mm PVC, including reconnection of all existing services. New connections for future development are required.

DCC Justification

This project is driven by need for additional capacity due to planned development along this corridor. DCC portion will be determined based on the change in cross sectional area of the upgrade and length of each section of pipe where the area is changing of the upgrade:

$$DCC \% = 1 - \frac{\left(\left(\frac{\pi(D_{1.1})^2}{4}\right) * L_{1.1}\right) + \left(\left(\frac{\pi(D_{1.2})^2}{4}\right) * L_{1.2}\right)}{\left(\left(\frac{\pi(D_2)^2}{4}\right) * L_2\right)} = 1 - \frac{\left(D_{1.1}^2 * L_{1.1}\right) + \left(D_{1.2}^2 * L_{1.2}\right)}{\left(D_2^2 * L_2\right)}$$

$$DCC \% = 1 - \frac{(0.2^2 * 25m) + (0.25^2 * 475m)}{(0.375^2 * 500m)} = 52\%$$



Time Frame

1-3 years

ITEM NO.	DESCRIPTION	UNIT	EST. QUANT.	UNIT PRICE	TOTAL PRICE
S2	Main & Station Street (Hillside to Bank)				
1.1	Materials 375ø PVC Sanitary Main - Supply and Install	m	500	\$480_	\$240,000
	Lined Concrete Manhole - Supply and Install	ea	8	\$8,000	\$64,000
1.2	Service Connections				
	Tie into existing	ea	6	\$3,000	\$18,000
	Reconnect existing services	ea	5	\$1,000	\$5,000
1.3	Other Construction				
	Asphalt Restoration	m²	2000	\$45	\$90,000
	Traffic Control	L.S.		\$15,000	\$15,000
				Subtotal	\$432,000
		Enginee	ring & Contin	gency (35%)	\$151,000
				TOTAL	\$583,000



Project: S3 – Similkameen Avenue (Tulameen to Airport)

Priority:	2	Туре:	Replacement/Upgrade
Trigger:	Capacity/Aging Infrastructure	DCC:	32%

Location Map



Issue

This main is a key connection in the sanitary collection network. The existing AC and VCT pipe is beyond its anticipated useful life of 50 years, and inspections in 2016 and 2017 reported that the pipe has significant condition issues. This segment of pipe is also flagged in the hydraulic model as having capacity issues under current and future wet weather conditions.

Scope

Replace approximately 415m of 200 mm and 75m of 250 mm of VCT/AC with 415m of 300 mm PVC and 85 m of 375 mm PVC to tie into existing 375 mm.

DCC Justification

This project is driven by need for additional capacity. DCC portion will be determined based on the change in cross sectional area of the upgrade and length of each section of pipe where the area is changing:



$$DCC \% = 1 - \frac{\left(\left(\frac{\pi(D_{1,1})^2}{4}\right) * L_{1,1}\right) + \left(\left(\frac{\pi(D_{1,2})^2}{4}\right) * L_{1,2}\right)}{\left(\left(\frac{\pi(D_2)^2}{4}\right) * L_2\right)} = 1 - \frac{\left(D_{1,1}^2 * L_{1,1}\right) + \left(D_{1,2}^2 * L_{1,2}\right)}{\left(D_2^2 * L_2\right)}$$

$$DCC \% = 1 - \frac{(0.2^2 * 415m) + (0.25^2 * 75m)}{(0.3^2 * 500m)} = 32\%$$

Time Frame

3-5 Years

ITEM NO.	DESCRIPTION	UNIT	EST. QUANT.	UNIT PRICE	TOTAL PRICE
S3	Similkameen Avenue (Tulameen to A	Airport)			
1.1	Materials 300Ø PVC Sanitary Main - Supply				
	and Install 375ø PVC Sanitary Main - Supply	m	415	\$400	\$166,000
	and Install Lined Concrete Manhole - Supply	m	85	\$480	\$40,800
	and Install	ea	11	\$8,000	\$88,000
1.2	Service Connections				
	Tie into existing	ea	10	\$3,000	\$30,000
	Reconnect existing services	ea	13	\$1,000	\$13,000
1.3	Other Construction				
	Asphalt Restoration	m²	2000	\$45	\$90,000
	Curb and Gutter	m	8	\$110	\$880
	Sidewalk	m	8	\$105	\$840
	Traffic Control	L.S.		\$15,000	\$15,000
				Subtotal	\$445,000
		<u> </u>			

Subtotal	\$445,000
Engineering & Contingency (35%)	\$156,000
TOTAL	\$601,000



Project: P4 – Okanagan Street at Similkameen

Priority:	2	Type:	Replacement/Upgrade
Trigger:	Aging Infrastructure	DCC:	0%

Location Map



Issue

The existing AC and VCT pipe is beyond its anticipated useful life of 50 years, and inspections in 2016 and 2017 reported that the pipe has significant condition issues.

Scope

Replace approximately 385m of 150 mm AC and 315m of 200 mm AC and VCT with 700m of 200 mm PVC.

DCC Justification

This project would not qualify for DCC.

Time Frame

3-5 Years



ITEM NO.	DESCRIPTION	UNIT	EST. QUANT.	UNIT PRICE	TOTAL PRICE
S4	Okanagan Street at Similkameen				
1.1	Materials 200Ø PVC Sanitary Main - Supply				
	and Install Lined Concrete Manhole - Supply	m	700	\$240	\$168,000
	and Install	ea	8	\$8,000	\$64,000
1.2	Service Connections				
	Tie into existing	ea	4	\$3,000	\$12,000
	Reconnect existing services	ea	40	\$1,000	\$40,000
1.3	Other Construction				
	Asphalt Restoration	m²	2800	\$45	\$126,000
	Curb and Gutter	m	12	\$110	\$1,320
	Sidewalk	m	12	\$105	\$1,260
	Traffic Control	L.S.		\$5,000	\$5,000
				Subtotal	\$418,000
		Enginee	ring & Contin	gency (35%)	\$146,000
				TOTAL	\$564,000



Project: P5 – Airport Street Alley (Skagit to Similkameen)

Priority:	2	Type:	Replacement/Upgrade
Trigger:	Aging Infrastructure	DCC:	0%

Location



Issue

The existing AC pipe is beyond its anticipated useful life of 50 years, and inspections in 2016 and 2017 reported that the pipe has significant condition issues.

Scope

Replacement of approximately 400m of 200 mm AC with 200 mm PVC.

DCC Justification

This project would not qualify for DCC.

Time Frame

3-5 Years



ITEM NO.	DESCRIPTION	UNIT	EST. QUANT.	UNIT PRICE	TOTAL PRICE
S5	Airport Street Alley (Skagit to Similk	ameen)			
1.1	Materials 200Ø PVC Sanitary Main - Supply				
	and Install Lined Concrete Manhole - Supply	m	400	\$240	\$96,000
	and Install	ea	4	\$8,000	\$32,000
1.2	Service Connections				
	Tie into existing	ea	2	\$3,000	\$6,000
	Reconnect existing services	ea	23	\$1,000	\$23,000
	Connect New Services	ea	0	\$2,000	\$0
1.3	Other Construction				
	Asphalt Restoration	m²	1600	\$45	\$72,000
	Curb and Gutter	m	4	\$110	\$440
	Sidewalk	m	4	\$105	\$420
	Traffic Control	L.S.		\$2,500	\$2,500
				Subtotal	\$232,000
		Enginee	ring & Conting	gency (35%)	\$81,000
				TOTAL	\$313,000



Project: P6 – McKinney Road (Coyote to Park)

Priority:	3	Туре:	Rehabilitation
Trigger:	Aging Infrastructure	DCC:	0%

Location Map



Issue

The existing 200 mm AC pipe is beyond its anticipated useful life of 50 years. Inspections in 2016 and 2017 reported that the pipe is in acceptable condition given its age. Rehabilitation is intended to extend the useful life of these assets with decreased cost.

Scope

Trenchless rehabilitation of 285m of 200 mm AC pipe using cured-in-place lining.

DCC Justification

This project would not qualify for DCC.

Time Frame

5-10 Years



ITEM NO.	DESCRIPTION	UNIT	EST. QUANT.	UNIT PRICE	TOTAL PRICE
S 6	McKinney Road (Coyote to Park)				
1.1	Materials Trenchless Rehabilitation (cured-in- place lining)	m	285	\$250_	\$71,250
1.2	Service Connections				
	Lining at Manholes	ea	5	\$1,000	\$5,000
	Lining at existing services	ea	1	\$500	\$500
1.3	Other Construction				
	Bypass Pumping	L.S.		\$10,000	\$10,000
				Subtotal	\$87,000
		Enginee	ring & Conting	gency (35%)	\$30,000
				TOTAL	\$117,000



Project: P7 - River Crossing at Fairview Road

Priority:	3	Туре:	Replacement/Upgrade
Trigger:	Aging Infrastructure	DCC:	56%

Location Map



Issue

This main is a very critical connection in the sanitary collection network. The existing 200 mm AC pipe is beyond its anticipated useful life of 50 years and is a high risk asset to the collection network.

Scope

Replace approximately 130m of 200 mm AC with 300 mm PVC.

(-) 2

DCC Justification

This project increases the capacity of the system for long term growth. DCC portion will be determined based on the change in cross sectional area of the upgrade:

DCC % =
$$1 - \frac{\left(\frac{\pi(D_1)^2}{4}\right)}{\left(\frac{\pi(D_2)^2}{4}\right)} = 1 - \left(\frac{D_1}{D_2}\right)^2 = 1 - \left(\frac{0.2}{0.3}\right)^2 = 56\%$$

Time Frame

5-10 Years



ITEM NO.	DESCRIPTION	UNIT	EST. QUANT.	UNIT PRICE	TOTAL PRICE
S 7	River Crossing at Fairview Road				
1.1	Materials 300Ø PVC Sanitary Main - Supply				
	and Install	m	130	\$400	\$52,000
	Lined Concrete Manhole - Supply and Install	ea	2	\$8,000	\$16,000
	Hardware (incl. hangers, casing, spacers, fittings)	m	75	\$1,000	\$75,000
1.2	Service Connections			;	,
	Tie into existing	ea	2	\$3,000	\$6,000
1.3	Other Construction				
	Asphalt Restoration	m²	260	\$45	\$11,700
	Curb and Gutter	m	8	\$110	\$880
	Sidewalk	m	8	\$105	\$840
	Traffic Control	L.S.		\$15,000	\$15,000
				Subtotal	\$177,000
		Enginee	ring & Conting	gency (35%)	\$62,000
				TOTAL	\$239,000



Project: P8 - Co-op Road (Main to Sawmill)

Priority:	3	Туре:	Replacement/Upgrade
Trigger:	Aging Infrastructure	DCC:	0%

Location



Issue

This main is a key connection in the sanitary collection network. The existing VCT pipe is beyond its anticipated useful life of 50 years, and inspections in 2016 and 2017 reported that sections of the pipe have condition issues.

Scope

Replace approximately 85 m of 150 mm, 115 m of 200 mm, and 170 m of 250 mm of VCT with 270 m of 250 mm PVC.

DCC Justification

This project would not qualify for DCC.



Time Frame

5-10 Years

ITEM NO.	DESCRIPTION	UNIT	EST. QUANT.	UNIT PRICE	TOTAL PRICE
S 8	Co-op Road (Main to Sawmill)				
1.1	Materials 250Ø PVC Sanitary Main - Supply				
	and Install	m	270	\$350	\$94,500
	Lined Concrete Manhole - Supply and Install	ea	9	\$8,000	\$72,000
1.2	Service Connections				
	Tie into existing	ea	5	\$5,000	\$25,000
	Reconnect existing services	ea	5	\$1,000	\$5,000
1.3	Other Construction				
	Asphalt Restoration	m²	1080	\$45	\$48,600
	Curb and Gutter	m	4	\$110	\$440
	Sidewalk	m	4	\$105	\$420
	Traffic Control	L.S.		\$5,000	\$5,000

Subtotal	\$251,000	
Engineering & Contingency (35%)	\$88,000	
TOTAL	\$339,000	



Project: P9 - Fir Avenue to Influent Lift Station

Priority:	3	Type:	Replacement/Upgrade
Trigger:	Aging Infrastructure	DCC:	56%

Location Map



Issue

This main is a very critical connection in the sanitary collection network. The existing 250 mm AC pipe has 10 years remaining in its anticipated useful life of 50 years.

Scope

Replace approximately 150m of 250 mm AC with 375 mm PVC and regrade to ensure adequate velocities to the Influent Lift Station.

DCC Justification

This project increases the capacity of the system for long term growth. DCC portion will be determined based on the change in cross sectional area of the upgrade:

$$DCC \% = 1 - \frac{\left(\frac{\pi (D_1)^2}{4}\right)}{\left(\frac{\pi (D_2)^2}{4}\right)} = 1 - \left(\frac{D_1}{D_2}\right)^2 = 1 - \left(\frac{0.25}{0.375}\right)^2 = 56\%$$

Time Frame

5-10 Years



Cost Estimate

ITEM NO.	DESCRIPTION	UNIT	EST. QUANT.	UNIT PRICE	TOTAL PRICE
S9	Fir Avenue to Influent Lift Station				
1.1	Materials 375ø PVC Sanitary Main - Supply and Install	m	150	\$480	\$72,000
	Lined Concrete Manhole - Supply and Install	ea	4	\$8,000	\$32,000
1.2	Service Connections				
	Tie into existing	ea	2	\$5,000	\$10,000
	Reconnect existing services	ea	2	\$1,000	\$2,000
1.3	Other Construction				
	Asphalt Restoration	m²	120	\$45	\$5,400
	Bare Land Restoration	m²	480	\$10	\$4,800
	Curb and Gutter	m	12	\$110	\$1,320
	Sidewalk	m	12	\$105	\$1,260
	Traffic Control	L.S.		\$5,000	\$5,000
				Subtotal	\$134,000
		Enginee	ring & Contin	gency (35%)	\$47,000
				TOTAL	\$181,000

APPENDIX D

Wastewater Treatment System Capacity Improvements Design Brief

(*Report Appendix A Excluded)

Wastewater Treatment System Capacity Improvements

HSIT

COLUMBIA

Design Brief

Town of

Dliver





January 2019 Project No. 306-1752



ENGINEERING ■ PLANNING ■ URBAN DESIGN ■ LAND SURVEYING

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Revision Log

0 SAC Jan. 21, 2019 Final	iption	Issue / Revision Description	Date	Revised by	Revision #
		Final	Jan. 21, 2019	SAC	0
					Contraction of the second second

Report Submission

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List of Acronyms

BOD LWMP MCC MFLNRO MOE OCP PLC PV SCADA TRUE	Biochemical Oxygen Demand Liquid Waste Management Plan Motor Control Centre Ministry of Forests, Lands, and Natural Resource Operations Ministry of Environment Official Community Plan Programmable Logic Controller Photovoltaic Supervisory Control and Data Acquisition TRUE Consulting Total Suspended Solids
TSS	Total Suspended Solids



Units of Measure

hp	horsepower
kg	kilogram
kŴ	kilowatt
lb	pound
m³	cubic metre
m³/day	cubic metres per day
m	metre
mg	milligram
mg/L	milligrams per Litre
SCFM	standard cubic feet per minute

Referenced Reports

Golder Associates Ltd. "Pseudo-Static and Liquefaction Assessment – Oliver Effluent Reservoir Dams," <17 April 2018>

TRUE Consulting Ltd. Liquid Waste Management Plan (LWMP) Update. <January 2002>

TRUE Consulting Ltd. Sanitary Sewer System 2017 Annual Report. <18 July 2018>



1.0 Description of Existing Wastewater Treatment Works

The wastewater treatment facility for the Town of Oliver has been in operation since 1965. From 1965 to 1984, the Town operated a treatment plant for municipal wastewater and discharged treated effluent to the Okanagan River. In response to regulatory agency requirements for reduced phosphorus loadings to surface water courses in the Okanagan River Basin, the Town constructed effluent storage and land disposal systems in the Fairview area in 1983 and 1984. Discharge to the Okanagan River was discontinued. Finally, in 1995, a two-cell aerated lagoon system was constructed in the Fairview area.

Currently, the overall existing wastewater treatment system is comprised of influent screening, equalization storage, a high lift pump station, a two-cell aerated lagoon treatment system, winter effluent storage, chlorine contact system and reclaimed water irrigation.

This two-cell aerated lagoon system is located north and adjacent to the winter effluent storage reservoir. The aerated cells designated as Cell No. 2 and Cell No. 3 have been constructed as the second and third cells of an ultimate 3 cell system. Piping and other design provisions have been made for the third cell to be located immediately east of the existing lagoons. The capacity of the existing aerated lagoon system is as follows. Note that each cell has an operating depth of 5.3m.

- Cell No. 2 37,600 m³
- Cell No. 3 38,200 m³

Aeration is provided by a submerged bottom fixed fine bubble diffuser system. Air to the system is supplied by two 40 hp positive displacement Aerzen Model GM35S blowers housed in a building located at the south-east corner of Cell No. 2. Piping, electrical and space provisions have been made in the building for the installation of two additional blower units.

The treatment system effluent is regulated by Operational Certificate for PE 13717 issued by the Ministry of Environment (MOE). This operation certificate specifies the following limits:

- Discharge rate 2,200 m³/day
- 5 Day Biochemical Oxygen Demand 45 mg/L
- Total Suspended Solids 60 mg/L

A location and site plan of the aerated lagoon treatment system is provided in Appendix B.



1

1.1 Existing Flows Entering Aerated Lagoon System

The total volume pumped to the aerated lagoons in 2017 was 689,098 m³, as specified in the Town's Sanitary Sewer System 2017 Annual Report, which equates to an average daily flow of 1,888 m³/day. This is an increase of 49,300 m³ (7%) compared to 2016. For comparison, average day influent flows for the period 1996 to 2017 are illustrated in Figure 1-1 as follows. This figure also illustrates census population for the Town over that time period.

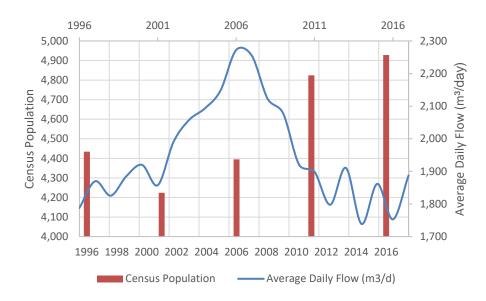


FIGURE 1-1: AVERAGE DAILY INFLUENT SEWAGE FLOWS AND CENSUS POPULATION FOR 1996 TO 2017



2.0 Wastewater Treatment System Deficiencies

The design average daily flow for the aerated lagoon system is 3,000 m³/day with a detention time of 12 days for each cell. The Town's Liquid Waste Management Plan (LWMP) Update dated January 2002 noted that the upgrading works for the system would be necessary around 2020, at which time it was recommended that the Town proceed with the construction of a third aerated lagoon. This future lagoon (referred to as Cell No. 1) would be sized at 20,000 m³.

It should be noted that growth projections from the Town's LWMP Update dated January 2002 have not yet been realized. Therefore, it is anticipated that the existing treatment works will be adequate past the 2020 upgrading date specified in that report, but this timeframe is limited by current and future sludge accumulation.

The Town's Sanitary Sewer System 2017 Annual Report reported multiple instances of BOD and TSS levels exceeding permitted levels. These exceedances have been attributed to sludge accumulation in the aerated lagoons. Based on these exceedances, the Town has begun the process of working towards providing additional capacity to this aerated lagoon system.

Other issues related to the aerated lagoon treatment system are summarized in the following sections.

2.1 Concerns Related to Proposed Cell No. 1 Location

In February 2017, a crown land tenure application was submitted to the Ministry of Forests, Lands, and Natural Resource Operations (MFLNRO) to obtain crown land necessary for the construction of Cell No. 1. Upon receipt of the crown land tenure application, MFLNRO staff informed the Town that an assessment relating to recreation and environmental protection of the Oliver Mountain area was currently being undertaken. MFLNRO also conducted a site visit and deemed the area to be "very" environmentally sensitive with significant concerns related to the following species:

- Lewis woodpecker
- Great Basin Spadefoot
- Behr's Hairstreak

On the basis of concerns raised by MFLNRO staff, it was recommended that the Town review other options for increasing the treatment capacity of the treatment works.



2.2 Sludge Accumulation

Sludge accumulation, specified in 2011 as approximately 5,000 m³ in Cell No. 2 and 3,000 m³ in Cell No. 3, has had the effect of reducing lagoon capacity and detention time. Therefore, sludge requires removal prior to treatment objectives being compromised due to reduced lagoon capacity. In this case, the Town of Oliver retained a sludge survey specialist in 2011 to conduct a review of sludge accumulation in the period since the lagoons were first constructed (summer 1995). The results of this survey indicated that sludge accumulation was far greater in Cell No. 2 than in Cell No. 3. This result is consistent with other municipalities experiences where sludge is found to accumulate near the inlet of the treatment system. After reviewing these findings, it was recommended that sludge volume is greater as a percentage of the total volume. Also, detention time at the inlet to the treatment system is more important than detention time near the "end" of the treatment system. In the period since 2011, sludge accumulation has likely remained consistent.

2.3 Middle Berm Stability

The third significant issue with the existing treatment system relates to the instability of the earthen berm separating Cell No. 2 and Cell No. 3. The Town's Pseudo-Static and Liquefaction Assessment of the Town's effluent reservoir dams completed by Golder Associates Ltd. in April 2018 also noted that this berm would be likely to fail during a seismic event. This berm is known to be saturated and will likely fail if Cell No. 2 is drained and bypassed during sludge removal operations. Another complicating factor is that Cell No. 3 must also remain in service to ensure that operating permit effluent quality is achieved. Therefore, operating levels must be adequate to allow for treatment to occur. Since minimum operating levels must be provided, it will be necessary to stabilize the earthen berm.

2.4 Summary of Aerated Lagoon Deficiencies

Considering the above Sections 2.1 to 2.3, the following summary of deficiencies is presented. These deficiencies represent required high priority upgrades necessary for the Town to correct issues related with the aerated lagoon and achieve treatment objectives specified in Operational Certificate PE 13717.

- Exceedance of permitted effluent BOD and TSS levels.
 - Capacity improvements are required for treatment objectives to be achieved.
- Stability of middle berm.
 - Middle berm is saturated and requires upgrading. The existing two-cell aerated lagoon system does not provide redundancy since the middle berm cannot be relied upon.



4

As discussed in Section 2.1, the proposed location of Cell No. 1 does not appear to be viable. Therefore, the Town will be forced to consider alternative options for achieving treatment objectives in the future. Expansion of the existing lagoon footprint also does not appear to be a viable option. Therefore, upgrading of the aerated lagoon treatment works will be required.



3.0 Upgrading Objectives

The primary objective of the Wastewater Treatment System upgrading will be the resolution of deficiencies related to the existing aerated lagoon system. As previously discussed, these deficiencies are related to capacity and safety. Upgrading should also consider the potential of an expansion of the overall capacity to meet future requirements.

The following sections are presented to ensure that recommended upgrades are consistent with the Town's future capacity requirements. Therefore, expected flows arising from future population growth will be reviewed in detail.

3.1 Population Projections

The 2016 Town of Oliver census population was 4,928. The Town of Oliver Official Community Plan projects that the Town can anticipate a growth rate between -1% to 1% over the next 20 years. A growth rate of 1% per year is used for population projections within the Town of Oliver to provide a representative estimate for asset upgrades and replacement. A growth rate of 2% is also presented to provide a more conservative estimate.

	Population Projection		
Year	1% growth rate	2% growth rate	
2018	5,027	5, 127	
2028	5,553	6,250	
2038	6,134	7,619	
2048	6,776	9,287	
2058	7,485	11,321	
2068	8,268	13,800	
2078	9,133	16,822	

TABLE 3-1: POPULATION PROJECTIONS BASED ON 2016 CENSUS

The following Figure 3-1 illustrates expected sewer influent flow associated with both specified growth rates. Note that future influent flow levels are based on 2016 average day flow conditions. The following figure shows that the two-cell aerated treatment system is expected to be adequate until between 2040 and 2070 depending upon future growth rates. This projection assumes that sludge accumulation does not affect treatment capacity.



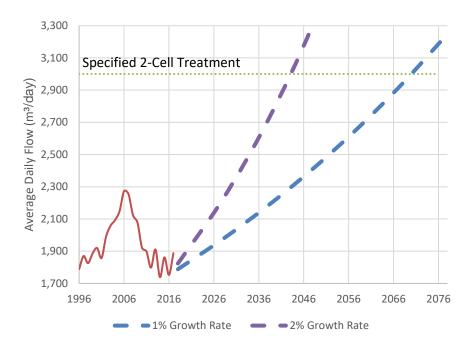


FIGURE 3-1: PROJECTED AVERAGE DAILY SEWAGE INFLUENT FLOWS

3.2 Design Capacity

This section is provided to determine when the treatment objectives relating to the existing treatment system will exceed permitted maximum levels of 45 mg/L BOD and 60 mg/L TSS. The following calculations are provided to indicate when these treatment objectives will be exceeded based on existing conditions (i.e. lagoons are not desludged) and ideal conditions (i.e. lagoons are fully desludged). Note that winter conditions govern and the Town's 2016 Annual Report indicated that average flow for this system is about 1,753 m³/d.

Existing Design Conditions (i.e. lagoons are fully desludged)

- Volume: Cell No. 2 has capacity of 37,600 m³ while Cell No. 3 has capacity of 38,200 m³ resulting in a total design capacity of 75,800 m³
- Detention time = 75,800 m³ divided by 1,753 m³/day = 43.2 days
- 2016 Oliver census population = 4,928 persons
- Theoretical BOD = 0.17 lb/capita or 0.077 kg/capita x 4,928 persons = 379 kg/day BOD in
- Influent BOD concentration = BOD in divided by flow = 379 kg/day divided by 1,753 m³/day = 0.216 kg/m³ x 1x10⁶ mg/kg divided by 1,000 L/m³ = 216 mg/L BOD in
- Theoretical reaction rate if wastewater temperature is assumed to be 5°C during winter conditions = 0.162 day⁻¹



- Removal efficiency = 1 / (1 + reaction rate x detention time) = 12.5% remaining
- Wastewater treatment system Effluent BOD = removal efficiency x BOD in = 12.5% x 216 mg/L = 27.0 mg/L BOD
- Exceedance of 45 mg/L during winter conditions:
 - found to be in 2077 with a population equivalent of about 9,080 persons (assumes 1% growth rate)
 - found to be in 2046 with a population equivalent of about 9,080 persons (assumes 2% growth rate)

Existing Conditions (i.e. lagoons are not desludged)

- Volume: As of 2011, Cell No. 2 had a sludge accumulation of 5,000 m³ while Cell No. 3 had a sludge accumulation of 3,000 m³.
- Projected sludge accumulation is based off annual sludge accumulation between 1996 and 2011.
- Detention time = about 65,000 m³ divided by 1,753 m³/day = 37.1 days for 2016 conditions
- 2016 Oliver census population = 4,928 persons
- Theoretical BOD = 0.17 lb/capita or 0.077 kg/capita x 4,928 persons = 379 kg/day BOD in
- Influent BOD concentration = BOD in divided by flow = 379 kg/day divided by 1,753 m³/day = 0.216 kg/m³ x 1x10⁶ mg/kg divided by 1,000 L/m³ = 216 mg/L BOD in
- Theoretical reaction rate if wastewater temperature is assumed to be 5°C during winter conditions = 0.162 day⁻¹
- Removal efficiency = 1 / (1 + reaction rate x detention time) = 14.3% remaining
- Wastewater treatment system Effluent BOD = removal efficiency x BOD in = 14.3% x 216 mg/L = 30.8 mg/L BOD
- Exceedance of 45 mg/L during winter conditions:
 - found to be in 2040 with a population equivalent of about 6,270 persons (assumes 1% growth rate)
 - found to be in 2032 with a population equivalent of about 6,780 persons (assumes 2% growth rate)

Based on the above, it can be assumed that the existing system has adequate capacity for the existing service population. Also, additional lagoon capacity will not be necessary until between 2032 and 2077 (depending upon sludge accumulation and future desludging efforts). Desludging will therefore allow the Town to defer capacity upgrades in the future. This projection is approximately consistent with the findings presented in Section 3.1.



4.0 Proposed Upgrading Works

The upgrading works discussed in this section have been recommended on the basis of addressing deficiencies to the existing aerated lagoon treatment system. As discussed in Section 0, the Town's aerated lagoons have adequate capacity to achieve treatment objectives until at least 2032 providing that adequate desludging occurs on an ongoing basis. Therefore, upgrading works will mostly address deficiencies related to safety and operational issues, but will also consider capacity upgrades that will be necessary at some point in the future. A site plan of the proposed upgrades is provided in Appendix B.

The following sections summarize proposed upgrades to address aerated lagoon system deficiencies. Also note that a photovoltaic system has been recommended to offset a portion of greenhouse gas emissions associated with operating the aeriated lagoon system.

4.1 Middle Berm Stabilization

The initial component of the project would be to stabilize the existing middle berm. As previously discussed, this berm is known to be saturated and would likely fail if the water level of one of the lagoons was lowered independently of the other. Therefore, to rectify this issue, it is proposed that two lock block walls be installed along the length of this berm. These walls would be tied to each other with geogrid to provide stability and infilled. Since the existing aeration system header is installed within the existing berm, this project would necessitate the replacement of the lagoon aeration system. It should also be noted that the existing aeration system is reaching the end of its expected lifespan and therefore this project would allow for its replacement. A secondary benefit of this berm stabilization would be that the existing lagoon capacity would increase due to the installation of a wall structure in place of the existing 3:1 lagoon slopes.

4.2 Aeration System Upgrades

Following the proposed middle berm stabilization project, the following upgrades are proposed as a means to increase treatment capacity of the existing lagoon system.

- Desludging of Cell No. 2:
 - draining of liquid components from Cell No. 2 to Cell No. 3,
 - removal of the aeration system in both cells,
 - pumping of sludge from Cell No. 2 to a dewatering system which is to be located in a Town owned property approximately 850m away from the lagoon system,
- Aeration system upgrades:
 - Installation of a new aeration header and laterals pipes to each lagoon. Note that a floating aeration system is proposed to ease future operations and maintenance.



- Provision of new aeration system diffusers.
- Installation of a new blower in the existing blower building. The new blower will act as
 the duty blower for the aeration system and is proposed to be controlled by a dissolved
 oxygen sensor in the lagoon. Therefore, the level of dissolved oxygen in the treatment
 system will control the level of airflow from the proposed blower. This system is
 expected to result in a more efficient aeration system and help the Town of Oliver to
 reduce power consumption relating to wastewater treatment.

The aeration system would be designed to allow for future conversion of the treatment works to an intermittently decanted extended aeration system. This type of system would allow higher levels of BOD, TSS and ammonia removal while continuing to utilize the existing lagoon footprint. These future improvements would be installed on an as required timeline based on population growth of the Town of Oliver.

4.3 50 kW Photovoltaic System

The final portion of this project will be to utilize the aerated lagoon site as a location for renewable energy production as a means to offset emissions produced by the Town of Oliver. The Photovoltaic (PV) power will be connected to the system by means of a "grid-tie" inverter and metered by FortisBC under their net metering program. This means that the grid is used as the battery, and electricity can flow in both directions as required. This project would place Oliver as a leader in the province in terms of photovoltaic energy production at a time when renewable energy is as important as ever. It will also further local knowledge and expertise in the photovoltaic industry. The proposed solar array would be sized at 50 kW which will ensure that the project remains within FortisBC's net metering limit per electrical service. Further, the anticipated consumption remains under the amount consumed at each location (another criteria of the FortisBC net metering program). The electricity usage at this site is by the municipality and is anticipated to remain stable long term.



5.0 Future Upgrades

As discussed in Section 4.2, the proposed upgrades would be designed to allow for future conversion of the treatment works to an intermittently decanted extended aeration system. This future upgrade will require the installation of the following additional components:

- Blowers airflow requirement of 1,150 SCFM
- Floating aeration system (this would be included in the aeration system upgrades portion of the project – see Section 4.2)
- Lagoon baffle curtains
- Influent manifold
- PLC Control system and control valves
- Control probes and transducers

The above upgrades are expected to increase the lagoon reaction rate of the aerated lagoons. A projection of treatment levels associated with these future upgrades are summarized following:

- Discharge rate 3,230 m³/day
- 5 Day Biochemical Oxygen Demand 20 mg/L
- Total Suspended Solids 20 mg/L

The 2016 average daily flow equates to approximately 355 L/capita/day. Therefore, the peak flow able to be treated utilizing the future intermittently decanted extended aeration system is approximately equivalent to 9,100 people which is projected to occur in about 60 years assuming the OCP specified growth rate remains appropriate. It should also be noted that the assumed future treatment objectives of 20 mg/L for both BOD and TSS are higher than the existing Class 'C' effluent requirements currently specified in the Town's operational certificate. If the specified effluent requirements remain consistent with current conditions, the future design flow rate would increase accordingly.



6.0 Assessment Summary

The Town's aerated lagoon treatment works were constructed in 1995/1996 to treat wastewater effluent to at least 45 mg/L BOD and 60 mg/L TSS. In the period since the treatment system was constructed, various deficiencies have been identified relating to capacity and operation issues. Deficiencies associated with the aerated lagoon treatment system are:

- Exceedance of permitted effluent BOD and TSS levels.
 - Capacity improvements are required for treatment objectives to be achieved.
- Stability of middle berm.
 - Middle berm is saturated and requires upgrading. The existing two-cell aerated lagoon system does not provide redundancy since the middle berm cannot be relied upon.

Conceptually, upgrading works to address the above identified deficiencies would comprise:

- Middle berm stabilization
- Aeration system upgrades including desludging
- Allowances for future capacity upgrades

The project would also include a 50 kW photovoltaic system to reduce the carbon footprint of the Town's treatment system.

A capital cost estimate for the above upgrades of \$4,645,000 is derived in the following Section 6.1.

Further to these proposed upgrades, a recommendation moving forward would be to desludge these lagoons on a regular basis to ensure that adequate treatment capacity is maintained. It should also be noted that a geotechnical investigation relating to the preferred method for stabilizing the middle berm would be required for this project. It is suggested that the Town proceed with this geotechnical investigation prior to commencement of the detailed design phase.

6.1 Capital Cost Estimate

A preliminary (Class D) capital cost estimate of expected costs associated with this project is provided following.



TABLE 6-1: CAPITAL COST ESTIMATE

Part	A - Middle Berm Stabilization		
A1.0	Bulk excavation of existing middle berm to allow installation of proposed lock block walls	22000 m ³ @ \$15 / m ³	\$330,000
A2.0	Two lock block walls	2000 m² @ \$1000 / m²	\$2,000,000
A3.0	Infill between lock block walls	4900 m ³ @ \$20 / m ³	\$98,000
A4.0	LDPE membrane	2000 m ² @ \$20 / m ²	\$40,000
	Subtotal: Part A - Mide	le Berm Stabilization	\$2,468,000
Part	B - Aeration System Upgrades		
B1.0	Remove aeration system	Allow	\$10,000
B2.0	phases to allow for dewatering of geotextile tubes)		
2.1	Mobilization and demobilization	Allow	\$20,000
2.2	Construct laydown area	Allow	\$15,000
2.3	Supply only geotextile tubes	12 ea. @ \$15000 ea.	\$180,000
2.4	Temporary overland piping to laydown area	850 l.m. @ \$50 / l.m.	\$42,500
2.4	Pump sludge to geotextile tubes	12000 m ³ @ \$20 / m ³	\$240,000
2.5	Bottom area cleanup and leveling	Allow	\$15,000
B3.0	Aeration system		
3.1	Aeration header	300 l.m. @ \$150 / l.m.	\$45,000
3.2	Aeration laterals (allow for floating system)	1000 l.m. @ \$115 / l.m.	\$115,000
3.3	Diffusers complete with rubber hose and connection to laterals	50 ea. @ \$1500 ea.	\$75,000
B4.0	Supply and install 30hp blower complete with variable frequency drive	L.S.	\$55,000
B5.0	Electrical and programming	Allow	\$30,000
	Subtotal: Part B - Aerat	ion System Upgrades	\$842,500
Part	C - 50 kW Photovoltaic System		
C1.0	Photovoltaic panels	50000 W @ \$1.5 / W	\$75,000
C2.0	Inverters	50000 W @ \$1.25 / W	\$62,500
C3.0	Installation	50000 W @ \$2.5 / W	\$125,000
	Subtotal: Part C - 50 kW	/ Photovoltaic System	\$262,500
Sumr	nary		
	Subtotal: Part A - Middle Berm Stabilization		\$2,468,000
	Subtotal: Part B - Aeration System Upgrades		\$842,500
	Subtotal: Part C - 50 kW Photovoltaic System		\$262,500
		Subtotal Parts A - C	\$3,573,000
	Contingencies & En	gineering (allow 30%)	\$1,072,000
		L (not including GST)	\$4,645,000



6.2 Lifecycle Expenditures

Consistent with the Guide to the Amortization of Tangible Capital Assets produced by the Local Government Infrastructure and Finance Division of the BC government in May 2008, the following expected lifespans are presented in relation to components of the Town's aerated treatment system.

 TABLE 6-2: "PUBLISHED" EXPECTED LIFESPANS OF AERATED LAGOON TREATMENT ASSETS

Asset	Expected Lifespan
Aerators	15 years
Blowers	10 years
Lagoons	50 years

Both the original aerators and blowers that are in service at the Town's aerated lagoon treatment system are still in operation. Therefore, the "published" expected lifespan for these components can be expected to be conservative. A comparison of these "published" lifespans and "observed" lifespans is therefore provided following. In order to provide an expected lifecyle expenditure, the "observed" lifespans will be utilized.

TABLE 6-3: "OBSERVED" EXPECTED LIFESPANS OF AERATED LAGOON TREATMENT ASSETS

Asset	Expected Lifespan
Aerators	25 years
Blowers	25 years

It is anticipated that the proposed project will result in fully rehabilitated aerated lagoons and therefore it is anticipated that the aerated lagoons will have a new expected lifespan of at least 50 years. Lifecycle capital expenditures for the aerated lagoon system must then include replacement of aerators, replacement of blowers, and desludging operations to match the expected lifespan of the lagoon system. The period between desludging operations is expected to be 25 years which is approximately equivalent to the currently planned desludging operations and the initial lagoon construction date. A projection of these expenditures is presented following. Note that these projected expenditures are presented in 2019 dollars and should be adjusted utilizing the ENR cost index to account for future costs.



TABLE 6-4: PROJECTED LIFECYCLE EXPENDITURES

Asset	Lifecycle Replacements and Unit Rate	Total Cost including 30% Contingency and Engineering	
Aeration System	2 @ \$75,000	\$195,000	
Blowers	2 @ \$80,000	\$208,000	
Desludging	2 @ \$512,500	\$1,332,500	
Total Capit	al Expenditure Cost over 50 years	\$1,735,500	
	Cost per year	\$34,710	

6.3 Annual Operating Costs

Annual operating costs are expected to include aeration system maintenance requirements and energy costs associated with the blowers. A projection of these annual costs is presented following:

TABLE 6-5: ANNUAL OPERATING COSTS

Component	Unit and Unit Cost	Cost
Aeration System Maintenance	50 hours @ \$60 / hr	\$3,000
Blower Electrical Costs	60,000 kWh @ 10.195 cents / kWh	\$6,000
	Total Annual Expenditures	\$9,000



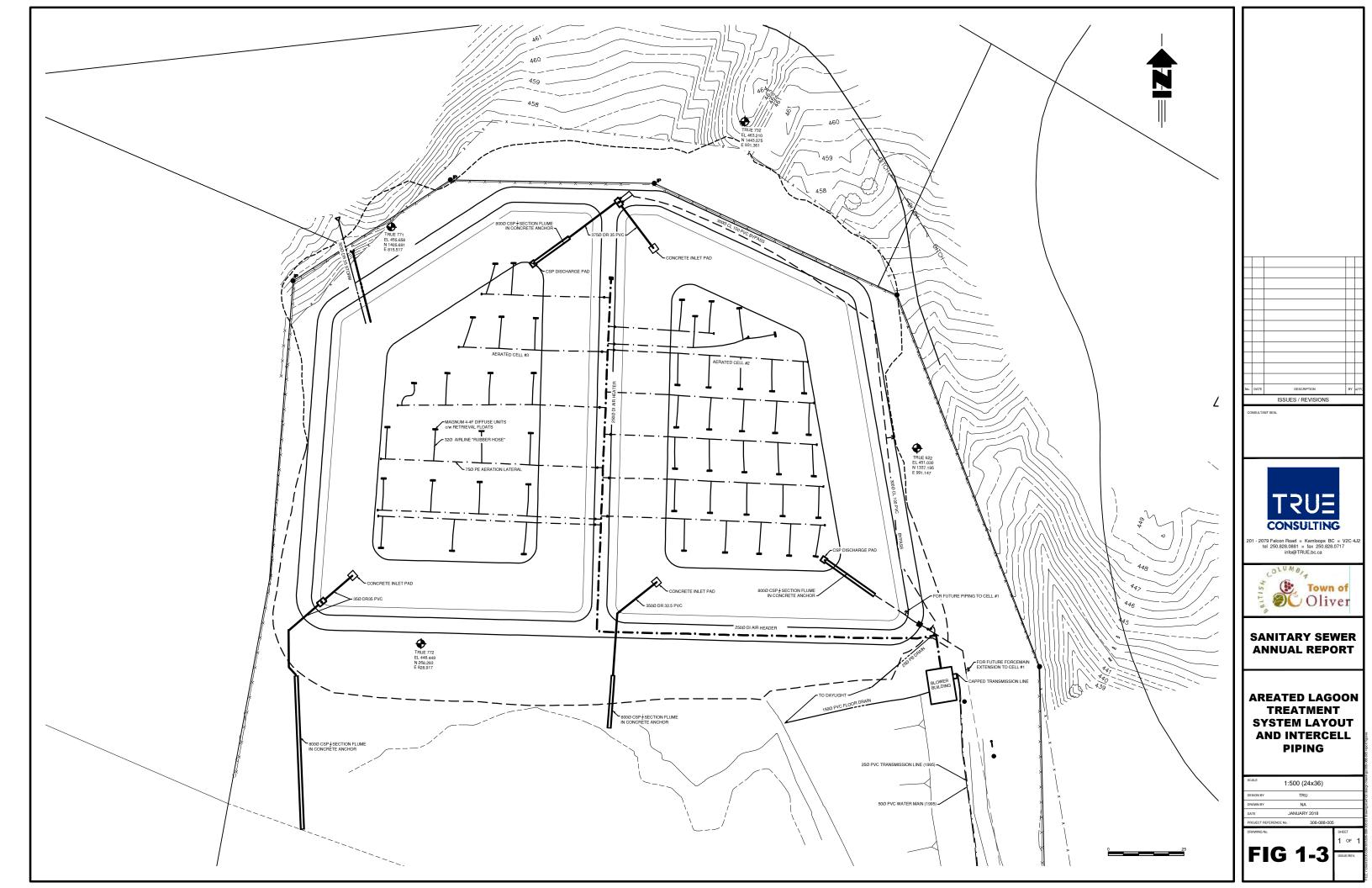
APPENDIX B

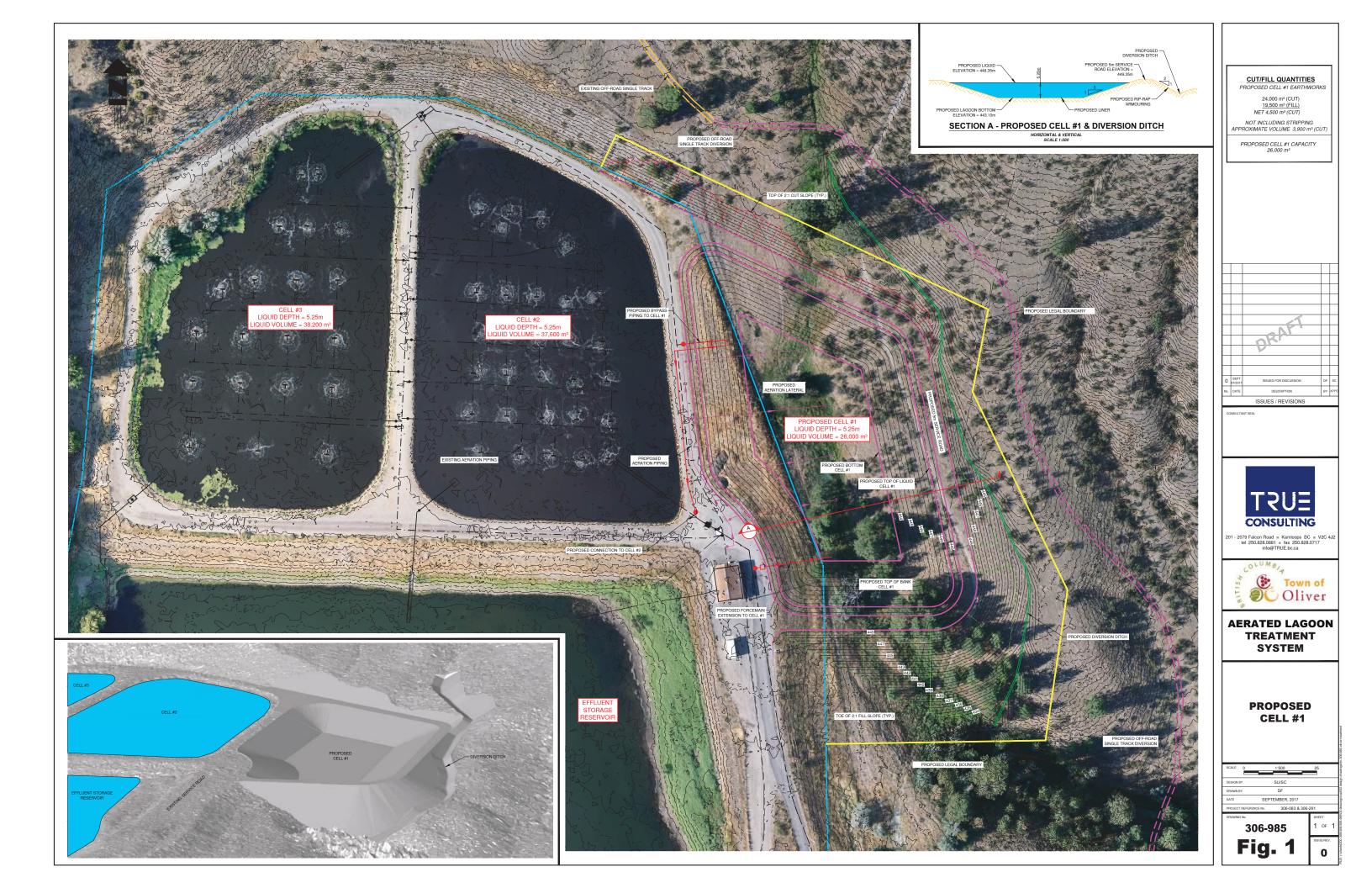
Figure 1-3 - Aerated Lagoon Treatment System Layout and Intercell Piping

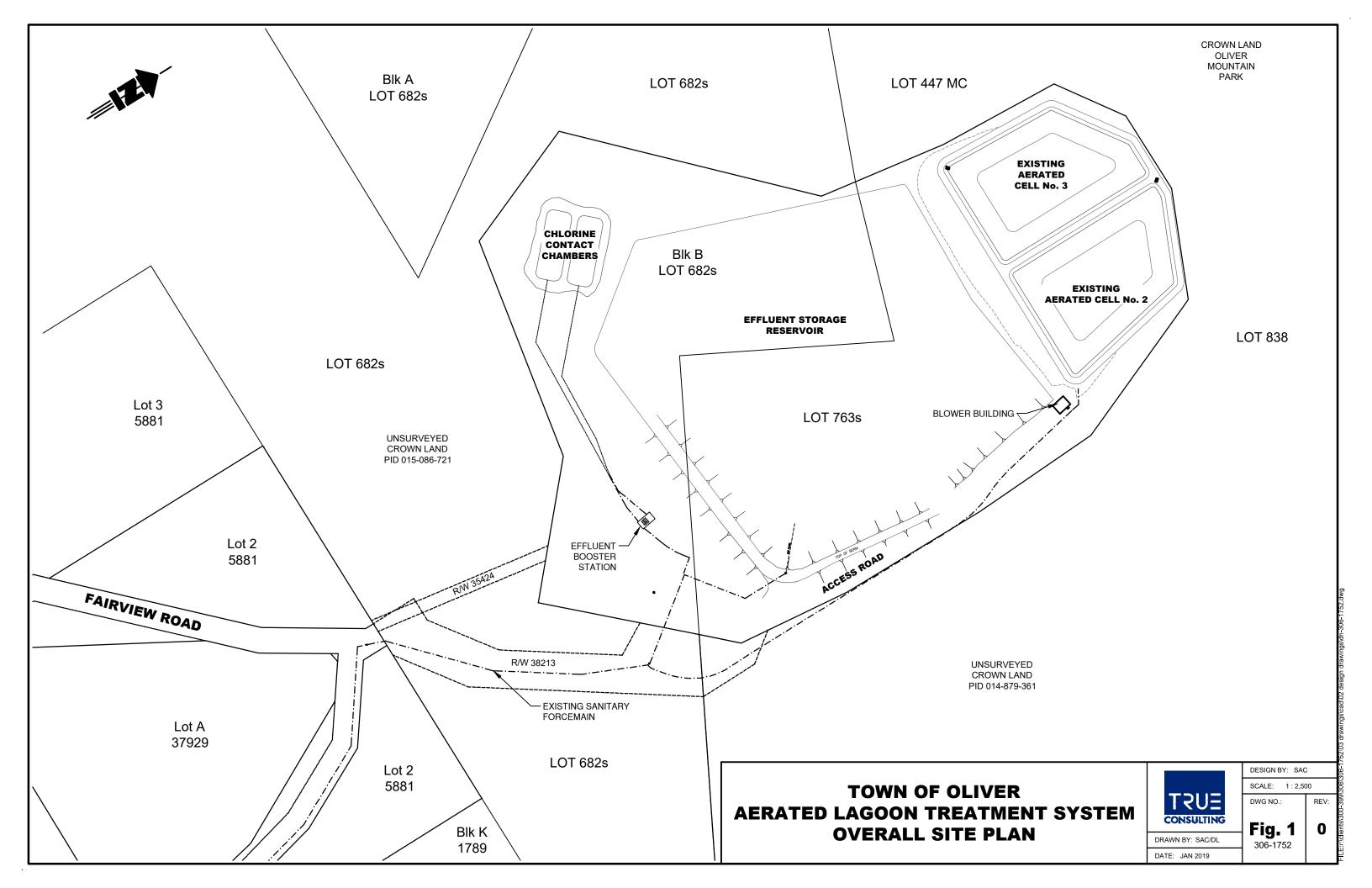
306-985 Figure 1 - Proposed Cell No. 1

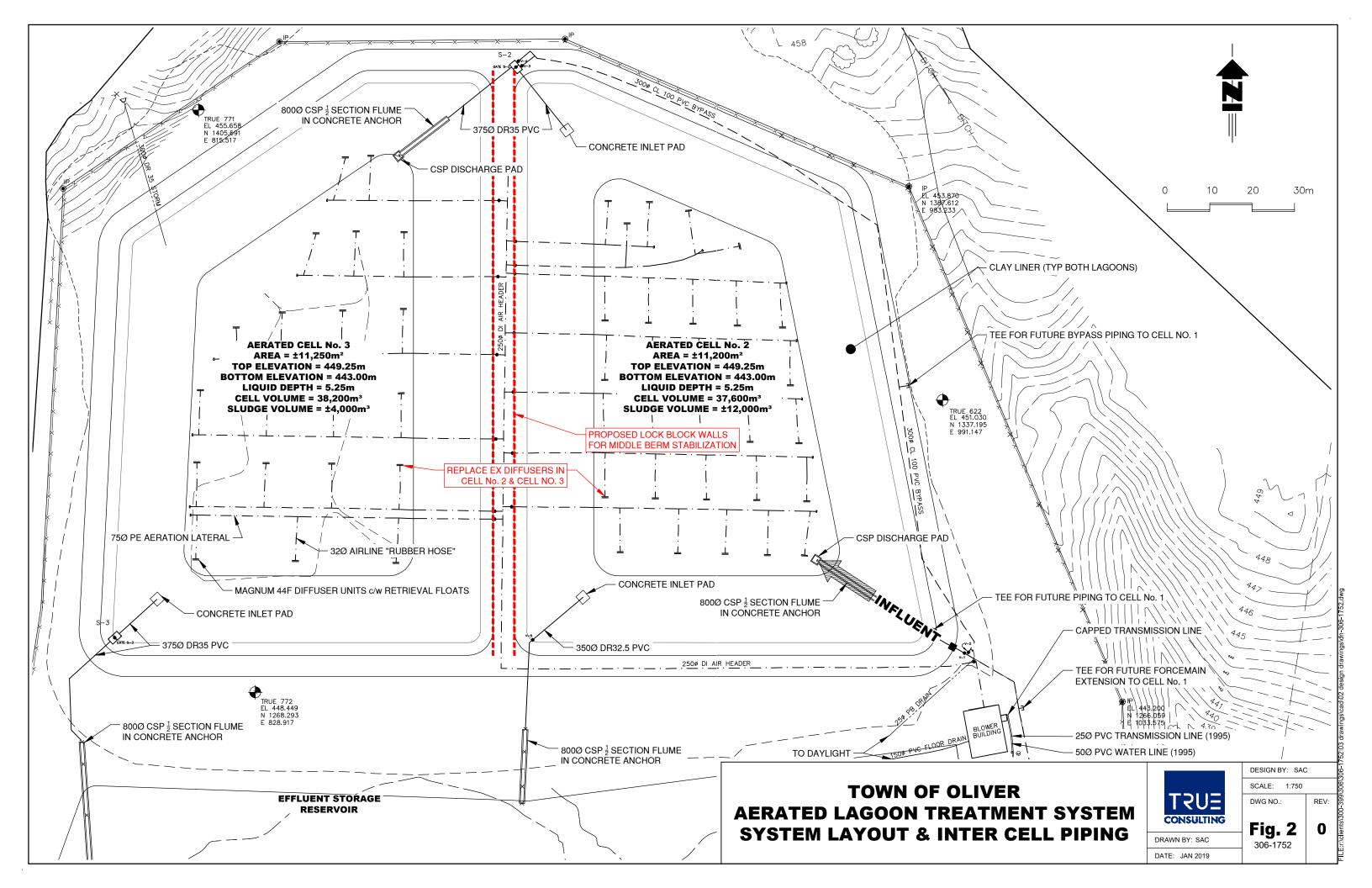
306-1752 Figure 1 - Overall Site Plan

306-1752 Figure 2 System Layout & Inter Cell Piping









APPENDIX C

Influent and Effluent Sampling Data

	F	ligh Lift Sta	tion		Chlorir	e Booster St	ation	
ľ	Daily	Total	Monthly		Rapid	Total	Total	Monthly
	Flow	Monthly	Average	Irrigation	Infiltration	Daily	Monthly	Average
January	m3/day	m3/day	m3/day	m3/day (1)	m3/day (2)		m3/day	m3/day
1	2384.13		ļ					
2	1493.05							
3	608.18							
4	1584.91							
5	1565.99							
6	1546.87							
7	1518.60							
8	2420.06							
9	1593.51							
10	653.00							
11	1551.78							
12	1589.89							
13	1549.34							
14	1598.40							
15	2472.55							
16	1669.77							
17	575.71							
18	1632.95							
19	1600.49							
20	1552.10							
21	1582.67							
22	2576.67							
23	1701.06							
24	726.88							
25	1589.45							
26	1608.99							
27	1603.98							
28	1632.07							
29	2611.34							
30	1702.11							
31	679.11							
		49176	1586	0.0	0		0.0	#DIV/0!
l	OC Limit	n/a	2050m3/day				n/a	n/a

Notes:

(1) These readings have been calculated by subtracting the flows read at the rapid infiltration site, from the flows read on the main meter in the Chlorine Booster Station. Both the irrigation flows and the rapid infiltration flows travel through this meter.

Ī	High Lift Station				Chlorine Booster Station				
ľ	Daily	Total	Monthly		Rapid	Total	Total	Monthly	
	Flow	Monthly	Average	Irrigation	Infiltration	Daily	Monthly	Average	
February	m3/day	m3/day	m3/day	m3/day (1)	m3/day (2)	m3/day (3)	m3/day	m3/day	
1	1,614								
2	1,644								
3	1,640								
4	1,613								
5	2,450								
6	1,726								
7	533								
8	1,703								
9	1,644								
10	1,616								
11 12	1,653								
12	2,407 1,612								
13	662								
14	1,619								
16	1,652								
17	1,781								
18	1,461								
19	2,317								
20	1,345								
21	856								
22	1,566								
23	1,614								
24	1,571								
25	1,575								
26									
27									
28									
29									
30									
31			-						
		00074	4505						
	001	39874	1595	0	0		0.0	#DIV/0!	
L	OC Limit	n/a	2050m3/da	iy			n/a	n/a	

Notes:

- (1) These readings have been calculated by subtracting the flows read at the rapid infiltration site, from the flows read on the main meter in the Chlorine Booster Station. Both the irrigation flows and the rapid infiltration flows travel through this meter.
- (2) These flows are read at two, 2 inch water meters located at the rapid infiltration site.
- (3) These are the flows that have been read at the main meter located in the Chlorine Booster Station.

	Hi	gh Lift Stati			Chlorir	ne Booster St	ation	
	Daily	Total	Monthly		Rapid	Total	Total	Monthly
	Flow	Monthly	Average	Irrigation	Infiltration	Daily	Monthly	Average
March	m3/day	m3/day	m3/day	m3/day (1)	m3/day (2)	m3/day (3)	m3/day	m3/day
	1 1795.828					0.0		
	2 1676.47					0.0		
	3 1596.23					0.0		
	4 1551.381					0.0		
	5 2325.6					0.0		
	6 1518.921					0.0		
	7 801.5					0.0		
	8 1644.5					0.0		
	9 1623.1					0.0		
	0 1521.3					0.0		
	1 1590.3					0.0		
	2 2366.366					0.0		
	3 1614.2					0.0		
	4 735.4504					0.0		
	5 1671.107					0.0		
	6 1604.6					0.0		
	7 1569.6					0.0		
	8 1562.387					0.0		
	9 2365.976					0.0		
	20 1579.056					0.0		
	21 568.97					707.9		
	2 1625.591					2070.2		
	1536.663					105.1		
	24 <u>1623.805</u> 25 1537.111					0.0		
	26 2197.869					0.0 0.0		
	27 1648.1					331.7		
	28 631.3					0.0		
	29 1618.483					434.4		
	30 1472.6					400.0		
	1482.835					375.9		
	1402.000					575.9		
		48657	1570	0	0		4425.6	143
	OC Limit	n/a	2050m3/da				n/a	n/a

Notes:

(1) These readings have been calculated by subtracting the flows read at the rapid infiltration site, from the flows read on the main meter in the Chlorine Booster Station. Both the irrigation flows and the rapid infiltration flows travel through this meter.

(2) These flows are read at two, 2 inch water meters located at the rapid infiltration site.

]	Hi	gh Lift Stati	on		Chlorin	ne Booster St	ation	
	ľ	Daily	Total	Monthly		Rapid	Total	Total	Monthly
		Flow	Monthly	Average	Irrigation	Infiltration	Daily	Monthly	Average
April		m3/day	m3/day	m3/day	m3/day (1)	m3/day (2)	m3/day (3)	m3/day	m3/day
	1	1611.466					335.0		
	2	2142.364					554.5		
	3	1668.145					571.3		
	4	750.1					541.7		
	5	1689.474					0.0		
	6	1416.1					334.8		
	7	1649.522					767.2		
	8	1724.065					1046.9		
	9	2141.3					2476.9		
	10	1838.816					3009.9		
	11	491.8528					1048.4		
	12	1685.477					1077.7		
	13	1614.5					1108.2		
	14	1639.3					833.3		
	15	1563.85					1616.3		
	16	2357.053					824.2		
	17	1676.3					1683.8		
	18	483.5473					1777.8		
	19	1641.775					1087.7		
	20	1688.714					781.4		
	21	1681.065					598.5		
	22	1632.998					354.9		
	23	2273.474					932.6		
	24	1656.452					1193.1		
	25	739.2314					821.9		
	26	1661.48					1415.0		
	27	1625.037					386.6		
	28	1623.774					1416.4		
	29	1583.81					1617.2		
	30	2450.066					1155.6		
	31	1730.287							-
	ļ								
			50131	1617	0	0		31368.9	1046
		OC Limit	n/a	2050m3/da	у			n/a	n/a

Notes:

(1) These readings have been calculated by subtracting the flows read at the rapid infiltration site, from the flows read on the main meter in the Chlorine Booster Station. Both the irrigation flows and the rapid infiltration flows travel through this meter.

(2) These flows are read at two, 2 inch water meters located at the rapid infiltration site.

	[Hig	gh Lift Stati	on		Chlorir	ne Booster St	ation	
		Daily	Total	Monthly		Rapid	Total	Total	Monthly
		Flow	Monthly	Average	Irrigation	Infiltration	Daily	Monthly	Average
May		m3/day	m3/day	m3/day	m3/day (1)	m3/day (2)	m3/day (3)	m3/day	m3/day
	1	1730.3					768.9		
	2	526.742					1208.5		
	3	1657.911					1199.8		
	4	1723.8					1561.7		
	5	1630.189					1279.3		
	6	1621.424					0.0		
	7	2644.703					756.7		
	8	1743.1					734.5		
	9	891.2107					1312.7		
	10 11	1725.3 1634.043					1759.4 1709.4		
	12	1604.8					1638.9		
	13	1711.3					878.5		
	14	2628.3					1183.0		
	15	1771.8					382.0		
	16	431.3055					0.0		
	17	1623.1					1038.0		
	18	1728.4					967.3		
	19	1631.9					1581.4		
	20	1620.4					1318.7		
	21	2489.499					743.8		
	22	1687.156					961.2		
	23	723.3					1539.3		
	24	1627.1					1603.0		
	25	1606.252					2098.5		
	26	1724.718					2501.0		
	27	1761.697					2479.0		
	28	2552.7					3024.3		
	29	1782.758					2354.5		
	30	1101.716					3294.7		
	31	1719.9					3423.0		
			F4057	40.47	^	^		45000.0	4.404
			51057	1647	0	0		45300.9	1461
	ļ	OC Limit	n/a	2050m3/da	iy			n/a	n/a

Notes:

(1) These readings have been calculated by subtracting the flows read at the rapid infiltration site, from the flows read on the main meter in the Chlorine Booster Station. Both the irrigation flows and the rapid infiltration flows travel through this meter.

(2) These flows are read at two, 2 inch water meters located at the rapid infiltration site.

	[Hig	gh Lift Stati	on		Chlorir	ne Booster St	tation	
		Daily	Total	Monthly		Rapid	Total	Total	Monthly
		Flow	Monthly	Average	Irrigation	Infiltration	Daily	Monthly	Average
June		m3/day	m3/day	m3/day	m3/day (1)	m3/day (2)	m3/day (3)	m3/day	m3/day
	1	1618.571					3567.9		
	2	1601.5					2816.4		
	3	1731.669					798.5		
	4	2760.5					354.3		
	5	1625.562					1096.6		
	6	1057.628					1352.4		
	7	1638.7					1016.7		
	8	1724.8					2641.9		
	9	1881.776					2112.3		
	10	1860.773					1099.1		
	11	3095.4					1115.7		
	12	2042.912					2071.9		
	13	1110.281					1864.7		
	14	1944.561					896.6		
	15	1991.27					1233.9		
	16	1951.2					1097.1		
	17	2098.769					357.8		
	18	2997.305					805.6		
	19	2752.965					849.9		
	20	548.7798					828.1		
	21	2128.4					1179.4		
	22	2195.717					2213.1		
	23	2306.448					2418.5		
	24	1638.6					2488.8		
	25	3573.8					3047.8		
	26	2167.519					3244.6		
	27	1338.82					3918.2		
	28	1804.3					4179.2		
	29	2077.204					3509.1		
	30	2049.95					3920.2		
	31			Γ					
			50040	4077		^		50000 0	4007
			59316	1977	0	0		58096.0	1937
	ļ	OC Limit	n/a	2050m3/da	iy			n/a	n/a

Notes:

(1) These readings have been calculated by subtracting the flows read at the rapid infiltration site, from the flows read on the main meter in the Chlorine Booster Station. Both the irrigation flows and the rapid infiltration flows travel through this meter.

(2) These flows are read at two, 2 inch water meters located at the rapid infiltration site.

		Hig	gh Lift Stati	on		Chlorin	e Booster St	tation	
		Daily	Total	Monthly		Rapid	Total	Total	Monthly
		Flow	Monthly	Average	Irrigation	Infiltration	Daily	Monthly	Average
July		m3/day	m3/day	m3/day	m3/day (1)	m3/day (2)	m3/day (3)	m3/day	m3/day
	1	1559.0					3377.8		
	2	3562.0					3842.9		
	3	2668.568					3607.2		
	4	694.6					3031.2		
	5	2142.587					1125.9		
	6	2135.311					1662.8		
	7	2055.617					2732.0		
	8	2211.448					1052.6		
	9	3370.6					1348.2		
	10	2725.181					3099.3		
	11	193.8879					2952.8		
	12	2062.2					3066.3		
	13	2068.192					3190.0		
	14	1998.993					3385.3		
	15	2208.4					3513.1		
	16	3403.6					3684.2		
	17	2188.697					3539.7		
	18	902.3621					4271.7		
	19	1812.158					4408.4		
	20	2109.1					4703.0		
	21	2078.3					3960.3		
	22	1983.7					4460.3		
	23	3300.367					3895.9		
	24	2302.933					4750.7		
	25	404.8539					4475.7		
	26	2132.968					4706.0		
	27	1939.0					4796.9		
	28	2144.009					3625.6		
	29	1883.4					5016.2		
	30	3179.415					3760.0		
	31	2680.7					4500.7		
									0-
			66102	2132	0	0		109542.7	3534
	ļ	OC Limit	n/a	2050m3/da	ıy			n/a	n/a

Notes:

(1) These readings have been calculated by subtracting the flows read at the rapid infiltration site, from the flows read on the main meter in the Chlorine Booster Station. Both the irrigation flows and the rapid infiltration flows travel through this meter.

(2) These flows are read at two, 2 inch water meters located at the rapid infiltration site.

	Hig	gh Lift Stati	on		Chlorir	ne Booster St	tation	
	Daily	Total	Monthly		Rapid	Total	Total	Monthly
	Flow	Monthly	Average	Irrigation	Infiltration	Daily	Monthly	Average
August	m3/day	m3/day	m3/day	m3/day (1)	m3/day (2)		m3/day	m3/day
1	195.8					4399.1		
2	2143.401					4411.8		
3	2242.8					3612.6		
4	1758.003					3855.2		
5	2123.641					4594.9		
6						3857.3		
7	2011.511					3722.2		
8						4111.3		
9						3532.3		
10						2916.7		
11	1977.031					2666.7		
12	2024.1					2755.5		
13	3026.6					2737.6		
14	1822.93					2774.7		
15	1041.58					2885.6		
16	1636.316					3508.5		
17	1892.8					2896.3		
18						3577.6		
19	1873.577					3418.4		
20						2536.6		
21						2770.0		
22	1046.466					2526.5		
23						2550.9		
24						1275.6		
25						1950.6		
26						2586.3		
27	2901.8					2305.9		
28						2847.7		
29						3510.1		
30						2654.6		
31	1807.6					3863.2		
		56953	1837	0	0		97612.3	3149
	OC Limit	n/a	2050m3/da	ıy			n/a	n/a

Notes:

(1) These readings have been calculated by subtracting the flows read at the rapid infiltration site, from the flows read on the main meter in the Chlorine Booster Station. Both the irrigation flows and the rapid infiltration flows travel through this meter.

(2) These flows are read at two, 2 inch water meters located at the rapid infiltration site.

(3) These are the flows that have been read at the main meter located in the Chlorine Booster Station.

[Hig	gh Lift Stati	on		Chlorin	e Booster St	ation	
	Daily	Total	Monthly		Rapid	Total	Total	Monthly
	Flow	Monthly	Average	Irrigation	Infiltration	Daily	Monthly	Average
September	m3/day	m3/day	m3/day	m3/day (1)	m3/day (2)		m3/day	m3/day
1	1918.467					2595.8		
2	1931.993					2744.3		
3	2726.8					2682.4		
4	1795.605					2480.5		
5	895.6871					3205.5		
6	1642.2					2868.4		
7	1585.93					3762.6		
8	1687.9					2465.1		
9	2044.291					3155.6		
10	2712.32					3863.5		
11	1772.498					2942.7		
12	918.8271					3003.1		
13	1972.3					3111.0		
14	1516.9					1896.9		
15	1897.7					577.5		
16	1687.238					883.2		
17	2684.2					1119.2		
18	2044.193					630.1		
19	506.3978					560.1		
20	1604.252					1151.8		
21	1722.011					2240.3		
22	1626.707					1674.0		
23	1592.7					2119.4		
24	2669.345					2585.5		
25	1846.845					1148.6		
26	695.2					202.5		
27	1643.9					1262.6		
28	1599.769					2524.1		
29	1713.201					2297.1		
30	1639.769					1835.2		
31								
		52295	1743	0	0		63588.6	2120
l	OC Limit	n/a	2050m3/da	ay			n/a	n/a

Notes:

(1) These readings have been calculated by subtracting the flows read at the rapid infiltration site, from the flows read on the main meter in the Chlorine Booster Station. Both the irrigation flows and the rapid infiltration flows travel through this meter.

(2) These flows are read at two, 2 inch water meters located at the rapid infiltration site.

(3) These are the flows that have been read at the main meter located in the Chlorine Booster Station.

	Hig	gh Lift Stati	on		Chlorir	ne Booster St	ation	
	Daily	Total	Monthly		Rapid	Total	Total	Monthly
	Flow	Monthly	Average	Irrigation	Infiltration	Daily	Monthly	Average
October	m3/day	m3/day	m3/day	m3/day (1)	m3/day (2)		m3/day	m3/day
1	2562.6					2472.3		
2	1807.135					541.7		
3	872.2425					181.3		
4	1685.043					900.8		
5	1602.4					2005.6		
6	1716.97					1896.5		
7	1683.317					2154.9		
8	2460.724					1523.7		
9	1699.803					650.8		
10	353.0723					186.4		
11	1578.404					927.2		
12	1679.513					2071.2		
13	1587.9					1968.6		
14	1594.8					2172.1		
15	2412.36					2134.2		
16	1641.5					1534.7		
17	700.4676					896.8		
18	1627.665					181.9		
19	1580.247					0.0		
20	1677.4					188.4		
21	1486.988					0.0		
22	2285.519					176.8		
23	1599.108					0.0		
24	749.3624					180.0		
25	1651.5					0.0		
26	1596.79					181.2		
27	1551.764					248.5		
28	1653.463					3.3		
29	2529.6					0.0		
30	1711.5					0.0		
31	461.0731					0.0		
		10000	4000				05050 0	
		49800	1606	0	0		25378.9	819
	OC Limit	n/a	2050m3/da	ау			n/a	n/a

Notes:

(1) These readings have been calculated by subtracting the flows read at the rapid infiltration site, from the flows read on the main meter in the Chlorine Booster Station. Both the irrigation flows and the rapid infiltration flows travel through this meter.

(2) These flows are read at two, 2 inch water meters located at the rapid infiltration site.

(3) These are the flows that have been read at the main meter located in the Chlorine Booster Station.

	Hi	gh Lift Stati	on		Chlorin	e Booster St	tation	
	Daily	Total	Monthly		Rapid	Total	Total	Monthly
	Flow	Monthly	Average	Irrigation	Infiltration	Daily	Monthly	Average
November	m3/day	m3/day	m3/day	m3/day (1)	m3/day (2)	m3/day (3)	m3/day	m3/day
1	1530.7							
2	1637.889							
3	1543.609							
4	1716.013							
5	2538.908							
6	1683.0							
7	698.5471							
8	1657.704							
9	1533.597							
10 11	1549.351 1632.9							
12	2607.48							
12	1740.456							
14	545.2021							
15	1505.828							
16	1653.0							
17	1554.7							
18	1626.277							
19	2532.194							
20	1971.952							
21	216.7694							
22	1512.202							
23	1512.4							
24	1588.285							
25	1588.7							
26	2605.49							
27	1640.265							
28	428.439							
29	1624.4							
30	1597.211							
31								
		47770	1500				0.0	
	OC Limit	47773 n/a	1592 2050m3/da	0	0		0.0 n/a	#DIV/0! n/a
		II/a	2030113/08	iy			11/a	11/a

Notes:

(1) These readings have been calculated by subtracting the flows read at the rapid infiltration site, from the flows read on the main meter in the Chlorine Booster Station. Both the irrigation flows and the rapid infiltration flows travel through this meter.

(2 & 3)

These are the flows that have been read at the main meter located in the Chlorine Booster Station.

]	Hig	gh Lift Stati	on		Chlorin	e Booster St	ation	
	Daily	Total	Monthly		Rapid	Total	Total	Monthly
	Flow	Monthly	Average	Irrigation	Infiltration	Daily	Monthly	Average
December	m3/day	m3/day	m3/day	m3/day (1)	m3/day (2)	m3/day (3)	m3/day	m3/day
1	1575.535							
2	1512.3							
3	2523.5							
4	1534.311							
5	661.4756							
6	1590.8							
7	1622.4							
8	1559.313							
9	1565.197							
10	2694.0							
11	1645.944							
12	627.0884							
13	1666.862							
14	1601.591							
15	1619.8							
16 17	1587.108							
18	2377.046 1480.64							
10	459.2425							
20	1640.1							
20	1611.191							
22	1579.401							
23	1669.757							
24	2625.653							
25	1644.602							
26	612.2							
27	1989.339							
28	2037.169							
29	1705.635							
30	1616.445							
31	2941.07							
		51577	1664	0	0		0.0	#DIV/0!
	OC Limit	n/a	2050m3/da	ay			n/a	n/a

Notes:

(1) These readings have been calculated by subtracting the flows read at the rapid infiltration site, from the flows read on the main meter in the Chlorine Booster Station. Both the irrigation flows and the rapid infiltration flows travel through this meter.

(2 & 3)

These are the flows that have been read at the main meter located in the Chlorine Booster Station.

	High Lift	t Station		Chlorine Boc	ster Station	
	Total	Monthly		Rapid	Total	Monthly
	Monthly	Average	Irrigation	Infiltration	Daily	Average
	m3/day	m3/day	m3/day (1)	m3/day (2)	m3/day (3)	m3/day
Jan	49176	1586	0	0	0	
Feb	39874	1595	0	0	0	
Mar	48657	1570	0	0	4425.5507	143
Apr	50131	1617	0	0	31368.883	1046
May	51057	1647	0	0	45300.949	1461
Jun	59316	1977	0	0	58095.98	1937
Jul	66102	2132	0	0	109542.74	3534
Aug	56953	1837	0	0	97612.251	3149
Sep	52295	1743	0	0	63588.614	2120
Oct	49800	1606	0	0	25378.897	819
Nov	47773	1592	0	0	0	
Dec	51577	1664	0	0	0	
Total	622711		0	0	435313.87	
Average	1706				1193	

TOWN OF OLIVER Summary of Monthly Sewer Flows

Notes:

- (1) These readings have been calculated by subtracting the flows read at the rapid infiltration site, from the flows read on the main meter in the Chlorine Booster Station. Both the irrigation flows and the rapid infiltration flows travel through this meter.
- (2) These flows are read at two, 2 inch water meters located at the rapid infiltration site except during the non-irrigation season when the rapid infiltration readings are read from the meter located in the Chlorine Booster Station.
- (3) These are the flows that have been read at the main meter located in the Chlorine Booster Station.

TOWN OF OLIVER
PE-13717 - Effluent Sampling - Cell #3, prior to storage reservoir - EMS ID E222151

		BOD5							
		Carbonac							
	Date	eous	TSS	Nitrate	Nitrite	Phosphate	Nitrate & Nitrite	Nitrogen	Nitrogen
OC Limit			60 mg/L	(as N)	(as N)	(as P)	(as N)	(Total)	(Organic)
Units			mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L
Frequency		monthly	monthly	semi-annually	semi-annually	semi-annually	semi-annually	semi-annually	semi-annually
January	10	17.4	12.8						
February	1	17.4	8.7						
March	1	14.5	16.1						
March	1			0.266	0.037	3.86	0.304	33.30	2.38
March	1					2.12			
April	4	18.5	18.4						
May	2	8	5.3						
June	7	<7.1	23.7						
July	4	<8.4	10						
August	2	7.7	16						
September	6			4.31	1.61		5.92	5.92	
September	6					1.26			
September	6	<7.0	13						
October	3	<6.2	<4.0						
November	9	10	14.7						
December	5	15.3	11.3						

PE - 13717 - Influent Sampling - Equalization Basin - EMS ID E222152 Influent Sampling

Semi- Annual

Ammonia	Kjeldahl	Phosphorus	Phosphorus
Total (as N)	,	Total (as P)	Total Dissolved
mg/L	mg/L	mg/L	mg/L
semi-annually	semi-annually	semi-annually	semi-annually
30.60	33.00	4.63	4.56
			6.88
			6.01

APPENDIX D

Reclaimed Water Storage Reservoir Level, Flow & Volume Calibration Curve

TOWN OF OLIVER

RECLAIMED WATER USE BY CUSTOMER (Readings in m3)

LOCATION	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014	2015	2016	2017	2018	2019	2020	2021	2022
AIRPORT	221400.0	238400.0	203100.0	161600.0	131800.0	201050.0	147688.3	153841.2	185686.70	124891.7	115743.3	98510.9	101779.8	99601.3	69142.8	19567.0	32276.3	28254.4
	4 40 4 5	4.4405	17005	47000	40045	40044.0	40000 70	4 4 0 0 7 0 0	10150.01	45000.4	4.405.4.00	4 40 40 07	40000.07	40054.47	40000 40	47400 75	40004 44	40005 50
CEMETERY	14015	14125	17325	17000	18215	13311.2	16338.73	14607.36	19159.94	15996.1	14354.03	14843.27	13399.67	12651.17	16986.46	17498.75	18291.44	18335.58
PUBLIC WORKS YARD	7720	12535	7580	5575	5795	6155.8	5163.96	6408.64	7085.72	7393.22	7380.1	8094.8	8340.74	6260.65	5939.63	8319.96	5387.7	6103.28
103 STREET PARK	4555	9255	7090	5280	6345	5377.24	6232.1	6621.86	8051.37	8749.04	7647.12	8359.52	1030.6*	5927.68	8858.46	1244.97	11676.42	8089.04
SOSS										48457	4873.58	0	1.55	0	25743.75	27419.66	24693.89	8545.39
ALONSO						3495.31	1670.9	7014.59	6714.65	3892.74	3850.51	2364.03	2498.39	1794.43	9240	6012.39	0	0
HUGGINS						15536.5	3787.05	2872.33	1290.33	meter off	8554.16	0	0	0	4614.7	0	0	0

Other Users Not Metered:

- Fairview Mountain Golf Course

- Fairview Park (new 2015)

*103 STREET PARK 2021 value amended from 8576.02 to 11676.42

TOWN OF OLIVER STORAGE RESERVOIR LEVEL DATA

	JANU	JARY	FEBR	UARY	MAR	RCH	AP	RIL
		VOLUME IN		VOLUME IN		VOLUME IN		VOLUME IN
DAY	ELEVATION	STORAGE*	ELEVATION	STORAGE*	ELEVATION	STORAGE*	ELEVATION	STORAGE*
1								
2								
3								
4		240,000					445.76	358,000
5								
5 6 7			444.00	000 000	445.00	000 000		
			444.69	292,000	445.26	333,000		
8 9								
10	444.1	252,000						
10	444.1	202,000					445.72	356,000
12							440.72	000,000
13								
14			444.83	303,000	445.49	344,000		
15						-		
16								
17	444.24	261,000						
18								
19							445.57	348,000
20					445 70			
21					445.72	356,000		
22 23								
23								
25	444.41	273,000					445.49	344,000
26	1 1 7.7 1	210,000					110.40	011,000
27			444.98	315,000				
28			445.1	322,000	445.74	357,000		
29								
30								
31	444.54							

* Volume in Storage above Elevation 439.00 Elevation 439.00 is minimum 60 day average operating level

	MA	λΥ	JU	NE	JU	LY	AUG	UST
		VOLUME IN		VOLUME IN		VOLUME IN		VOLUME IN
DAY	ELEVATION	STORAGE*	ELEVATION	STORAGE*	ELEVATION	STORAGE*	ELEVATION	STORAGE*
1							443.79	231,000
2 3	445.47	343,000						
4					444.85	305,000		
5								
6			445.25	332,000				
							440 44	200,000
5 6 7 8 9	445.48	344,000					443.44	209,000
10		344,000						
11					444.81	301,000		
12					101	301,000		
13			445.17	327,000				
14								
15							443.24	197,000
16		344,000						
17								
18								
19					444.49	279,000		
20			445.25	332,000				
21								
22							443.02	183,000
23		0.40,000						
24		342,000						
25 26								
20			445.11	322,000				
28			440.11	522,000				
29							442.87	174,000
30		335,000						,
31								

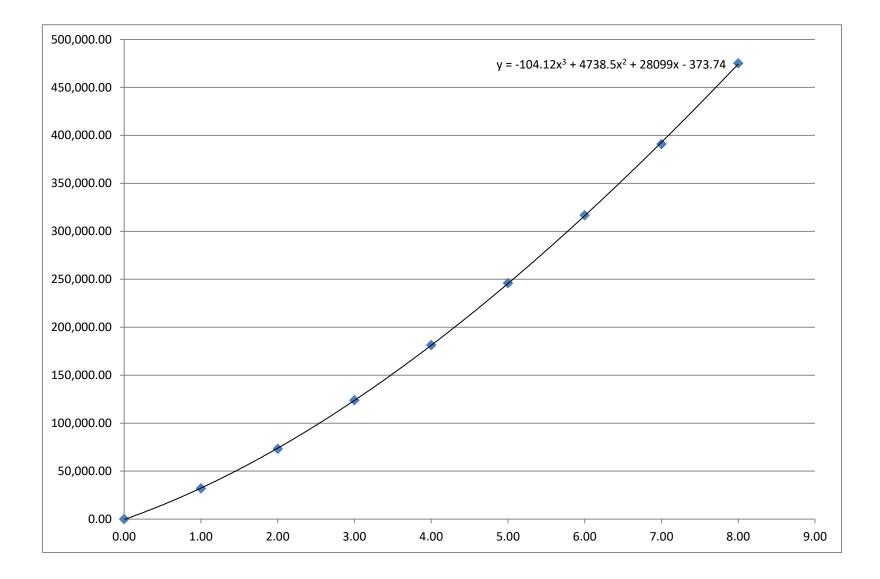
* Volume in Storage above Elevation 439.00 Elevation 439.00 is minimum 60 day average operating level

	SEPTE	MBER	ОСТО	DBER	NOVE	MBER	DECE	MBER
		VOLUME IN		VOLUME IN		VOLUME IN		VOLUME IN
DAY	ELEVATION	STORAGE*	ELEVATION	STORAGE*	ELEVATION	STORAGE*	ELEVATION	STORAGE*
1 2 3 4 5 6 7	442.62	161,000	442.31	140,000			443.55	217,000
8 9 10 11 12 13 14 15	442.4	126,000	442.30	140,000	443.10	189,000	443.71	226,000
13 16 17 18 19 20 21 22 23			442.23	136,000	443.26	198,000	443.82	233,000
23 24 25 26 27 28 29 30 31	442.36	144,000	442.36 442.77	144,000	443.44	209,000	444.05	249,000

* Volume in Storage above Elevation 439.00 Elevation 439.00 is minimum 60 day average operating level

Town of Oliver - Effluent Storage Reservoir - Volume Capacity

Reservoir Elevation (m)	Elevation above 439.0m	Total Operating Storage (cu. m.)	Calculated Volume (m ³)	% Difference from Measured
439.00	0.00	0.00	-373.74	N/A
440.00	1.00	32,000.00	32359.6	1%
441.00	2.00	73,300.00	73945.14	1%
442.00	3.00	124,000.00	123758.16	0%
443.00	4.00	181,600.00	181173.94	0%
444.00	5.00	246,000.00	245567.76	0%
445.00	6.00	316,800.00	316314.9	0%
446.00	7.00	391,000.00	392790.64	0%
447.00	8.00	475,200.00	474370.26	0%



APPENDIX E

Irrigation Plan



TOWN OF OLIVER

9

AUG



Reference: 66483

AUG 0 6 2002 Her Worship Mayor Linda Larson and Councillors Town of Oliver PO Box 638 Oliver BC V0H 1T0

Dear Mayor Larson and Councillors:

I am pleased to inform you that the update to the Town of Oliver's Liquid Waste Management Plan (LWMP) is hereby approved in principle in accordance with section 18 of the *Waste Management Act.*

I recognize that your LWMP update was rather complicated and required the concerted efforts of your staff and your consultant to complete. I commend your efforts and those of your consultant and wish you well in the continued implementation of your LWMP.

The implementation and administration of the LWMP will require resolution of details involving financial, engineering, operational and administrative elements, and I request that you continue to work closely with ministry staff on plan implementation details. I am sending a copy of this letter to my colleague, the Minister of Community, Aboriginal and Women's Services (formerly Municipal Affairs), the Honourable George Abbott so that he is aware of my support for your funding request for the continued implementation of this plan.

Best regards,

Joyce Murray

/Joy∕ce Murr'ay Minister

CC:

The Honourable George Abbott, Minister of Community, Aboriginal and Women's Services

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we all a point front house of participations

Ministry of Water, Land and Air Protection Office of the Minister

Mailing Address: Parliament Buildings Victoria BC V8V 1X4 OPIES BH

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FULL

WMI

COMMENTS



December 13, 2018

Our File: 306-088-005

Ministry of Environment & Climate Change Strategy 102 Industrial Place Penticton, B.C. V2A 7C8

Attn: Regional Waste Manager

Dear Sir/Madam:

RE: Town of Oliver – Update to Reclaimed Water Irrigation Plan - OC PE-13717

The Town of Oliver requests approval from the Ministry for expansion of their reclaimed water irrigation system as authorized in Operational Certificate PE-13717. The current works authorized within this Operational Certificate are outlined in Site Plan A, dated December 14, 1995. The areas include:

Location	Legal Description
Fairview Mountain Golf Course	Lot 1, Plan KAP62023, DL2450S, SDYD
Alonso	Lot A, Plan KAP37929, Sec 12, Township 54, SDYD
Huggins	Lot 3, Plan KAP5881, Sec 12, Township 54, SDYD

The Town requests authorization for expansion of the irrigation system. The expansion areas are shown in Figure 1 enclosed herein. They are identified as Reclaimed Water Irrigation Expansion Areas (2006). Their location and legal descriptions of the expansion areas are as follows.

Location	Legal Description				
High School Park	 Lot 2H, DL 2450S, SDYD, Townsite of Oliver Southern portion of Block C, DL 2450S, SDYD, Irrigation Lateral SRW shown on PL 330, Lot 2G BLF52 on Oliver Townsite map 				
Fairview Park	 Lot 2J, DL 2450S, SDYD, Townsite of Oliver Block 34, DL 2450S, SDYD, Townsite of Oliver, Incl Closed Rd PL B7567 				
Oliver Secondary School	Block 32, Plan KAP4297, DL 2450S, SDYD				
Public Works	Lot 2, Plan KAP54258, DL 2450S, SDYD				
Airstrip	Lot 2, Plan KAP38137, DL 2450S, SDYD				
Cemetery	Lot 1, Plan KAP 24065, DL 2450S, SDYD, Portion L 203A				

.../2

Total reclaimed water use is measured by a flow meter located at the booster station, adjacent to the reclaimed water storage reservoir. Meters have also been installed at the Cemetery, Airport, Public Works Yard, Alonso Property, Southern Okanagan Secondary School, High School Park and Huggins Property for the purposes of measuring total reclaimed water use at each location. There is no flow meter on the irrigation service to the Fairview Mountain Gold Course. Usage is calculated as the total annual irrigation, less all other metered usage. Annual reporting of the irrigated areas will be consistent with the reporting requirements as outlined in PE-13717 and include the total usage, crop type, irrigated area, irrigation application rate, and irrigation period.

Groundwater monitoring plans are established for the airport and Fairview Mountain Gold Course sites, the two largest users of reclaimed water. Sampling data is included in annual reporting.

As per the operational certificate, no reclaimed wastewater will be applied to the ground any closer than 15 metres from the edge of flowing streams or bodies of water. Additionally, no reclaimed wastewater is irrigated within 30 metres of any well or inground reservoir for domestic supply.

Should questions arise or for additional information, please do not hesitate to contact the undersigned.

Yours truly,

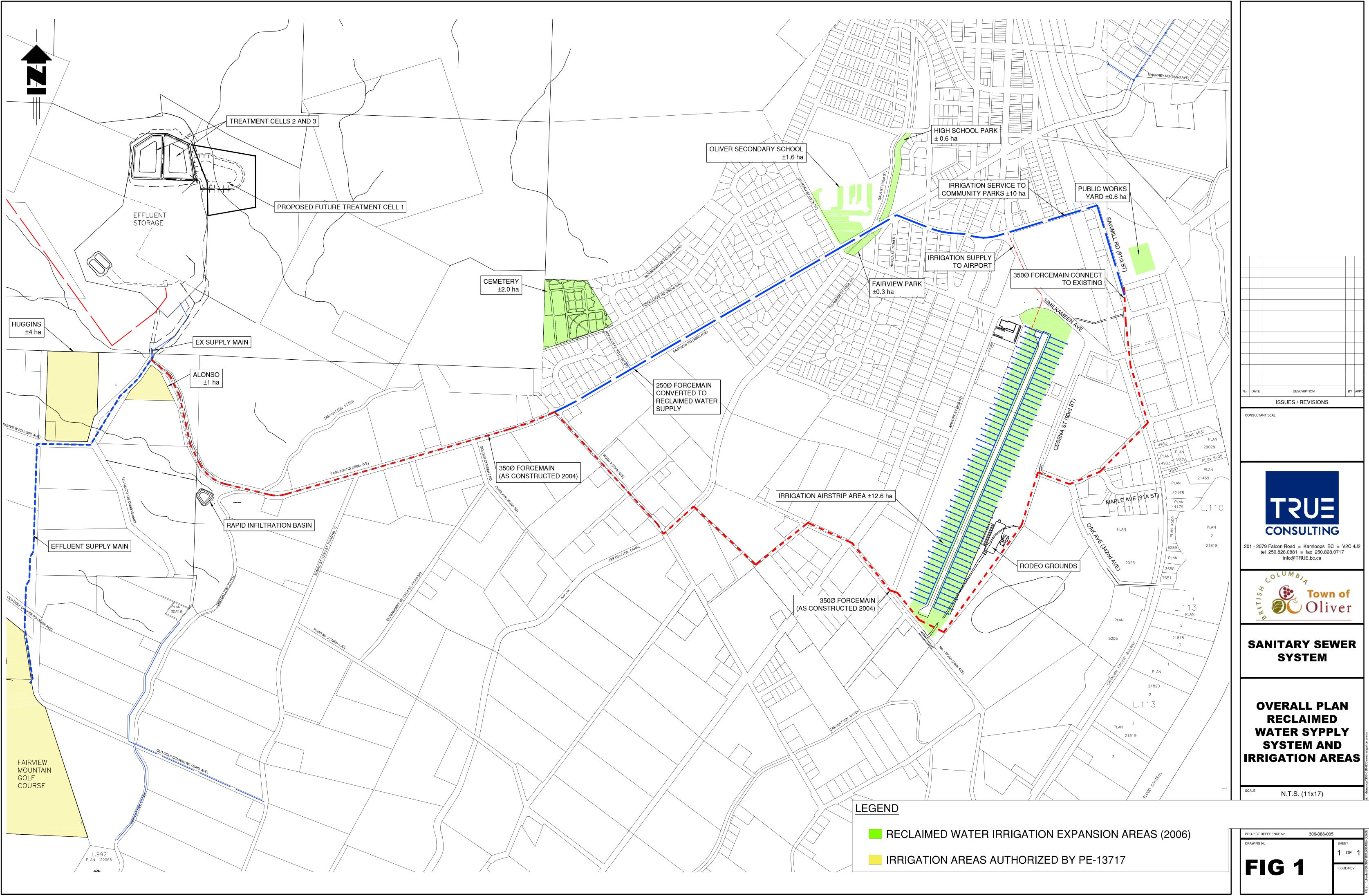
TRUE CONSULTING

Steve Underwood, P. Eng.

Enclosures

NA/

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January 17, 2019

Our File: 306-088-005

Ministry of Environment & Climate Change Strategy 102 Industrial Place Penticton, B.C. V2A 7C8

Attn: Jen Pape, Environmental Protection Officer, Municipal Liquid Waste

Dear Ms. Pape:

RE: Town of Oliver – Irrigation Area Expansion Notification - OC PE-13717

In response to your email dated January 10, 2018, the following supplemental information is provided to support the Update to Reclaimed Water Irrigation Plan submitted to the Ministry on December 13, 2018.

- 1. The Town currently provides treated reclaimed water to the Alonso and Huggins vineyards for irrigation purposes. The Huggins service is turned off, but this service provides a backup source to the user in the event of a drought period. Both vineyards use drip irrigation to water crops. There are no supplemental food crops in the irrigation area.
- 2. The following drawings of the Town of Oliver Effluent Infiltration Basin are enclosed herein:
 - a. General Location Map (Dwg. No. 306-1201-05)
 - b. Effluent Infiltration Basin Plan and Profile (Dwg. No. 306-1322-03)

Should questions arise or for additional information, please do not hesitate to contact the undersigned.

Yours truly,

TRUE CONSULTING

Vatalie alter

Natalie Alteen, EIT

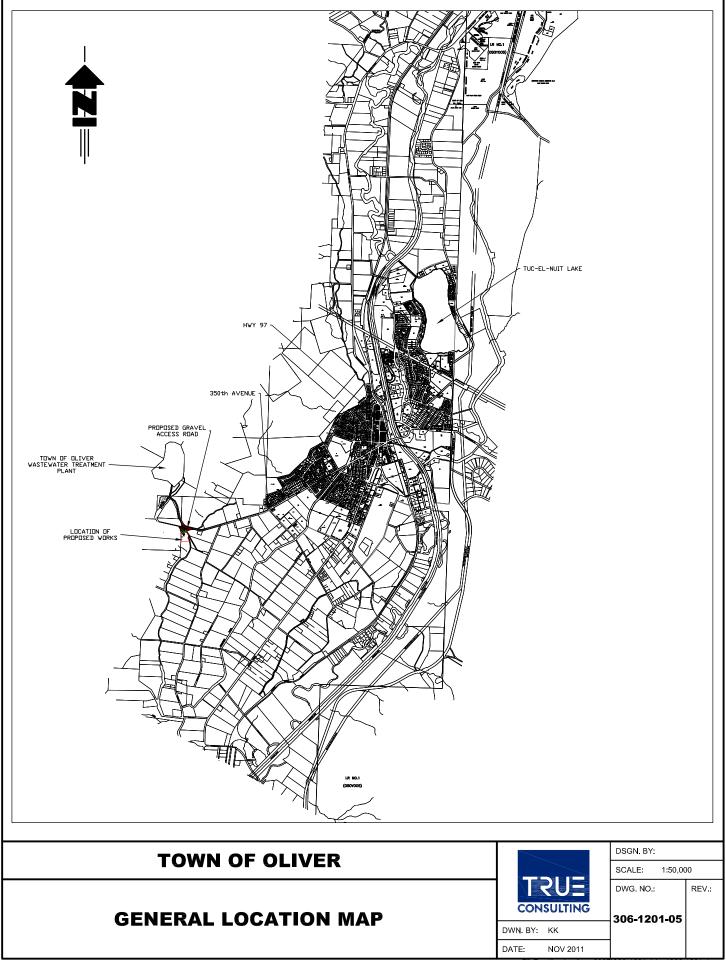
Enclosures

NA

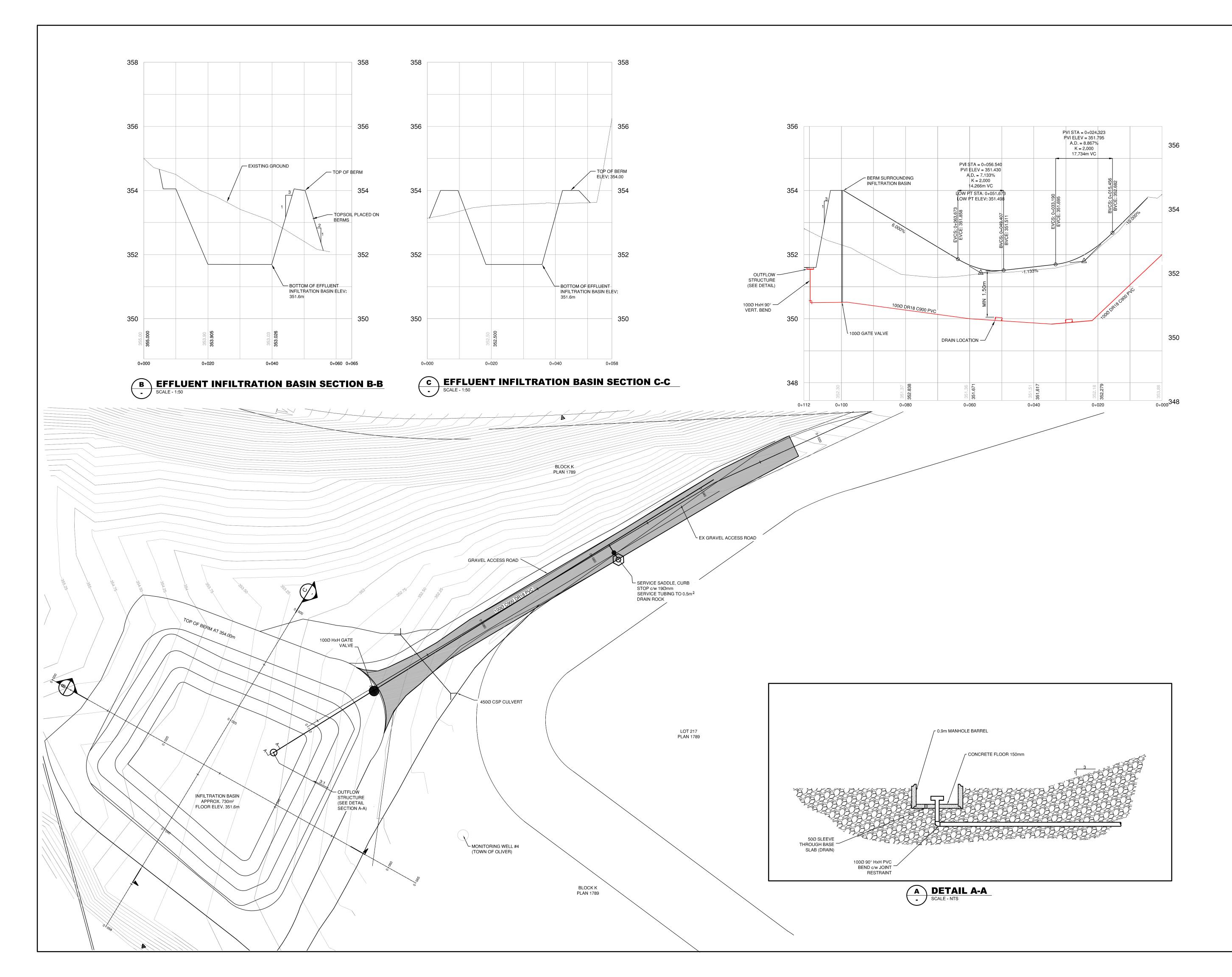
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201-2079 Falcon Road Kamloops BC V2C 4J2 www.true.bc.ca tel 250.828.0881 fax 250.828.0717

ENGINEERING ■ PLANNING ■ URBAN DESIGN ■ LAND SURVEYING



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February 25, 2020

Our File: 306-088-007

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Ministry of Environment and Climate Change Strategy 102 Industrial Place Penticton, B.C. V2A 7C8

Attn: Jen Pape, Environmental Protection Officer, Municipal Liquid Waste

Dear Ms. Pape:

RE: Town of Oliver – Update to Reclaimed Water Irrigation Plan – OC-PE-13717

The Town of Oliver submitted an approval request to the Ministry for expansion of their reclaimed water irrigation system as authorized in Operational Certificate ("OC") PE-13717 on December 13, 2018 (please see attached). This letter serves as a notification for additional expansion.

CURRENT WORK AUTHORIZED WITHIN PE-13717 (ISSUED: DECEMBER 14, 1995)

Works authorized within the OC, as described in Site Plan A of the permit, are outlined in the Table 1.

TABLE 1 AUTHORIZED WORKS WITHIN OC PE-13717 SITE PLAN A (DATED DECEMBER 14, 1995)

Location	Legal Description
Fairview Mountain Golf Course	Lot 1, Plan KAP62023, DL2450S, SDYD
Alonso	Lot A, Plan KAP37929, Sec 12, Township 54, SDYD
Huggins	Lot 3, Plan KAP5881, Sec 12, Township 54, SDYD

As described in the response letter submission to the Ministry on January 17, 2019 (please see attached), the Alonso and Huggins properties utilize reclaimed water irrigation for their vineyards. The Huggins service is turned off but provides a backup source to the user in the event of a drought period. Both vineyards utilize drip irrigation to water crops and there are no supplemental food crops in the irrigation area.

EXPANSION AREA NOTIFICATION (DECEMBER 13, 2018)

On December 13, 2018, the Town requested authorization for expansion of the irrigation system as described in Table 2. These areas are currently being irrigated.

Location	Legal Description;
Gala Street Linear Park	Lot 2H, DL 2450S, SDYD, Townsite of Oliver; Southern portion of Block C, DL 2450S, SDYD, Irrigation Lateral SRW shown on PL 330, Lot 2G BLF52 on Oliver Townsite map
Fairview Park	Lot 2J, DL 2450S, SDYD, Townsite of Oliver; Block 34, DL 2450S, SDYD, Townsite of Oliver, Incl Closed Rd PL B7567
South Okanagan Secondary School	Block 32, Plan KAP4297, DL 2450S, SDYD; Block 48, Plan KAP2507, DL2450S, SDYD
Public Works	Lot 2, Plan KAP54258, DL 2450S, SDYD
Oliver Municipal Airport	Lot 2, Plan KAP38137, DL 2450S, SDYD
Cemetery	Lot 1, Plan KAP 24065, DL 2450S, SDYD, Portion L 203A

TABLE 2 PROPSED EXPANSION AREA BY TOWN IN NOTIFICATION TO MINISTRY (DATED DECEMBER 13, 2018)

EXPANSION AREA NOTIFICATION

The Town wishes to notify the Ministry of an expansion to the South Okanagan Secondary School irrigation area. This irrigated area has increased from \pm 1.6 ha to \pm 5.4 ha as show on Figure 1-1 enclosed herein.

SYSTEM METERING

To date, total reclaimed water use is measured by a flow meter located at the booster station, adjacent to the reclaimed water storage reservoir. To measure total reclaimed water use at each location meters have been installed at the Cemetery, Oliver Municipal Airport, Public Works Yard, Alonso Property, Southern Okanagan Secondary School, Gala Street Linear Park, Huggins Property and most recently at Fairview Park.

There is no flow meter on the irrigation service to the Fairview Mountain Golf Course therefor usage is calculated as the total annual irrigation, less all other metered usage. Annual reporting of the irrigated areas is consistent with the reporting requirements as outlined in PE-13717 and include the total usage, crop type, irrigated area, irrigation application rate, and irrigation period.

GROUNDWATER MONITORING

Groundwater monitoring plans are established for the airport and Fairview Mountain Golf Course sites, the two largest users of reclaimed water. Sampling data is included in annual reporting.

As per the operational certificate, no reclaimed wastewater will be applied to the ground any closer than 15 metres from the edge of flowing streams or bodies of water. Additionally, no reclaimed wastewater is irrigated within 30 metres of any well or inground reservoir for domestic supply.

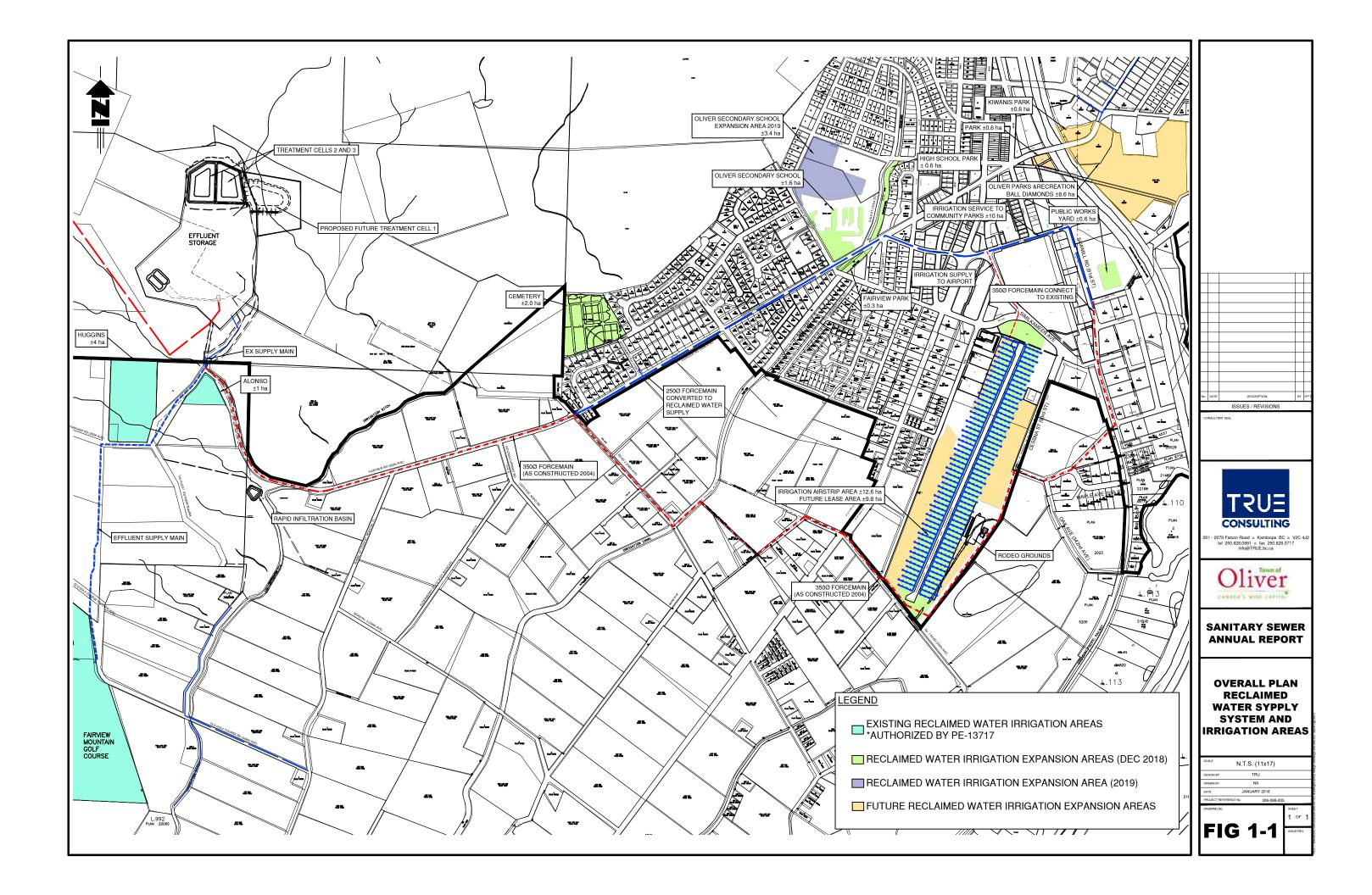
Should questions arise or for additional information, please do not hesitate to contact the undersigned.

Yours truly,

TRUE CONSULTING

Vatalie Alter

Natalie Alteen, EIT



APPENDIX F

Yearly Precipitation Data

Seasonal Precipitation Summary

Oliver STP)							SEASON TOTAL (mm)
YEAR	APR	MAY	JUNE	JULY	AUG	SEPT	OCT	
1992	41.4	8.0	64.8	62.0	9.8	2.2	11.8	200.0
1993	50.6	34.5	48.0	67.9	39.5	18.4	14.8	273.7
1994	42.4	30.8	37.8	12.2	33.9	17.4	24.8	199.3
1995	17.5	17.9	37.6	10.2	22.6	7.5	10.6	123.9
1996	15.8	62.2	27.9	24.2	5.2	52.3	28.2	215.8
1997	35.3	41.8	87.9	47.6	18.5	63.4	29.0	323.5
1998	29.4	79.1	31.2	25.1	12.3	2.9	33.7	213.7
1999	20.1	28.9	40.3	15.5	44.1	1.2	11.7	161.8
2000	10.4	24.8	25.8	26.7	4.5	14.4	19.6	126.2
2001	37.6	16.4	39.4	32.2	15.0	13.6	24.1	178.3
2002	8.7	43.0	4.8	9.8	0.3	9.4	7.3	83.3
2003	29.4	18.4	12.9	0	0.0	11.4	21.7	93.8
2004	27.9	30.7	56.0	7.8	27.7	32.3	48.9	231.3
2005	12.4	41.1	48.4	2.9	1.3	2.9	22.4	131.4
2006	20.8	52.0	36.0	14.2	0.1	8.7	12.4	144.2
2007	4.9	3.2	24.1	29.0	2.8	12.2	11.6	87.8
2008	5.0	3.65	27.5	5.0	19.9	2.7	9.9	73.7
2009	4.8	26.8	13.4	28.6	27.8	20.2	39.5	161.1
2010	20.0	55.9	68.3	14.6	9.1	38.9	13.7	220.5
2011	12.5	69.6	24.4	18.7	0.0	3.4	22.4	151.0
2012	39.9	14.8	78.7	46	0.3	2	40.8	222.5
2013	16.5	30.5	35.0	8.6	36.6	47.5	5.6	180.3
2014	15.3	24.4	42.8	25	12.2	19.3	35.9	174.9
2015	2.2	54.4	13.2	17	19.9	3	26.3	136.0
2016	5.8	14.9	38.5	25.9	1.2	16.4	62.8	165.5
2017	40.5	61.2	21.2	0	0.0	4.8	5.3	133.0
2018	50.4	31.3	53.2	31.4	1.5	9.4	33.1	210.3
2019	8.0	3.7	6.9	10.4	6.1	80.9	11.1	127.1
2020	20.5	57.6	61.3	7.9	2.8	5.8	30.2	186.1
2021	1.8	2.0	17.6	4.6	2.9	7	32	67.9
2022	5.3	29.1	45.8	29.3	10.0	5.4	2.6	127.5
Avg.	21.1	32.7	37.8	21.3	12.5	17.3	22.7	165.3

1992 to 1996 data from Environment Canada 1997 - present data compiled from Town of Oliver daily records

APPENDIX G

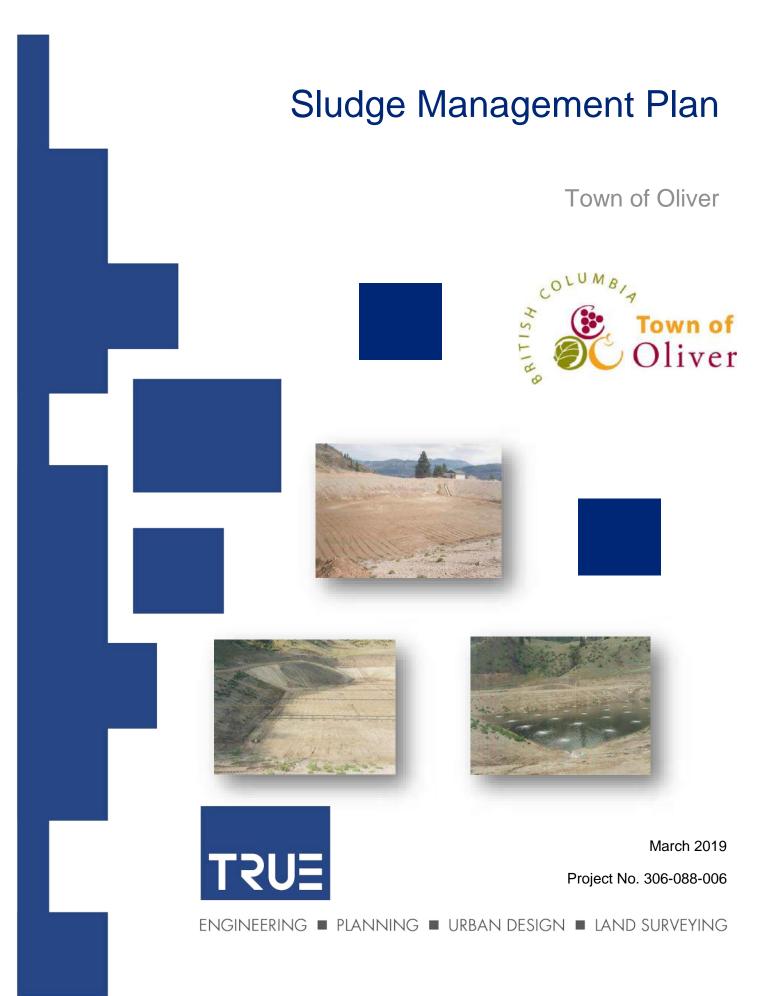
Sludge Monitoring (Quality) Data and Management Plan

TOWN OF OLIVER PE-13717 - Effluent Sludge - Cell #2

ANALYTICAL REPORT - Sampled on

				WALP Gu	idelines	
		CELL 2 EFF	Agricultural	Agricultural	Retail	Retail
Parameter	Unit	SLUDGE-1	Low Grade	High Grade	Low Grade	High Grade
Aluminum	ug/g					
Antimony	ug/g					
Arsenic	ug/g	10.3	75	75	75	75
Barium	ug/g					
Beryllium	ug/g					
Bismuth	ug/g					
Cadmium	ug/g	2.19	25	20	20	5-20
Calcium	ug/g					
Chromium	ug/g	41.9				
Cobalt	ug/g	3.33	150	150	150	150
Copper	ug/g	1710				
Iron	ug/g					
Lead	ug/g	47.7	1000	500	500	500
Magnesium	ug/g					
Manganese	ug/g					
Mercury	ug/g	4.12	10	5	5	5
Molybdenum	ug/g	23.2	20	20	20	20
Nickel	ug/g	22.7	200	180	180	180
Phosphorus	ug/g					
Potassium	ug/g					
Selenium	ug/g	13.4	14	14	14	14
Silver	ug/g					
Sodium	ug/g					
Strontium	ug/g					
Tellurium	ug/g					
Thallium	ug/g					
Tin	ug/g					
Titanium	ug/g					
Vanadium	ug/g					
Zinc	ug/g	1080	2500	1850	1850	1850
Zirconium	ug/g					
		-				

Total Solids	%	8.5
Volatile Solids	%	41.9



Distribution List

# of Hard Copies	PDF Required	Association / Company Name
1	1	Town of Oliver
	1	Ministry of Environment
1	1	TRUE Consulting

Revision Log

Revision #	Revised by	Date	Issue / Revision Description
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Report Submission

Report Prepared By:

Report Reviewed By:

Vatleen

Natalie Alteen, ElT Project Engineer

R DERWOOD Terry Underwood, P. Eng. Project Engineer Mar 13 / 2019

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SLUDGE MANAGEMENT PLAN TOWN OF OLIVER – MARCH 2019

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APPENDICES

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List of Acronyms

BC MOE	British Columbia Ministry of Environment,
OC	Operational Certificate
OCP	Official Community Plan
OMRR	Organic Matter Recycling Regulation
TRUE	TRUE Consulting

Units of Measure

ft	feet
km	kilometre
L/d	Litres per day
L/m	Litres per minute
L/s	Litres per second
lpcd	Litres per capita per day
m	metre
mg/L	milligrams per Litre
mm	millimetre
NTU	Nephelometric Turbidity Units
psi	pounds per square inch
USgpm	US gallons per minute

Referenced Reports

Lambourne Environmental	"Lagoon Survey Report for Town of Oliver Cells 1 & 2," December 2011
Canadian Council of Ministers of the Environment	"Guidance Document for the Beneficial Use of Municipal Biosolids, Municipal Sludge and Treated Septage," 2012
TRUE Consulting	"Sanitary Sewer System 2017 Annual Report," February 2018



1.0 Background

The wastewater treatment facility for the Town of Oliver has been in operation since 1965. From 1965 to 1984, the Town operated a treatment plant for municipal wastewater and discharged treated effluent to the Okanagan River. In response to regulatory agency requirements for reduced phosphorus loadings to surface water courses in the Okanagan River Basin, the Town constructed effluent storage and land disposal systems in the Fairview area in 1983 and 1984. Since 1985, the Town has utilized treated effluent in the Fairview area with the principle end user of treated effluent being the Fairview Mountain Golf Course. In 1995, a two-cell aerated lagoon system was constructed in the Fairview area (see Figure 1).

The existing treatment facility is comprised of influent screening, equalization storage, a two-cell aerated lagoon treatment system, winter effluent storage, chlorination contact chamber and reclaimed water irrigation.

In accordance with the Town of Oliver's Operation Certificate (OC) No. PE-13717 issued under the provisions of the Waste Management Act, the Town has prepared a Sludge Management Plan as it relates to the wastewater treatment facility. This document outlines the monitoring, management and beneficial use of the Town's municipal biosolids.

2.0 Characterization of Sludge

The Town of Oliver's wastewater collection system is generated primarily from residential and commercial buildings. The sludge is comprised of a mixture of fecal matter, organic and inorganic materials. Trace amounts of heavy metals, solvents, and petroleum products may enter the system as a result of municipal activities.

Source control initiative are imperative as they ensure the wastewater treatment facility functions properly, operator health and safety are protected, and the quality of treated effluent/biosolids is maintained. This mandate is included in the Town's Official Community Plan (OCP) Bylaw 1370, which prioritizes public awareness for potential groundwater contamination and health hazards related to the discharge of toxic substances into the municipal drainage system.



3.0 Sludge Sampling and Monitoring Program

3.1 System Design

Effluent is pumped from the equalization basins to the aerated lagoon Cells No. 2 and No.3 via the High Lift Station. Biological degradation and sedimentation of suspended solids is a primary function of the aerated lagoons system. Treatment is accomplished through the stabilization of organic wastes by bacteria and algae. Waste products include carbon dioxide (CO₂), ammonia and phosphates.

The aerated lagoon treatment system is comprised of two treatment cells, with aeration allowing for microbial degradation of organic material. Effluent enters Cell No.2 and then proceeds to secondary treatment in Cell No.3.

Cell No.2 provides primary digestion of influent. As such, sludge accumulates around the perimeter of the cell in the low current areas. This material sinks to the bottom of the cell, forming a sludge blanket. The capacity of Cells No.2 and No.3 are as follows. Each lagoon has a maximum operating depth of 5.3 m.

Cell No.3

Cell No.2				
Surface Area at FWL 11,000 m ²				
Storage Volume 37,600 m ³				

Surface Area at FWL 10,100 m² Storage Volume 38,200 m³

Anaerobic degradation occurs in areas with low dissolved oxygen and sunlight. Anaerobic bacteria produce water, carbon dioxide, nutrients, ammonia, alkalinity, hydrogen sulfide and methane as waste products.

On this basis, solids accumulations will occur in the aerated lagoons and require removal from the system. Excessive solids accumulations in the cells may result in odours, visible masses of floating solids on the lagoon surface, reduced detention time and degraded effluent quality.

The rate at which solids accumulate in the aerated cells and the point at which accumulations may significantly impair the operation of the system varies. Piping and other design provisions have been made for a future third cell construction east of the existing lagoons (see Figure 2).

Overall, the Operational Certificate for the system required the Town of Oliver to develop a strategy or plan to ultimately deal with sludge accumulations in the aerated cells. The OC specifies the following limits:

- Discharge rate 2,200 m³/day
- 5 Day Biochemical Oxygen Demand 45 mg/L
- Total Suspended Solids 60 mg/L





3.2 Theoretical Sludge Production Rates

Sludge accumulation rates within the system are dependent on the following variables:

- Amount of suspended solids entering the system in the raw sewage. Influent suspended solids to the treatment system are reduced as the influent is screened prior to entering the aerated lagoons.
- Operating temperature. As sludge accumulates on the floor of each cell, anaerobic digestion processes occur. This results in volatile solids removal and corresponding reductions in accumulated solids volume and mass. The digestion process is temperature dependent. Recognizing the geographic location of Oliver and generally "hot" summer weather conditions, anaerobic digestion processes on the floor of the cells represent a mechanism for significant sludge volume and mass reductions.
- Hydraulic load to the system and residence time.
- Sludge characteristics and compression. As sludge accumulates on the bottom of the lagoons, compression of the actual sludge mass will occur. This results in higher solids concentrations expressed as a % solids. Literature suggests that compression mechanisms are time and characteristic dependent.

Recognizing that influent is screened, there are favorable conditions for in-pond anaerobic digestion. The cells are adequately sized to allow for associated compression processes and there is no chemical addition to the system. Therefore, sludge accumulation within the lagoon cells is expected to be lower that other systems within the region.

A theoretical sludge accumulation rate calculation is presented herein. This rate is based on an assumed sludge production rate of 0.2 kg/kg of BOD removal. This sludge production rate is typical of extended aeration treatment plants in which digestion processes represent a mechanism for internal sludge quantity reductions:

	Influent BOD Loading Average Influent Flow Total BOD Daily Loading	180 mg/L 2000 m³/d 360 kg/d	
Cell No. 2	Average BOD removal Cell #2- 70% Theoretical Sludge Production- 250 Sludge Volume/day= 50 kg @ 10% Sludge Volume/year	x 0.2	250 kg/d 50 kg/d 0.50 m ³ /d 182 m ³ /yr
Cell No. 3	Average BOD removal Cell #3- 70% Theoretical Sludge Production- 80 x Sludge Volume/day= 16 kg @ 10% Sludge Volume/year	0.2	80 kg/d 16 kg/d 0.16 m ³ /d 60 m ³ /yr

The preceding calculations suggest that the sludge accumulation rate in Cell No.2 will occur at a rate at least three times greater than Cell No.3. This has been shown in accumulation surveys and described in Section 4.0.



3.3 Monitoring Methods

Sludge accumulation are to be measured by direct and indirect monitoring as described herein.

3.3.1 Direct Monitoring

Direct sludge monitoring should be undertaken every two years. It is important that sampling is completed at the same time each year. In this manner, inaccuracies related to temperature dependent digestion process will be eliminated. September or October are suggested as the most appropriate periods to undertake a sludge accumulation survey.

The primary objective is to define the amount of sludge accumulation by probing the cell bottom and recording the apparent sludge thickness and location on a plan of the lagoon system. Each successive monitoring activity should attempt to probe approximately the same locations to assist in the determination of the accumulation rate.

Anticipated primary areas of sludge accumulation will be in the general vicinity of the inlet piping in the relatively quiescent areas between air diffusers. Sludge will generally not accumulate in the vicinity of the aerators.

The design depth of the lagoons (5.3m) will make in-cell measurements of sludge accumulation less than straightforward. Sludge accumulation measurements may be simplified to some extent by lowering the operating levels of Cells No.2 and No.3 by lowering the slide gate in hydraulic structure S-3. Lowering of operating levels should be undertaken on a gradual basis.

Any deviation from normal operation (i.e. lowering of operating levels) will require notification and approval of the Ministry of Environment.

3.3.2 Indirect Monitoring

Indirect Monitoring of sludge accumulation can be accomplished via analysis of treated effluent water quality. If treated effluent water quality exceeds the permitted discharge concentration limits, assessment of the sludge accumulation depth is triggered.

3.4 Sludge Sampling

Which final disposal method for sludge removed from the lagoons will be dependent on the characteristics of the sludge and require approval from the MOE. To enable evaluation of sludge disposal options and to support a proposal/plan submission for approval to the MOE, it is recommended that a minimum of two sludge samples be taken during accumulation surveys for physical and chemical analysis.



Samples may be obtained by a pipe-type probe or at depth samplers. Analysis of the sludge samples should include the following parameters:

% solids % volatile solids Fecal Coliform* Arsenic Cadmium Chromium Cobalt	MPN/g* (mg/kg)* (mg/kg)
Copper Mercury	(mg/kg) (mg/kg)
Molybdenum	(mg/kg)
Nickel	(mg/kg)
Lead Selenium	(mg/kg) (mg/kg)
Zinc	(mg/kg)
*On a dried weight basis	

All parameters listed above should be analyzed during the initial phases of the sludge monitoring program. As data is compiled some parameters may be identified as not representing a concern, and in consultation with the MOE, the scope of the analysis accordingly reduced.

The chemical and physical characteristics of the final sludge product will be a major factor in determining the disposal method which will be acceptable to the MOE. The Town must follow the Organic Matter Recycle Regulation (OMRR) process and quality criteria for the desired end use of the bioldoids.

3.5 Sludge Removal

Sludge accumulation monitoring will provide data on when scheduling of sludge removal should be undertaken. Excessive sludge accumulations have the potential to significantly impact the performance of the system. Conditions that suggest accumulated sludge may be negatively impacting the system will be evident in the south-east corner area of Cell No 2, in the vicinity of the influent pipe. Indicators of excessive sludge accumulations in the area may include:

- Black color of wastewater
- Low dissolved oxygen concentrations
- Floating sludge masses
- Localized odours
- What appears to be "air bubbles" covering the lagoon surface during warm weather periods.



Sludge removal options which may be considered by the Town include the use of specialized equipment while the system is in operation, or alternatively draining of the cell for removal using excavation equipment. Equipment that can be utilized include: a float or barge mounted "dredge" type pump, floating discharge line, and on-shore portable sludge dewatering system.

The second approach involves cell draining and removal using excavation equipment. Utilization of this approach related to Cell No.2 is described herein.

3.5.1 Cell No.2 Draining Procedure

The procedure to drain Cell No.2 for sludge removal with a reduced water content is described as follows:

 Lower the operating level of Cells No.2 and No.3 by gradually lowering the overflow weir gate in hydraulic structure S-3. This procedure should be undertaken over a 3 to 5 week period. When complete, the adjustable slide gate in hydraulic structure S-3 will be in the fully down position.

IMPORTANT NOTE: Lowering of the operating level of the system is required to reduce the hydraulic head difference across the common berm between the cell to be drained and the cell remaining in operation. Failure to reduce the system operating level as described herein may result in localized instability and soil slumping at the toe of the slope of the common berm in the drained cell.

- ii. The system should then be operated in the Cell No.2 bypass mode.
- iii. The air supply to the aeration system in Cell No.2 should be shut off by closing isolation valves on the air header. Cautionary aspects related to the aeration system include:
 - Ensure air flow to diffuser units remining in service do not exceed the manufacturer's recommended maximum per unit flow.
 - Confirm blower operation remains within the accepted operation range specified by the manufacturer.

Operation of the aeration system with partial flow release to the pressure relief valve on the blower discharge piping may be necessary to maintain operation of the aeration system in Cell No.3 within ranges specified by both the blower and aeration system manufacturer.

- iv. Reduce the operating level in Cell No.2 by opening valve V-5. Opening of valve V-5 will enable partial draining of Cell No.2, by gravity, to the winter effluent storage reservoir. Valve V-5 should be gradually opened such that the drop in liquid level in Cell No.2 does not exceed 150 mm per day.
- v. Set up portable pumping equipment and completed draining of Cell No.2. Ideally, the discharge from the drainage pump will be directed into the Cell No.3 side chamber of hydraulic structure S-2. In this manner, contents from Cell No.2 will be provided treatment in Cell No.3 prior to discharge into the storage reservoir. Care



should be given to ensure the discharge piping is securely fastened to hydraulic structure S-2.

CAUTION: During draining operation of Cell No.2, simply pumping the contents across the common berm with the discharge piping laid on the berm is not recommended. The pump discharge, in this case, could result in serious erosion and localized instability of the exposed and/or submerged berm slope in Cell No.3.

Locating the pump at the north end of Cell No.2 is recommended to minimize operational problems associated with sludge plugging the pump suction and/or sludge being drawn into the pump and simply relocated to Cell No.3.

- vi. Upon completion of draining, allow the exposed sludge accumulation to air dry. The period necessary for air drying is difficult to estimate. An air-drying period of at least one month should be anticipated in the schedule planning of the desludging operation. The objective of the drying period is to reduce the water content of accumulated sludge, thereby making removal by excavation equipment more straightforward.
- vii. Disconnect air feeder lines from laterals and remove from the lagoon. Temporary caps should be placed on cell lateral outlets to prevent sludge or other foreign material from entering the lateral piping.

CAUTION: Care is essential to ensure foreign material does not enter the lateral piping when the air feeder lines are removed. If foreign material ends up in the lateral piping, it will be carried after reassembly by air flowing into the diffusers, leading to clogging.

While the lagoon cell is drained, the aeration system should be thoroughly inspected and any corroded or "suspect" components replaced. Replacement of the air diffuser membranes and ropers to the retrieval floats is straightforward with the cell drained and should be scheduled to be done concurrent with the desludging operation.

viii. Remove accumulated sludge from Cell No.2. The most appropriate equipment required for the removal operation will be determined on-site based on the apparent water content of the material and the actual amount and location of the accumulations in the cell.

The preceding procedure would be followed in reverse to return the cell to service after desludging. In reassembling the aeration system, the manufacturer's design details should be complied with in terms of connection fittings and anchor locations. It is important that the actual diffuser units be installed at the same level within tolerances recommended in the manufacturer's Operation and Maintenance Manual. The lagoon cell should be filled to "just submerge" all aeration components at which time all laterals should be air tested by carefully partially opening ("cracking") isolation valves on the air supply header.



CAUTION: The aeration system in Cell No.2 should not be returned to normal operation by opening of the isolation valve on the air header until the wastewater elevations in Cells No.2 and No.3 are equal.

3.6 Sludge Disposal

In British Columbia, the quality and beneficial use of biosolids for land application and composting is regulated under the Organic Matter Recycling Regulation (OMRR). This regulation applies to the construction and operation of composting facilities, as well as the production, distribution, storage, sale and use or land application of biosolids and compost.

When planning sludge removal operations, a written notification is to be provided to the Regional Waste Manager at least two weeks prior to the commencement of de-sludging operations. The notification should include the following requirements as outlined in the OMRR:

- An estimate of the total sludge volume based on monitoring data.
- Classification of the biosolids and an overview of the proposed treatment process.
- Analytical characterization derived from sampling data.
- A description of the proposed disposal method.

To a major extent, the analytical characterization of the sludge will determine what disposal options and sites will be acceptable to the Ministry. Compliance with pathogen and metal testing treatment objectives will be required. If the intended use is land application, a Land Application Plan (LAP) must be developed and signed by a Qualified Professional prior to any land application. Information required in this plan is set out in Schedule 7 of the OMRR.

Consistent with the strategy of the Town's wastewater treatment and disposal system, the objective of the sludge disposal method evaluation should be to provide the greatest flexibility possible for beneficial use. Options which may be considered consistent with this objective include:

3.6.1 Class A Biosolid

Composting to result in a Class A biosolid. These biolsolids must meet all of the following requirements:

- Schedule 1, Pathogen Reduction Processes;
- Schedule 2, Vector Attraction Reduction;
- o Schedule 3, Pathogen Reduction Limits;
- Section 3 of Schedule 4, Quality Criteria;
- Schedule 5, Sampling and Analyses-Protocols and Frequency;
- Schedule 6, Record Keeping.

Class A biosolids can be applied in quantities greater than 5 cubic meters per year per parcel of land in accordance with the LAP and the soil substance concentrations specified in Schedule 10.1



of the OMRR. They must only be distributed in volumes that do not exceed 5 cubic meters per vehicle per day. If they are distributed in sealed bags for retail purposes, they are not to exceed 5 cubic meters, with no restrictions on the number of bags distributed per vehicle per day. They may be distributed in volumes greater than 5 cubic metres to composting facilities or biosolids growing medium facilities.

3.6.2 Class B Biosolids

Composting to result in a Class B biosolid. These biosolids must meet all of the following requirements:

- Schedule 1, Pathogen Reduction Processes;
- Schedule 2, Vector Attraction Reduction;
- Schedule 3, Pathogen Reduction Limits;
- o Column 3 of Schedule 4, Quality Criteria;
- Schedule 5, Sampling and Analyses-Protocols and Frequency;
- Schedule 6, Record Keeping.

Class B biosolids must be applied to land in accordance with the LAP, the methodology specified in Schedule 8 and the soil substance concentrations specified in Schedule 10.1 of the OMRR. Class B biosolids may be distributed to composting facilities with no volume restrictions. They may be distributed to a biosolids growing medium facility with no volume restrictions if they meet the pathogen reduction and vector attraction requirements for Class A biosolids. They must not be applied to land in a watershed used as a permitted water supply under the Drinking Water Protection.

3.6.3 Biosolids Growing Medium

Biosolids that meet the requirements of all the following are biosolids growing medium:

- o Column 2 of Schedule 4, Quality Criteria;
- Schedule 5, Sampling and Analyses-Protocols and Frequency;
- Schedule 6, Record-keeping;
- Schedule 11, Requirements for Biosolids Growing Medium.

Biosolids growing medium may be distributed with no volume restriction.

3.6.4 Disposal at the Sanitary Landfill

Sludge can be landfilled with other solid waste or used as a soil conditioner in final cover areas to enhance vegetation growth. Disposal at the landfill with sold waste should be considered as the least preferred option as no benefit is achieved and landfill "air space" is consumed. However, it should be recognized that the quality of the sludge may, in the final analysis, leave the landfill as the only feasible disposal option.



4.0 Recent Sampling

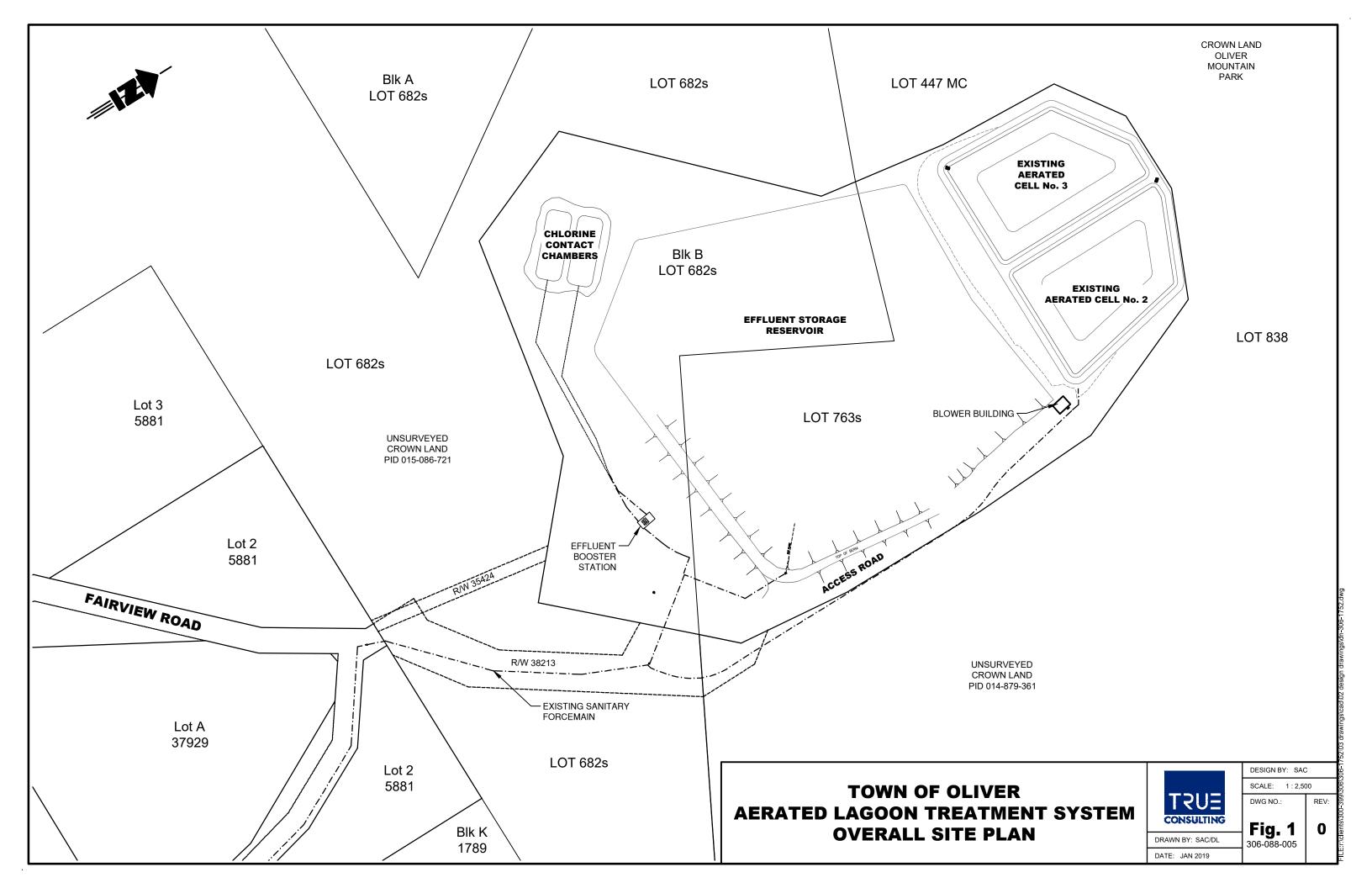
A sludge survey was completed by Lambourne Environmental in 2011 using a digital GPS and gridded sampling programme (see Appendix A). The dry down tell results for Cell No.2 range from 2.97 to 24.13 % solids, whereas Cell No.3 ranges from 3.82 to 7.12 % solids. As derived in theoretical calculations, Cell No.2 has an increased rate of sludge production due to the treatment system design.

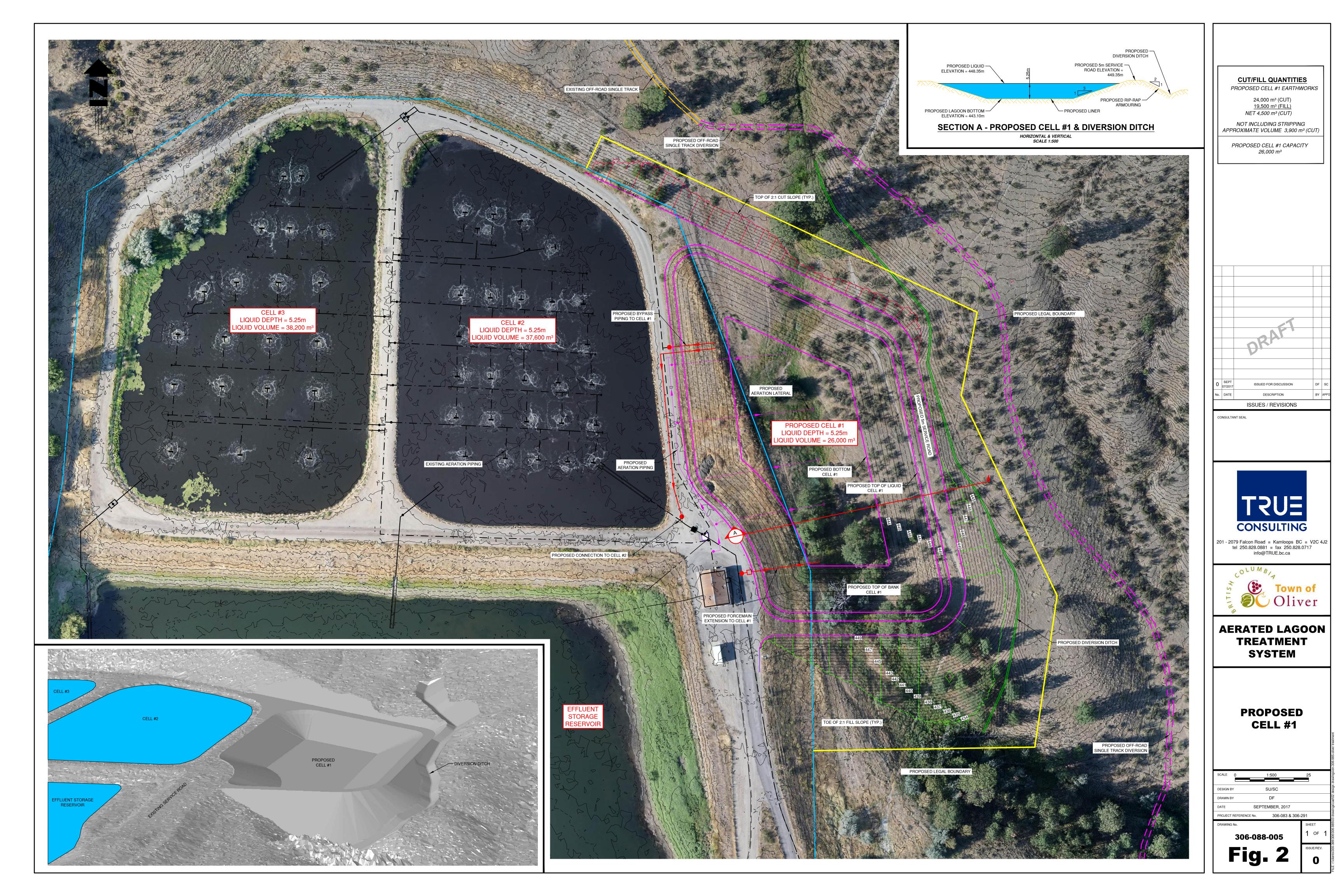
The Town completed sludge sampling in 2017. Following sampling, Cell No.2 was lowered, and sludge was removed around the perimeter of the cell. Sludge accumulation sampling was again completed in 2018.

5.0 Recommendations

As the Town continues to advance their Sludge Management Plan, a reserve fund should be maintained for sludge removal and upgrading of the lagoons as required. Sludge sampling for thickness and density in Cell No.2 and No. 3 is to be completed every 2 years (at a minimum). Ongoing monitoring and maintenance will allow the Town to adapt to increases in population growth and reductions of water resources in a sustainable manner. Options for beneficial reuse of sludge should continue to be explored in the future.







APPENDIX A

Referenced Report



51, 37337 Burnt Lake Trail, Red Deer County, AB T4S 2K5 Ph. (403)348-8298 Fax (403) 348-8290

December 15, 2011

Town of Oliver 35016 - 97 St. PO Box 638 Oliver, BC V0H 1T0 Attn: Shawn Goodsell

Re: Lagoon Survey Report for Town of Oliver, Cells 1 & 2

Dear Shawn,

Lambourne Environmental was contracted to conduct a sludge survey of cells 1 and 2 in Oliver. This survey was completed on November 17, 2011 and was conducted using a digital GPS system, with a boat being used to take the depth measurements and to gather samples from the lagoons. At the time of the survey, the lagoons were ice free and the aeration system had been turned off.

The calculation of volumes for the cells is shown in Table 1 below. The volume calculations were done using Carlson Civil 3D software. While collecting the samples for dry matter testing, it was difficult to find sludge in the second cell. The material in cell 2 was of low density and was found mostly along the east side of the cell. Several attempts to obtain samples in other areas of cell 2 yielded only gravel or stones and dark water. Cell 1 did contain some areas of accumulation and the sludge density varied considerably as seen in the dry down results obtained using our in-house single sample ovens. The majority of the sludge in cell 1 was around the perimeter of the cell indicating the aeration system is moving the material around and it is settling out in the low current area around the perimeter.

When calculating the dry tonnes, we typically see fairly consistent solids results. We take the average of the dry downs and multiply by the sludge volume to arrive at the dry tonnes. In this case, there were a few samples that showed significantly higher solids than the rest of the samples. We retested these samples on different dry down ovens to ensure consistent results. The average number used may skew the calculation of dry tonnes present, particularly in cell 1. The extent of the higher density material was not determined, but it may correspond to the location of the inlets to the cell or it could be material that has not been removed for some time. In the higher density samples, the biosolids did seem to contain a significant inorganic content of sand and grit.

Table 1

Cell #	Total Volume (m ³)	Biosolids Volume (m ³)	Average % solids	Calculated Dry Tonnes	Cell Depth (m)	Biosolids Height (m)
1	36,229	5,000	9.20%	460	5.6	0.1 – 1.95
2	36,278	3,000	5.13%	154	5.5	0 – 2.52
Total	72,507	8,000				

The following are the dry down test results from each cell.

Cell 1				
Sample #	% Solids			
1-1	11.13			
1-2	3.93			
1-3	2.97			
1-4	6.52			
1-5	6.51			
1-6	24.13			

Cell 2				
Sample #	% Solids			
2-1	7.12			
2-2	3.82			
2-3	4.99			
2-4	4.59			

I have also included the following drawing and data exhibits:

- 1. Cell 1 Carlson drawing indicating the lagoon shape and points from where the depth measurements were taken.
- 2. Cell 1 Table indicating the total depth measurements as well as the height of sludge in each location.
- 3. Cell 2 Carlson drawing indicating the lagoon shape and points from where the depth measurements were taken.
- 4. Cell 2 Table indicating the total depth measurements as well as the height of sludge in each location.
- 5. Cell 1 and 2 Drawing indicating where the samples used for determining percent solids were collected from.

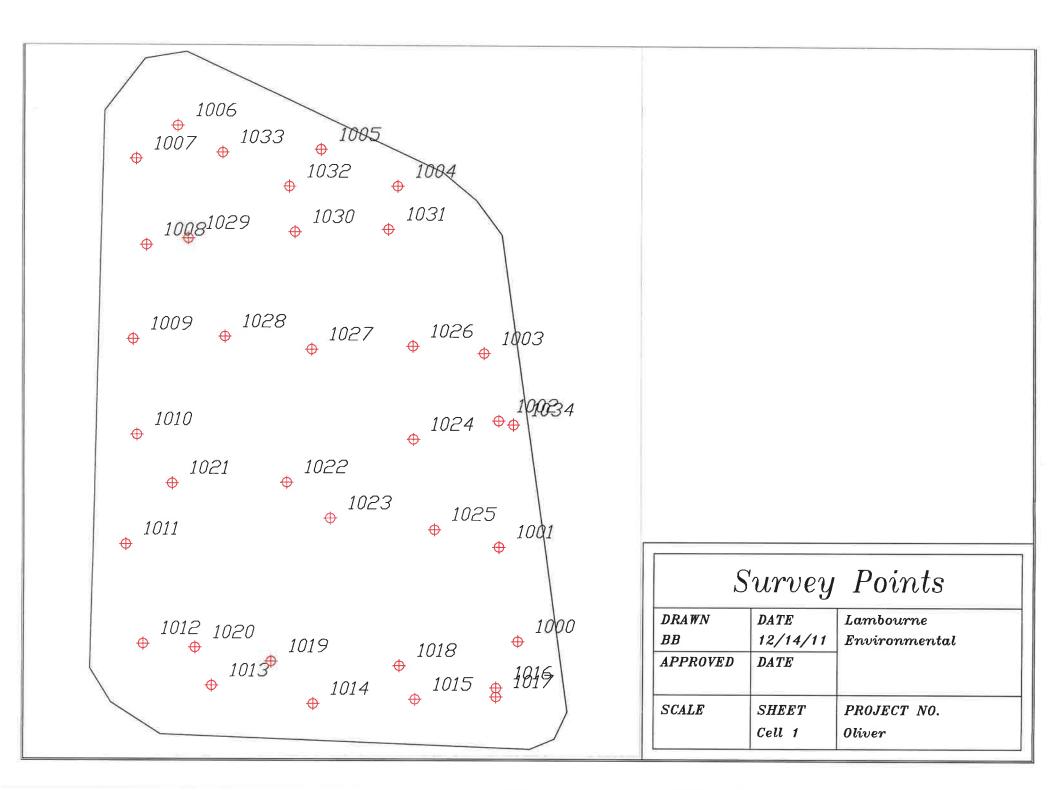
We appreciate the opportunity to work with you on this project. If there is any additional information you require, please let me know.

Yours truly, Lambourne Environmental Ltd.

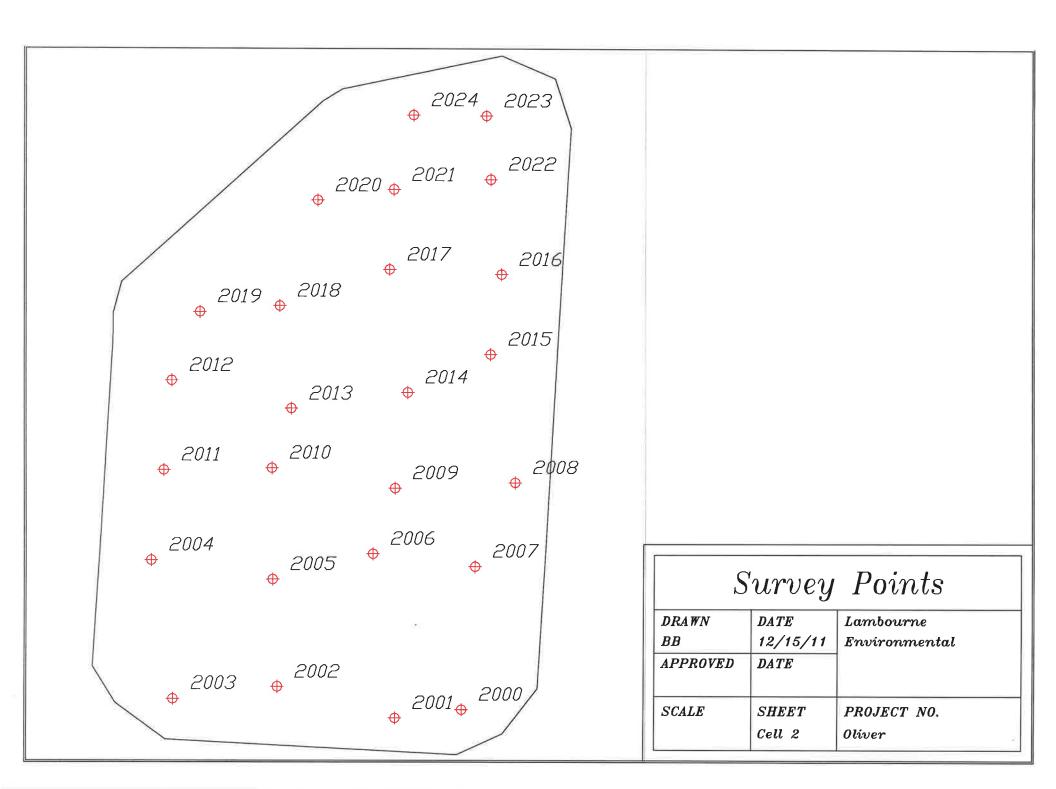
Blair Benn, P. Ag. Vice-President

Encl.

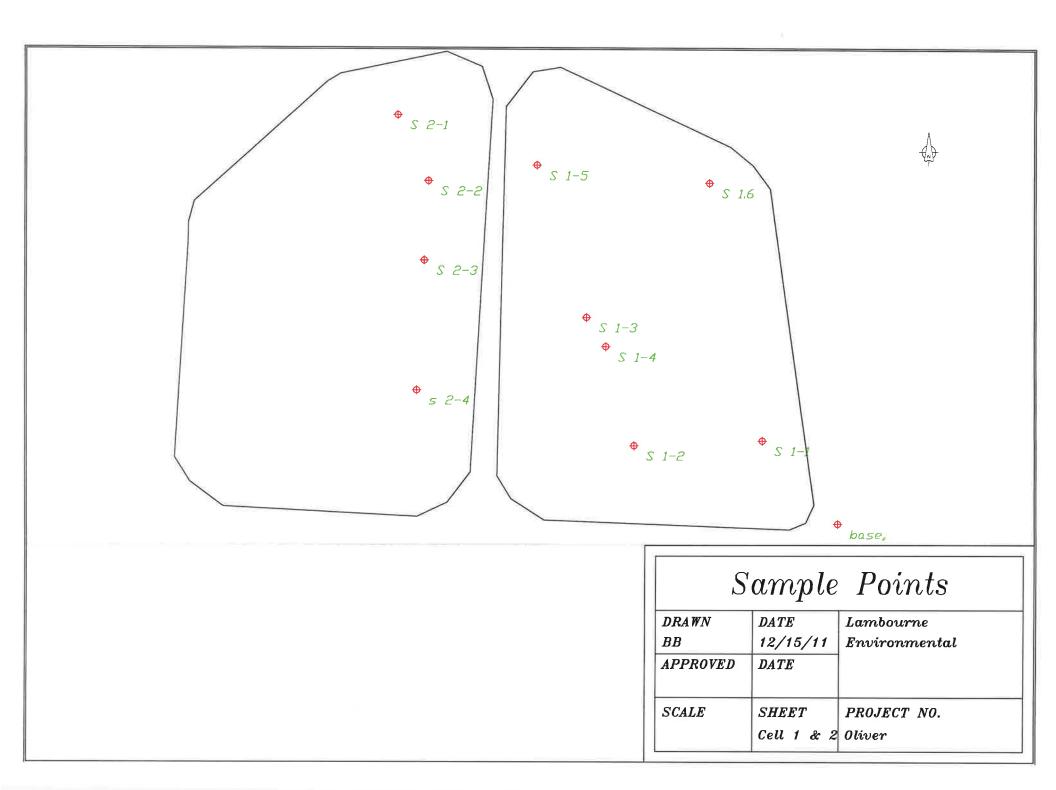
Cc: True Consulting Group Ltd. - Kaitlin Klamut



	Oliver Cell 1						
Point #							
1000	2.64	1.54					
1001	2.86	1.76					
1002	1.87	0.67					
1003	2.00	1.00					
1004	1.60	0.60					
1005	1.72	0.52					
1006	2.76	1.86					
1007	1.53	0.43					
1008	2.18	0.88					
1009	1.54	0.04					
1010	2.06	1.36					
1011	1.46	0.06					
1012	2.12	0.12					
1013	2.54	0.34					
1014	1.71	0.01					
1015	2.22	0.02					
1016	2.72	0.62					
1017	2.46	1.86					
1018	4.18	0.18					
1019	4.35	1.15					
1020	4.37	0.87					
1021	4.58	1.08					
1022	5.50	0.00					
1023	5.50	0.40					
1024	5.67	0.67					
1025	5.43	0.03					
1026	5.61	0.01					
1027	5.46	0.06					
1028	5.42	0.02					
1029	4.55	1.15					
1030	5.45	0.05					
1031	4.75	1.95					
1032	5.13	0.03					
1033	4.91	1.71					
1034	0.97	0.47					



	Oliver				
Point #	Cell 2	Cludge Usight			
	Total Depth	Sludge Height			
2000	1.53	0			
2001	1.84	0			
2002	3.78	0.68			
2003	1.91	0			
2004	3.23	0.03			
2005	5.45	0.55			
2006	5.53	0.63			
2007	4.64	1.34			
2008	2.08	0.00			
2009	5.68	0.08			
2010	5.54	0.04			
2011	3.67	0.00			
2012	3.58	0.58			
2013	5.64	0.04			
2014	5.67	0.37			
2015	4.84	1.84			
2016	3.64	0.54			
2017	5.55	0.05			
2018	4.81	0.00			
2019	3.14	1.14			
2019	1.70	0.00			
2020	5.75	0.25			
2021	4.72	2.52			
2022	3.17	1.17			
2023	3.32	0.42			



APPENDIX H

2021 Western Water Associates Well Installation Report and Hydrogeological Review

WWAL Project: 20-046-01VR



January 28, 2021

Town of Oliver c/o TRUE Consulting Ltd. 201-2079 Falcon Road, Kamloops, B.C. V2C 4J2

Attn: Natalie Alteen, EIT

Re: Hydrogeological Review of the Town of Oliver Reclaimed Wastewater Irrigation Groundwater Monitoring Program

Western Water Associates Ltd. (WWAL) is pleased to provide this hydrogeological review of the Town of Oliver's (the Town) reclaimed wastewater irrigation groundwater monitoring program. The Town has been utilizing reclaimed wastewater to irrigate several properties since the mid 1980's and the wastewater treatment and reclaimed water irrigation is permitted by the Ministry of Environment (ENV) under Operational Certificate PE-13717 (last amended 1995).

1.0 PROJECT BACKGROUND

The Town of Oliver collects wastewater from the community and pumps it to two aerated lagoons for treatment. The operational certificate requires that effluent in the treatment lagoons meet 45 mg/L BOD₅ and 60 mg/L Total Suspended Solids (TSS) criteria before the treated effluent is transferred to a storage lagoon. The results of monthly sampling provided in previous annual monitoring reports indicates that these criteria are typically met.

Between 1997 and 2019, annual effluent flows into the treatment lagoons ranged from 625,911 m³ to 829,413 m³.

Treated wastewater is stored over the winter in the storage lagoon. In the spring through fall, the stored treated wastewater is disinfected and beneficially reused as reclaimed irrigation water at several properties inside and outside the Town of Oliver boundary, and this has been occurring since the mid-1980s. Properties originally permitted to be irrigated with reclaimed under PE-13717 water include the Fairview Mountain Golf Course, the Huggins and Alonso properties.

Over time, the Town has expanded irrigation to additional lands, and plans to further expand this land base in the future (see attached figures). Over the years irrigation was expanded to include:

- Fairview Park,
- Gala Street Linear Park,
- South Okanagan Secondary School,
- the Town's Public Works Yard,
- lands surrounding the Oliver Municipal Airport, and
- the Cemetery.

The Town received Ministry approval by letter to irrigate the above-listed areas in May 2020. Future expansion of the irrigated area at the airport is proposed, as is irrigation of the Oliver Parks and Recreation Ball Diamonds, Kiwanis Park and another small park, all along or east of the Okanagan River. TRUE Consulting's Figure 1-1 (attached) illustrates the illustrates where and how irrigation has expanded to over time.

Total annual reclaimed water use for irrigation has been fairly constant between 2011 and 2019, ranging from approximately 407,000 m³ to 504,000 m³. The Fairview Mountain Golf Course is the largest consumer of reclaimed irrigation water, using 50-70% of the total volume in a given year. The airport is the second largest consumer of reclaimed water using approximately 15-25% of the annual total.

Table 1-10 below summarizes 2019 reclaimed water quality testing results which provide an indication of the water quality being used for irrigation.

	Fecal Coliforms	Total Coliforms	Total P	Total N	Chloride	Sodium	Free CL Res
OC Limit	<2.2 MPN/100 ml	n/a	n/a	n/a	n/a	n/a	n/a
Unit	MPN/100ml	MPN/100ml	mg/L	mg/L	mg/L	mg/L	mg/L
April 15, 2019	<2.2	<2.2	4.6	22.2	143	99.2	0.19
May 6, 2019	<2.2	<2.2	4.99	23.8	157	112	0.35
June 11, 2019	<2.2	<2.2	5.1	22.5	162	121	0.35
July 2, 3019	<2.2	<2.2	4.02	20.3	168	111	0.4
August 12, 2019	<2.2	<2.2	4.49	14.5	171	113	0.32
September 3, 2019	<2.2	<2.2	4.27	13.3	170	120	0.23
October 2, 2019	<2.2	<2.2	4.41	13.9	166	111	0.1

TABLE 1-10: SUMMARY OF RECLAIMED WATER QUALITY DATA

Data Source: TRUE 2020.

In addition to reclaimed wastewater irrigation, the Town constructed a Rapid Infiltration Basin and has the ability to discharge treated wastewater to ground. The RIB is utilized to maintain appropriate water levels in the storage lagoon to accommodate wastewater inflows during the non-irrigation season. From 2017 to 2019, between 16,858 m³/yr and 38,391 m³/yr of reclaimed water has been infiltrated into the RIB.

WWAL was requested to complete this hydrogeological review of the current groundwater monitoring program and to make recommendations for modifications to the monitoring plan to reflect the newly permitted and future irrigation areas. In concert with this hydrogeological review, WWAL coordinated and participated in a soil investigation and reclaimed water irrigation suitability assessment of the new irrigation areas (Hamilton and Associates 2020).

2.0 SCOPE OF WORK

WWAL's work program was outlined in our accepted proposal P20-077 dated May 7, 2020. We completed the following scope of work for this assessment:

- Reviewed pertinent background information on the wastewater system. This included Operational Certificate PE-13717, several annual sanitary sewer system monitoring reports prepared by TRUE Consulting (2015 2020), previous hydrogeological reports (Golder 1998a and b), well logs for monitoring wells, and the results of the current groundwater monitoring program.
- Reviewed available information on area geology and hydrogeology, including aquifer mapping, data from provincial groundwater observation wells in the area, and well logs for reported water wells in the area.
- Completed a site visit to view the monitoring well sites, the location of the rapid infiltration facility and the new irrigation areas.
- Compiled water level and water quality data from annual monitoring reports, and created time series plots for water levels and key indicators of wastewater influence in groundwater.
- Prepared this report outlining the results of our assessment including recommendations to modify or update the annual monitoring program.

3.0 SITE DESCRIPTION, PHYSIOGRAPHY AND GEOLOGY

3.1 Site Description

Oliver, B.C. is located in the South Okanagan valley, straddling the Okanagan River between Vaseux Lake to the north and Osoyoos Lake to the south. The largest surface water bodies in the Oliver area are the Okanagan River and Tugulnuit Lake. The Okanagan River flows north-south through Oliver and Tugulnuit Lake is located in the northeast of the Town. Highway 97 transects the Town, roughly following the Okanagan River. Oliver is bounded by mountainous terrain to its east and west with land in the area generally sloping towards the river valley bottom. Elevations in the Town of Oliver range from approximately 600 m above sea level (asl) in upland areas to 300 m asl in the valley bottom.

The bulk of the Town's wastewater treatment and storage infrastructure, including the aerated treatment lagoons, effluent storage reservoir and RIB are located in the Fairview area to the west of the Town boundary (Figure 1). Currently permitted, newly permitted and future irrigation areas are shown on TRUE's Figure 1.1 and other figures provided as an attachment. A summary of each irrigation area is provided below.

Fairview Mountain Golf Course:

The Fairview Mountain Golf Course is located along the hillside southwest of the Town boundary and approximately 1 km south of the aerated lagoons and effluent storage reservoir. An area of approximately 45 ha is irrigated with reclaimed water at the golf course and irrigation volumes range from approximately 250,000 m³ to 350,000 m³ per year. Land to the north, south and west of the golf course is largely undeveloped rocky/forested hillside with land to the east being agricultural in use.

Huggins Property:

The Huggins irrigation area is a 3.7 ha vineyard located along Fairview Road south of the aerated lagoons and effluent storage. Service to the Huggins property is currently turned off with reclaimed water being used to meet irrigation demands in case of drought. The Town's WWTP is located to the north of the Huggins property, to the east is the Alonso property and areas to the west and south area largely undeveloped with some agricultural land use to the south.

Alonso Property:

The Alonso property is located on Fairview Road directly to the east of the Huggins vineyard. The Town's WWTP is located to the north of the Alonso Property and undeveloped land followed by agricultural land borders the property to the east and south. The irrigated lands at the Alonso property encompass a 1 ha vineyard that receives approximately 1,600 m³ to 9,200 m³ of reclaimed water annually during the irrigation season. The RIB is located approximately 100 m southeast of the Huggins vineyard.

Fairview Park:

Fairview park is located within the Town of Oliver, just south of South Okanagan Secondary School. 0.3 ha of land are irrigated at Fairview park and reclaimed water flows are not yet metered in this location.

Gala Street Linear Park:

Gala Street Linear park is located along Gala Street to the east of South Okanagan Secondary School. To the north, east and south Gala Street Linear Park is bordered by residential areas. Gala Street Linear Park receives approximately 6,200 m³ to 8,900 m³ of reclaimed water via spray irrigation annually over an area of 0.8ha.

South Okanagan Secondary School:

South Okanagan Secondary School is located at 6140 Gala Street. Land use surrounding the school is largely residential. 5.4 ha of land are irrigated at South Okanagan Secondary School, receiving 25,700 m³ of reclaimed water for irrigation in 2019.

Cemetery:

The Cemetery is located along the Town's west boundary, is bordered by agricultural land and a gravel pit to the west, the Town to the east and south and undeveloped hillslopes to the north. An area of 0.74 ha is irrigated with reclaimed water at the cemetery, receiving on the order of 13,400 m³ to 17,000 m³ of reclaimed water annually.

Public Works Yard:

The Town's Public Works Yard is located to the northeast of the airport along the west shore of the Okanagan River at 5971 Sawmill Road. Approximately 5,100 m³ to 8,300 m³ of reclaimed water are applied to an area of 0.6 ha annually. In addition to utilizing reclaimed water for irrigation at the Public Works Yards, reclaimed water is applied to compost piles.

Oliver Community Parks and Recreation Ball Diamonds/Kiwanis Park:

These parks cover an area of 8.6 ha along the east shore of the Okanagan River and is bordered by Fairview Road to its northwest. Kiwanis Park (0.6 ha) is located to the north of Fairview Road and another small section of park (0.6 ha) is located across the Okanagan River. The Oliver Community Park area is not yet irrigated with reclaimed water but is proposed as a future expansion area.

Oliver Municipal Airport:

The Oliver Municipal airport is located southeast of the Town's core and to the west of the Okanagan River. Currently 12.6 ha of land are irrigated with reclaimed water at the airport with the irrigation area being proposed to be expanded by an additional 9.8 ha. The airport receives approximately 69,000 m³ to 186,000 m³ of reclaimed water yearly. To the east and south west the airport is bordered by agricultural land and by commercial properties to the north and west.

3.2 Geological Setting

In northern and southern areas, including the southern extent of the airport, Oliver is underlain by metamorphic rocks of the Grand Forks Gneiss/Monashee Complex from the Proterozoic era (2500-570 million years before present). Bedrock of this complex includes quartz-biotite gneiss, quartzite, marble and amphibolite. In areas underlying the aerated lagoon, RIB and Fairview Mountain Golf Course, bedrock is mapped as metamorphic rocks of the Kobau Group described as schist, chlorite schist, quartzite, amphibolite and minor marble, Carboniferous to Permian in age (362.5 to 245 million years before present). The remainder of Oliver, mainly the Town centre as well as areas to the east and west of the Town centre, are underlain by bedrock of the Okanagan Batholith Group. Rocks of the Okanagan Batholith Group are described as granodioritic intrusive rocks from the Middle Jurassic, 178-157.1 million years before present (ENV, 2020).

Surficial geology in the Okanagan Valley was extensively mapped and described by Hugh Nasmith in Bulletin No. 46 *Late Glacial History and Surficial Deposits of the Okanagan Valley British Columbia* (1962). Surficial geology in the upland areas underlying in the Fairview Mountain Golf Course and RIB is characterized by outwash terrace deposits consisting of stratified glacial drift material deposited from meltwater streams and lakes during glacial retreat. The remainder of the upland areas are mapped as raised alluvial fans, terraces and deltas. Modern day Okanagan River floodplain deposits are found along the Okanagan River. Surficial geology underlying the town centre to the west of the Okanagan River is characterized by raised alluvial fans and deltas.

4.0 HYDROGEOLOGICAL SETTING

There are four provincially-mapped aquifers underlying the Oliver area, of which three are present beneath some or all of the irrigation areas (ENV, 2020). The mapped aquifers include Aquifers 254 IIA, 255 IA, 256 IIA and 1108 IIA, select details for which are provided in Table 4.1. The extent of these aquifers is shown on Figure 2. The two primary aquifers over which the bulk of reclaimed water irrigation occurs are Aquifer 256 and 254.

6

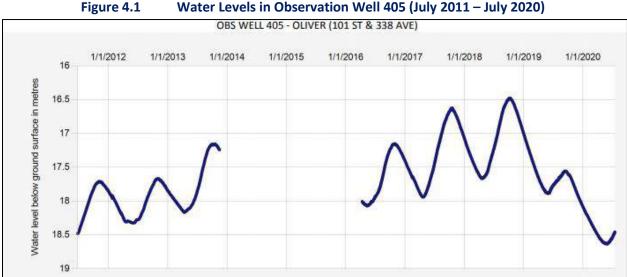
Aquifer Number	Aquifer Type	Description	Vulnerability	Productivity	Demand	Irrigated Areas Overlying
		Unconfined valley bottom alluvial aquifer,				• Airport
	Sand And	generally east of Highway 97 extending from				 Public Works Yard
254 IIA	Gravel	Tugulnuit Lake to Osoyoos Lake	High	High	Moderate	 Oliver community Park
		Unconfined valley bottom alluvial aquifer,				
	Sand And	extending from Tugulnuit Lake north to				
255 IA	Gravel	Vaseaux Lake	High	Moderate	High	
						 Fairview Mountain GC
						 Allonso/Huggins
						• S. Okanagan Secondary
						School
		Predominantly confined aquifer system				 Fairview Park
		comprised of alluvial or colluvial deposits,				• Gala Linear Park
	Sand And	occupying the terraces and hillsides west of				Cemetery
256 IIA	Gravel	Highway 97	Low	Low	Moderate	• RIBs
						A bedrock aquifer
						underlies all areas
		Predominantly unconfined fractured				receiving reclaimed
		crystalline bedrock aquifer, underlies the				water, but overburden
		Oliver Town core and mountainous areas to				aquifers overly bedrock in
1108 IIA	Bedrock	the west.	High	Low	Low	most areas.

Table 4.1Mapped Aquifers in the Oliver Area

The mapped overburden aquifers (Aquifers 254 IIA, 255 IA, 256 IIA) form an unconfined to semi-confined valley bottom aquifer system along the Okanagan River receiving recharge from upland bedrock areas, Vaseux Lake, the Okanagan River and irrigation. Elevated nitrate levels have long been reported in the aquifer system (Hodge 1992) and are likely caused by agricultural activity (Geller, D. and B. Manwell, 2016). Groundwater flow direction in Aquifers 254 IIA and 255 IA is inferred to follow the Okanagan River southwards towards Osoyoos Lake. In Aquifer 256 IIA groundwater flow is inferred to be eastwards towards the Okanagan River from upland areas, with Aquifer 256 discharging into the valley bottom Aquifer 254 system.

The Town of Oliver relies on a network of groundwater supply wells to provide potable water to the community. In addition to supplying potable water the Town supplies irrigation water to approximately 5,200 acres of farmland and 455 acres of non-farmland. The majority of irrigation water is sourced from surface water with a small portion being provided by groundwater. The potable water supply well located closest to the irrigation areas is the Rockcliffe Well (WTN82376), approximately 400 m west of the airport. The Town's Fairview irrigation well is located approximately 1,300 m east of the golf course. The location of the Town's municipal supply wells (within the extent of the map area) are shown on Figure 1.

Provincial observation well # 405 (OW 405) is located approximately 770 m west of the southern extent of the airport. OW405 is completed in Aquifer 256 IIA and water levels for OW405 are available from 2011 on, although a data gap exists from November 2013 to April 2016. Water level data for OW 405 (Figure 4.1), indicates annual water level fluctuations in the aquifer are on the order of 0.3 m to 1.3 m, with highest water levels being observed in the fall (October or November) and lowest levels occurring in the spring (April, May). The annual water level trend in Aquifer 256 differs from that of other monitoring wells in the interior completed in sand and gravel aquifers, where annual groundwater highs typically occur in the late spring/early summer and are typically associated with freshet induced recharge to aquifers. Higher aquifer levels in the fall indicate that Aquifer 256 is likely receiving recharge from irrigation return flows as the high water levels correspond with the end of the typical irrigation season (May to October). Aquifer levels appear to have been stable or slightly increasing from 2011 to 2018. Recent data suggests that aquifer levels are declining with the lowest aquifer levels on record being observed in early 2020.



Water Levels in Observation Well 405 (July 2011 – July 2020)

5.0 CURRENT GROUNDWATER MONITORING AND SAMPLING PROGRAM

The current groundwater monitoring program includes seven monitoring wells (Figure 1), of which five intercept groundwater and can be sampled.

Four of the monitoring wells are located in the Fairview area and were constructed in 2000. Town MWs 5, 6 and 7 are located east of the Fairview Golf Course and Town MW4 is located further north, in close proximity to the currently used RIB. Town MW4 and MW5 reportedly always contain water, while MW6 has reportedly been dry since 2003 and MW 7 has reportedly been dry since 2006. Well logs for the monitoring wells in the Fairview area indicate that the area is underlain by sand and gravel with varying silt content followed by clayey silt. These monitoring wells are typically completed with screens just above the clayey silt, but some of the screens are located within the clayey silt and do not contain groundwater.

Three monitoring wells (referred to as Wells #1, #2 and #3) located east of the airport are inferred to have been constructed in 2005 around the time reclaimed water irrigation began at the airport. No well logs are available for these wells, however these wells consistently intercept groundwater and are sampled.

Table 5.1 provides a summary of construction details for the wells in the current monitoring program.

	Table 5.1	Summary of Monitoring Well Construction Details			
Well ID	Well Depth m (ft)	Screened Interval m (ft) bgs	Diameter mm (in)	Top of Casing Elevation m asl	Location
Well #1	10.52 (34.5)				
(Air Cadet)	btoc	unknown	50 (2)	308.52	East (Downgradient) of Airport
Well #2	8.08 (26.5)				
(Rodeo Grounds)	btoc	unknown	50 (2)	306.56	East (Downgradient) of Airport
Well #3	4.1 (13.5)				
(91A Street)	btoc	unknown	50 (2)	295	East (Downgradient) of Airport
Town MW4	10.98 (36)				
(near RIB)	btoc		50 (2)	351.906	Downgradient of RIB
Town MW5	13.25 (43.5)				
(125 th Street)	btoc		50 (2)	363.361	Assumed Background
	18.29 (60)	13.29-18.29			
Town MW6	bgs	(43.6-60)	50 (2)	362.702	Downgradient of Golf Course
Town MW7	25.91 (85)	20.91-25.91			
(Road No. 5)	bgs	(68.6-85)	50 (2)	362.859	Downgradient of Golf Course

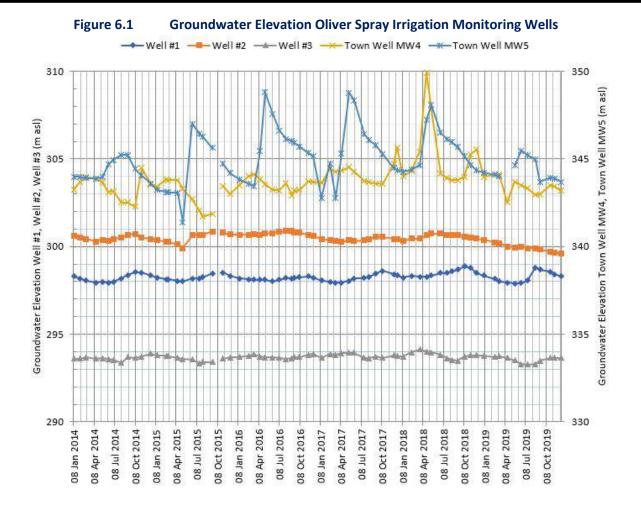
In addition to the above, the Town has three monitoring wells located between the Huggins and Alonso properties, just south of the wastewater treatment and storage lagoons. These wells were installed in 1997 as part of hydrogeological investigation supporting the design and commissioning of a RIB in the area (this RIB was only used for a few years in the late 1990s and early 2000s and is no longer in use). These three wells are not currently monitored.

The current monitoring program sees groundwater levels measured in each of the seven active wells monthly, and water quality samples collected biannually in April and September. Monitoring wells are sampled for the following parameters:

- Nitrogen species (nitrate, nitrite, ammonia)
- Total and dissolved phosphorous
- Chloride, sodium, calcium and magnesium
- Hardness
- conductivity

6.0 HISTORICAL GROUNDWATER LEVEL DATA

WWAL was provided monitoring well water level data collected from 2014 to 2019. Annual Sanitary Sewer Systems Reports prepared by TRUE indicate that Town MW6 has been dry since at least 2003 and Town MW7 was first noted to be dry in 2006 (TRUE, 2020). Monitoring well logs indicated that Town MW's 4, 5 and 7 are screened either above or across the clayey silt unit whereas Town MW6 is screened within the clay unit which could be the reason for this well being dry. Figure 6.1 illustrates water levels in the monitoring wells from 2014 to 2019.



The monitoring wells near the airport (Wells #1 to #3, completed in Aquifer 254) show a different pattern of water level fluctuations than Town MW4 and MW5, which are completed in Aquifer 256. Wells #1 to #3 fluctuate on the order of 0.5 to 1 m annually and are relatively stable. Water levels in Well #1, Well #2 and Well #3 appear to be at their highest near the end of the irrigation season suggesting that irrigation return flows are contributing recharge to the aquifer.

Water levels in Town MW4 and MW5 display greater fluctuations in water levels when compared to the monitoring wells installed near the airport. MW5, the assumed program background well, shows the most annual fluctuation, on the order of 3 to 6 m. Seasonal peaks tend to occur in May or June. This contrasts with the pattern observed at provincial observation well #405 (discussed in Section 4), where seasonal highs occur in October, presumably in response to irrigation return flows. Town MW5 is located hydraulically upgradient of most of the irrigated areas and the pattern of fluctuation is more indicative of the typical freshet influenced aquifer recharge response observed in the Okanagan.

Town MW4 displays less seasonal fluctuation than Town MW5 but still more than the wells near the airport. A noticeable spike in water levels is evident in May 2018, and is assumed to be the result of use of the RIB at that time. As water level measurements are only collected monthly, the full impact of use of the RIB (which may only occur for a week or two) is likely not being captured.

7.0 HISTORICAL GROUNDWATER QUALITY DATA

The current groundwater monitoring program assesses impacts of reclaimed water disposal on the receiving environment in locations downgradient of the two areas receiving the greatest amounts of reclaimed irrigation water (Fairview Mountain Golf Course and Airport) along with impacts of effluent infiltration through the RIB. Environmental receptors of concern include aquifers downgradient of the irrigation areas and RIB where wells may be used, as well as downgradient aquatic receiving environments, mainly the Okanagan River. Aside from groundwater being utilized for drinking water the area south of Oliver is largely agricultural in use, therefore groundwater may also be used for irrigation and livestock watering.

Considering the above receptors of concern, water quality results were compared to the B.C. Contaminated Sites Regulation, Schedule 3.2, Generic Numerical Water Standards for Drinking Water (CSR DW), Aquatic Life (CSR AW), Livestock Watering (LW) and Irrigation (IW) (ENV, 1997).

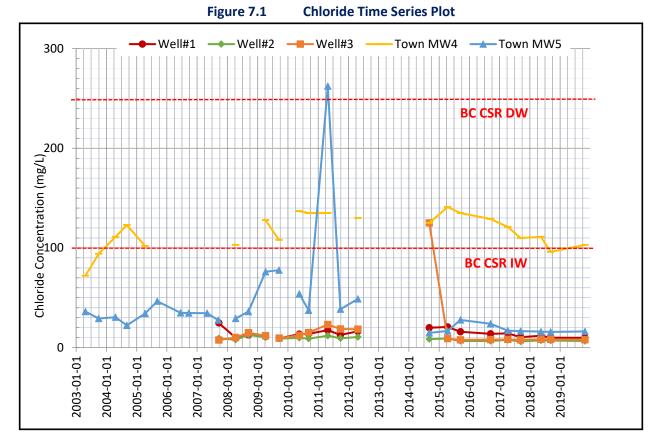
Water quality results for parameters sampled at the monitored wells are discussed in the sections below along with time series plots, illustrating concentrations of each parameter over time.

7.1 Chloride

Chloride is regarded as a conservative ion, meaning it does not biogeochemically degrade and is indicative of the degree of anthropogenic input. While chloride is typically present in low concentrations in freshwater aquifer systems, elevated chloride can be due to anthropogenic activities such as reclaimed water irrigation, wastewater effluent disposal to ground, road salting, industrial processes, and agricultural activity. Figure 5.1 illustrates a time series plot of chloride concentrations in monitoring well samples. For context, chloride concentrations in the reclaimed water used for irrigation in 2019 was in the 140 to 170 mg/L range.

Overall chloride levels in Well #1, Well #2 and Well #3 appear relatively stable in recent years and are generally found below 30 mg/L with the exception of a spike in chloride at Well #3 in September 2014. Town MW4 generally displays the highest chloride concentrations out of all monitored wells, which is likely associated with the downgradient location of Town MW4 with respect to the RIB and surrounding agricultural activity.

Town MW5 is used as a background well as reclaimed water irrigation is no longer practiced upgradient of this well. Over the last 5 years chloride concentrations in Town MW5 were relatively stable and similar to concentrations at wells #1-3. Prior to 2012, when irrigation with reclaimed water was presumably occurring upslope, chloride concentrations were higher.



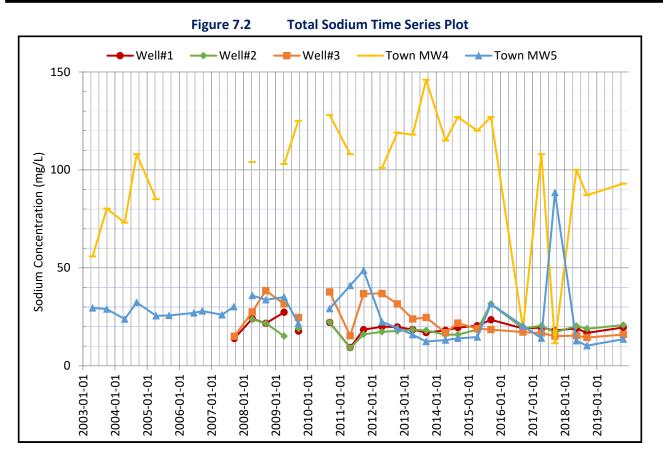
7.2 Sodium

The presence of sodium above background concentrations can indicate wastewater impacts on groundwater. Sodium can also be present due to anthropogenic activities such as road salting, industrial effluents, home water softener use, and agricultural activity.

Sodium concentrations in Well #1, Well #2 and Well #3 remained relatively stable since 2014, showing some moderate fluctuations prior to 2014

Town MW4 displays the highest sodium concentrations and sizeable fluctuations in sodium concentrations. Sodium levels in Town MW4 declined rapidly in the fall of 2016 after which spikes in concentrations were observed in samples collected in the spring. These observed spikes are likely the result of reclaimed water infiltration through the RIB as the RIB was in use during the winters of 2017, 2018 and 2019. MW4 and the RIB are located within a draw, which may also convey waters impacted by upgradient agricultural activities towards the area.

Town MW5 shows relatively large variations in sodium concentrations, with concentrations generally being below Town MW4 and in the same range as the airport monitoring wells.

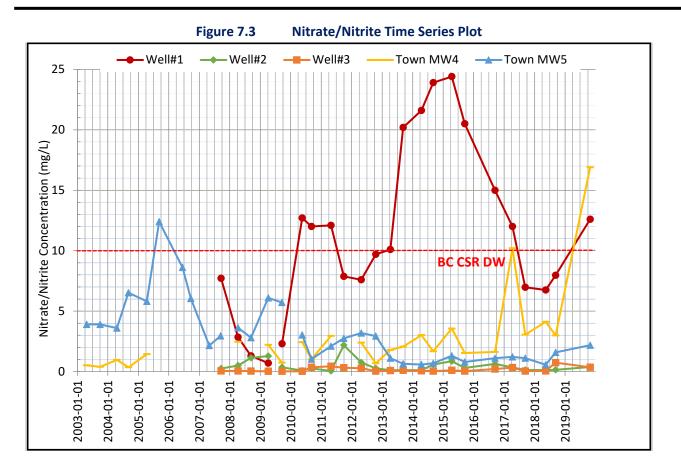


7.3 Nitrate/Nitrite

Nitrate rarely occurs naturally in water and generally occurs in water due to anthropogenic activities. Nitrate concentrations greater than 3 mg/L are considered by the Province to reflect human impacts (ENV, 2007). The most common anthropogenic sources of nitrates include agricultural activities, wastewater disposal to ground, and discharge from industrial processes and mining (blast residuals from ammonium-nitrate or other explosives). Nitrite is an unstable form of nitrogen that rapidly oxidizes to nitrate or reduces to nitrogen gas, as such nitrite is typically found at low concentrations in the environment (ENV, 1998).

Overall, Well #1 displays the highest nitrate/nitrite levels with concentrations frequently exceeding the BC CSR DW standard. Nitrate/nitrite concentrations appear to have peaked in Well #1 in 2015 at close to 25 mg/L, decreasing until late 2018, then rising again. The concentration and pattern of nitrate concentrations in Well #1 is anomalous, and suggests there may be another point source of nitrate being added to the aquifer near this location. Nitrate/nitrite concentrations in Well #2 and Well #3 have remained relatively stable and mostly below 1 mg/L.

An increasing trend in nitrate/nitrite concentrations is apparent in Town MW4 with the sample collected in the fall of 2019 exceeding the BC CSR DW standard. Again, water quality in Town MW4 appears to be influenced by the RIB. Nitrate and nitrite concentrations in Town MW5 show a decreasing trend although some impact is still evident and likely due to agricultural activity in the surrounding area.

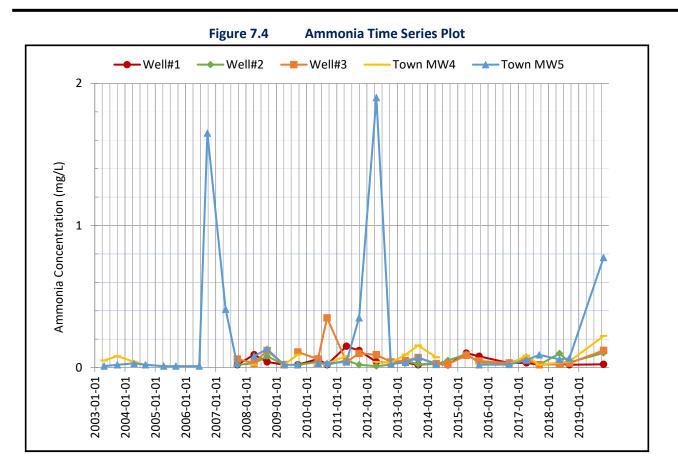


7.4 Ammonia

Ammonia is the primary form of nitrogen in raw wastewater but is quickly converted to nitrite and eventually nitrate during wastewater treatment (MoE 1998). When ammonia or nitrite are present in groundwater, it indicates that the source of nitrogen is close by, and that the nitrification process was not completed prior to nitrogen reaching the groundwater table. Anthropogenic sources of ammonia include wastewater effluent, agriculture and urban development, industrial effluents, and mining (blast residuals).

Ammonia concentrations in all wells except MW5 have been relatively stable since 2011. Several spikes in ammonia concentration in MW5 have occurred which do not correspond to spikes at other locations and is considered anomalous. The ammonia data indicate a point source other than the reclaimed irrigation water may be impacting MW5.

The ammonia concentration in most monitoring wells trended upward in the fall sample collected in 2019.



8.0 CONCLUSIONS

Based on our assessment, we provide the following conclusions:

- C1 The current groundwater monitoring program includes seven monitoring wells, three downgradient of the airport (Well #1, Well #2, Well #3), two downgradient of the Fairview Mountain Golf Course (MW6 and MW7), one downgradient of the RIB (MW4) and one background well (MW5). Water levels in the monitoring wells are checked monthly and samples are collected from the monitoring wells semi-annually, usually in the spring and fall.
- **C2** MW6 and MW7 which are intended to monitor impacts from irrigation of the Fairview Mountain Golf Course have been dry for more than a decade, so no monitoring of the impacts of golf course irrigation is currently completed.
- **C3** The monitoring wells near the airport (Well #1, #2 and #3) are completed in valley bottom Aquifer 254, while the remaining wells which are completed at higher elevation in the Fairview area are completed in Aquifer 256. The pattern of groundwater level fluctuation in these two groups of monitoring wells are different and evident in the data being collected. Airport monitoring wells show a small magnitude of seasonal fluctuation on the order of 0.5 to 1.0 m, with peaks occurring in the fall suggesting the influence of irrigation recharge. MW5, the assumed program background well, shows the highest magnitude of fluctuation in the 3 6 m range, with peaks in the spring

typical of an aquifer response to freshet induced recharge. MW4, located immediately downgradient of the RIB shows moderate seasonal fluctuations of 2 - 3 m and the data indicate groundwater level spikes occur in response to loading of the RIB, which is to be expected.

- C4 Water quality results from the groundwater monitoring program indicate the following:
 - Water quality in MW4 shows elevated sodium, chloride and nitrate/nitrite concentrations, with the most recent nitrate sample collected being 17 mg/L, above the drinking water quality guideline of 10 mg/L. MW4 is located immediately downgradient of the RIB, and in a draw leading from the Alonso and Huggins properties located upslope. MW4 is impacted by the RIB and likely upslope land uses, and a plume of nitrate-impacted groundwater is expected to migrate away from the area following loading of the RIB. The geometry and extent of that plume is not known. It is likely that the current monitoring program does not capture the full range of impacts from use of the RIB, as the RIB is typically loaded continuously for a period weeks while water levels are measured monthly and water quality samples are only collected biannually.
 - Town MW5, which is utilized as the program background well shows water quality impacts. Of note are recurring spikes in ammonia concentrations at levels not seen in other monitoring wells. As lands near MW5 are not currently irrigated with reclaimed water, the observed water quality impacts may be due to other point sources.
 - Well #2 and Well #3 located downgradient of the airport generally display the lowest impacts on groundwater quality, with concentrations of chloride, sodium, nitrate and ammonia at what are likely background levels for Aquifer 254. Well #1 is an exception, as it is characterized by very high nitrate concentrations often above 10 mg/L, and reaching as high as 25 mg/L in 2015. The data suggest a point source of nitrate in the area other than the reclaimed water may be impacting groundwater at Well #1. The Air Cadet building is located very close to Well #1, and we noted a vineyard and BC Tree Fruits facility across the street to the east.
- **C5** The current reclaimed water irrigation monitoring program appears to adequately assess impacts of the reclaimed water irrigation and disposal system downgradient of the airport, however the data for Well #1 indicates a significant impact to groundwater and warrants additional investigation.

Town MW4 is well sited to monitor impacts from reclaimed water infiltration at the RIB, however the frequency of monitoring at this well is not sufficient to adequately characterize the impact to groundwater.

Town MW5, the program background well, displays some indication of impacts to groundwater, even though reclaimed water irrigation no longer occurs upslope.

Lastly, as the two wells sited to assess impacts from irrigation of the Fairview Mountain Golf Course have been dry since at least 2007, the impacts of golf course irrigation are not being assed in the current program.

7. **RECOMMENDATIONS**

- **R1** WWAL recommends continued monthly monitoring of water levels and bi-annual sampling at Wells #1, #2, #3 and Town MW5.
- **R2** We recommend an increased level of monitoring at Town MW4 located near the RIB. We recommend that a transducer be installed in this well to better characterize the effect on water levels when the RIB is utilized. We also recommend that for one full year, groundwater quality samples from Town MW4 be collected monthly.
- **R3** We recommend incorporating the three wells between the Huggins and Alonso properties into the monitoring program for 1 year if the wells are still present. Groundwater levels should be measured monthly and water quality samples collected biannually on the same schedule as the other wells. After reviewing the results of the one year of monitoring, it may be found that one of these wells would serve as a better program background well.
- R4 Well #1 located near the Air Cadet building near the airport shows significant nitrate impacts, the source of which is not known and is inconsistent with the data obtained from the other airport monitoring wells which demonstrate little impact. The source of this nitrate contamination should be investigated. Possible sources include the nearby vineyard, BC Tree Fruits facility, possible septic field for the Air Cadet building, or leaking wastewater or reclaimed irrigation water mains. Depending on the results of this investigation, additional monitoring wells in the area may be required to further investigate the source of the nitrate in groundwater.
- **R5** Several additional monitoring wells are required to adequately monitor the "new" areas receiving or slated to receive reclaimed irrigation water, and to monitor impacts from the current largest consumer of reclaimed water, the Fairview Mountain Golf Course. The following monitoring wells are recommended:
 - 1. One monitoring well in the Gala Street Liner Park, sited to monitor the impacts of irrigation in the park and at the Secondary School.
 - 2. One monitoring well in the southern end of Oliver Community park.
 - 3. One monitoring well in the southern end of the Public Works Yard.
 - 4. One monitoring well along the southern property boundary of the cemetery. The need for this well can be discussed further, as there may be public opposition to drilling in a cemetery. In addition, a monitoring well at this location may be influenced by the cemetery as well as the reclaimed water irrigation.

 Two monitoring wells east of the Fairview Mountain Golf Course to replace MW6 and MW7.

Ideally these monitoring wells would be installed before the April 2021 sampling event, and after installation, would be monitored and sampled at the same frequency as the other monitoring wells.

R6 After the new wells have been monitored for one year, the data should be compiled, reviewed and interpreted by a hydrogeologist. Modifications to the monitoring plan can be made after that.

Table 8.1 Summary of Recommended Modifications to Groundwater Monitoring Program

Recommendation	Details
Increased level of Monitoring at MW4	Install a transducer, or increase the frequency of manual water level measurements to weekly. Increase the frequency of water quality sampling to monthly for one year.
Incorporate the existing three monitoring wells near the Alonso and Huggins Property into the monitoring program for one year.	Monitor/sample on the same schedule as the other wells in the program
Install one monitoring well in the Gala Street Liner Park, sited to monitor the impacts of irrigation in the park and at the Secondary School.	Monitor/sample on the same schedule as the other wells in the program
Install one monitoring well in the southern end of Oliver Community park.	Monitor/sample on the same schedule as the other wells in the program
Install one monitoring well in the southern end of the Public Works Yard.	Monitor/sample on the same schedule as the other wells in the program
Install one monitoring well along the southern property boundary of the cemetery. POSSIBLE	Monitor/sample on the same schedule as the other wells in the program
Install two monitoring wells east of the Fairview Mountain Golf Course to replace MW6 and MW7.	Monitor/sample on the same schedule as the other wells in the program

9.0 COST ESTIMATES

WWAL has prepared a high-level cost estimate to complete the above recommended tasks. Table 9.1 below summarized the estimates by task.

Contractor	Cost Estimate	
Environmental Drilling Contractor – 6 monitoring wells	\$25,000	
WWAL – Core well installation program: Confirmation of well sites, utility locates. Field oversight of monitoring well drilling. Well development and initial sampling. Provide well logs and a map.	\$10,000	
WWAL – Expanded program. Purchase and install recommended transducer in Town MW4 near RIB. Investigate source of high nitrate in Air Cadet well (Well #1). Compile and review data collected during 2021 and make recommendation for refinement of monitoring program moving forward.	\$10,000	

Table 9.1: Cost estimates to complete recommended tasks.

Notes:

- Costs in Table 9.1 do not include costs for monthly water level sampling and bi-annual sampling of the existing and proposed expanded monitoring well network. This routine monitoring is currently completed by Town public works staff. WWAL costs do include initial development and sampling (April 2021) of the recommended new monitoring wells (up to 6).
- Costs to install six new monitoring wells based on a quote from Mud Bay Drilling (attached). We suggest adding a \$5,000 contingency to this estimate to account for variability in well depths.

10.0 CLOSURE

We trust this letter provides the information you require. If you have any questions or would like to discuss these findings further, do not hesitate to contact the undersigned.

WESTERN WATER ASSOCIATES LTD.

lise Goratime

Lisa Gardiner, P.Eng. Environmental Engineer

Jan-2021 M. RHODES #32839 SCIE

Ryan Rhodes P.Geo. Hydrogeologist

<u>Attachments:</u> Figures 1 and 2; Mud Bay Drilling Quote

#106 - 5145 26th Street, Vernon, BC, Canada, V1T 8G4 Prince George Victoria P:1.250.541.1030 www.westernwater.ca

11.0 REFERENCES

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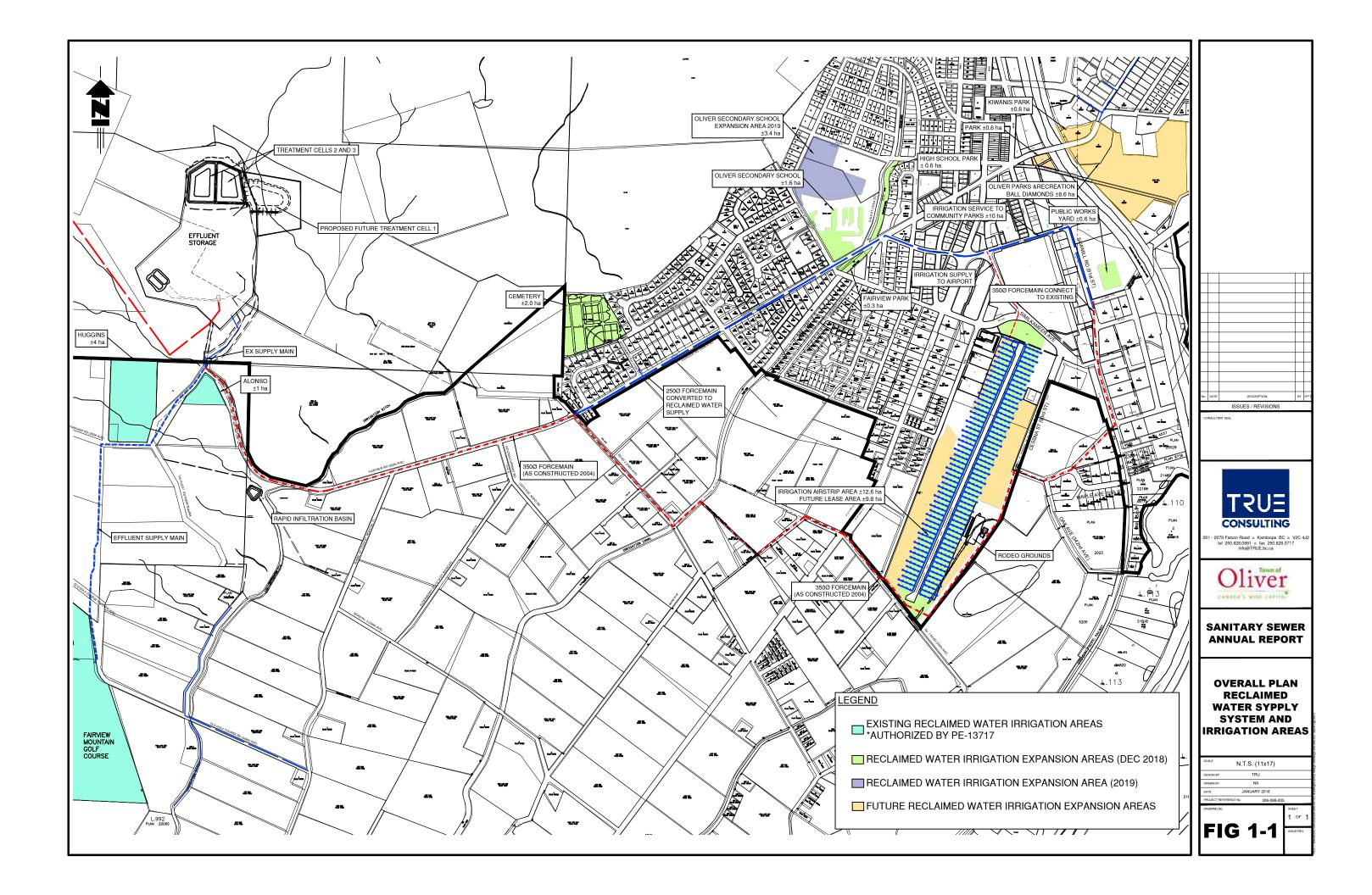
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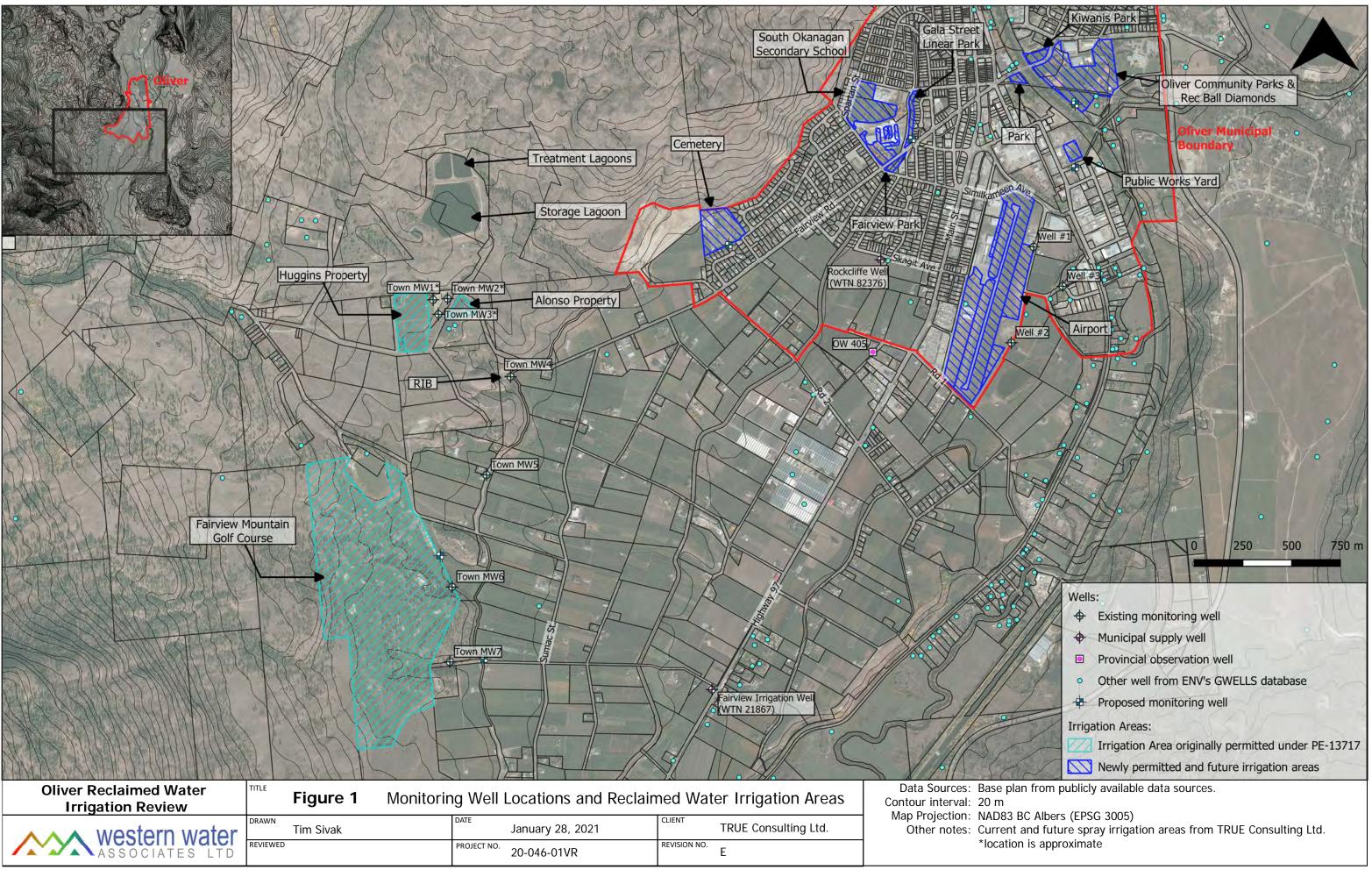
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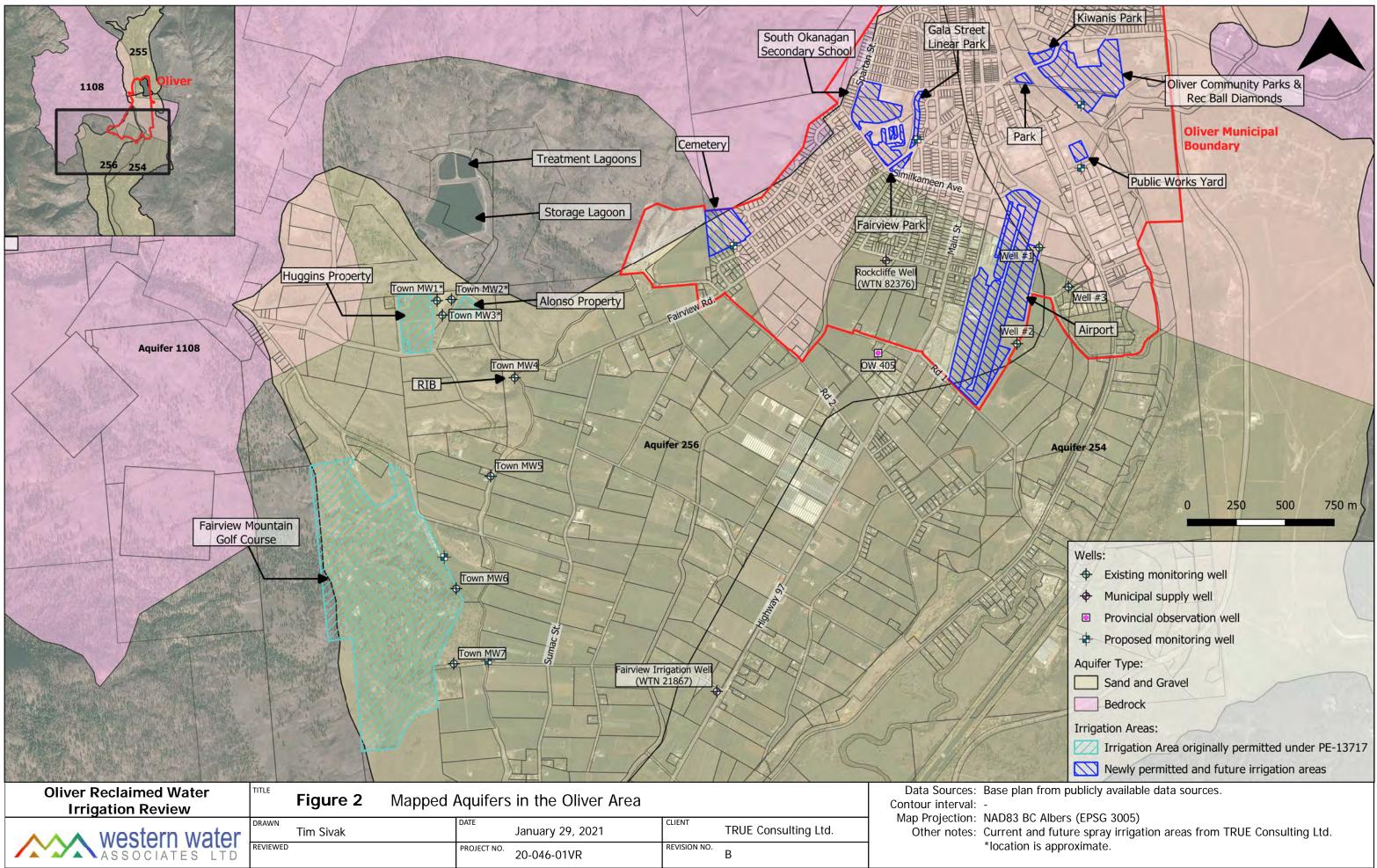
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2 mw's to 80' and 4 mw's to 40'

9015B Jim Bailey Road Kelowna, BC V4V 2W4

T: 250-765-2210 F: 604-888-4206

Contact:	Ryan Rhodes
Company:	Western Water Associates
Address:	106-5145 26th St
	Vernon, BC, V1T 8G4
Phone:	250-541-1030
Email:	ryan@westernwater.ca
Date:	Wednesday, August 26, 2020
Site:	Oliver

Estimate Number:	20-1207497
Revision Number:	20-1207497.2
Prepared By:	BSEY
Proposed Rig:	Sonic DB320

Scope

ltem	Description	Rate	Unit	Qty	Extended
Mobilization	Equipment and crew	\$800.00	Lump sum	1	\$800.00
Drilling, sampling, and Installations	All operations on site	\$475.00	Hours	29	\$13,775.00
Overtime	Over 8 hours on site	\$75.00	Hours	5	\$375.00
Crew travel	Crew only to / from site	\$185.00	Hours	2	\$370.00
Living allowance		\$750.00	Shift	2	\$1,500.00
Support unit		\$350.00	Shift	3	\$1,050.00
Bit and casing Wear		\$45.00	Meter	54.88	\$2,469.60
PVC screen	2" SCHD40	\$21.00	Meter	18.3	\$384.30
PVC blank	2" SCHD40	\$14.00	Meter	27.43	\$384.02
PVC fittings	J-Plug and sand point	\$41.00	Set	6	\$246.00
Silica sand		\$16.00	Bags	36	\$576.00
Bentonite chips		\$21.00	Bags	44	\$924.00
Concrete		\$16.00	Bags	6	\$96.00
45 gal. Drums with lids		\$70.00	Each	10	\$700.00
Well covers	Flush mount or stick-up	\$145.00	Each	6	\$870.00
Core boxes	10' per box	\$60.00	Each		\$0.00

Total (CAD \$): \$ 24,519.92

Notes and Assumptions

- Client is responsible for all locates and permits

- ConeTec and Mud Bay will not be responsible for damage to any underground utilities
- Client will provide suitable access for truck mounted equipment and transport truck and trailers

- Water must be available on site, or provisions made for prior to mobilization

- No allowances made for insitu testing or sampling

- No allowances made for disposal of cuttings or waste

- Client will be responsible for creating and submitting well closure reports

- Assumes secure site for overnight equipment parking

- Based on 10 hour work days + daily crew travel

- Weekend or night work premium will apply if required

- Traffic control and flaggers will be provided by the client if required

Town of Oliver Monitoring Well Installation



20-046-02VR

REFERENCE:

TECHNICAL MEMORANDUM

TO:	Shawn Goodsell (Town	of Oliver), Natalie Alte	en, P.Eng. (TRUE)	DATE:	26-Aug-2021
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FR: Morgan Jackson, B.Sc. and Ryan Rhodes, P.Geo, (WWAL)

RE: MONITORING WELL INTALLATION, DEVELOPMENT AND SAMPLING – TOWN OF OLIVER RECLAIMED WASTEWATER IRRIGATION SYSTEM ENVIRONMENTAL MONITORING PROGRAM, OLIVER, B.C.

INTRODUCTION

Western Water Associates Ltd. (WWAL) is pleased to provide this brief Technical Memorandum to the Town of Oliver (the Town) and TRUE Consulting Ltd. documenting the installation of new and replacement monitoring wells for the Town's reclaimed wastewater environmental monitoring program.

In 2020, WWAL completed a review of the Town's environmental monitoring program (WWAL 2021), which is a requirement of the Town's reclaimed wastewater system Operational Certificate PE-13717. Over time, the Town of Oliver has expanded the areas receiving reclaimed wastewater for irrigation, but the monitoring network had not been updated in concert so new monitoring wells to increase coverage of irrigated areas was recommended. In addition, two wells in the existing network were reportedly dry for the past decade, and we recommended those be replaced.

In total, four wells were completed in 2021. Drilling was completed in early May 2021. After drilling and installation, monitoring wells were developed, purged and sampled by WWAL for wastewater indicator parameters. In addition, WWAL was able to rehabilitate one of the original monitoring wells (Town MW6) to make it suitable for continued sampling.

MONITORING WELL DRILLING PROGRAM

WWAL installed four monitoring wells between May 4 and 7, 2021. Three of the monitoring wells were installed to provide coverage to newer areas receiving reclaimed water for irrigation that were not being monitored:

- MW8 south side of the Town Public Works Yard
- MW9 south end of the Oliver Cemetery
- MW10 Gala Street linear park, east of the South Okanagan Secondary School.

The fourth monitoring well (MW-11) is located near the west end of 332nd Avenue, and was installed as a replacement for pre-existing monitoring well Town MW7, which has been dry since at least 2006.

All four monitoring wells were drilled by Mud Bay Drilling of Surrey, B.C. with a rubber tracked Sonic DB320 drill rig. The wells were completed to depths of between 6.6 m to 29.7 m (22 ft to 97.5 ft) below ground surface (bgs) into unconsolidated sediments. The wells are 50 mm (2 inches) in diameter and are equipped with a J-Plug cap and a 10 slot screen of 1.5 m or 3 m (5 ft or 10 ft) in length. A 10-20 filter sand pack was installed in the annulus surrounding the well screens and a bentonite seal was installed as appropriate within the annular space, above the screened interval, and at surface. Three wells are completed flush with ground surface and one well (MW-11) was completed with an above ground steel protector. The well covers or monuments for all four wells were cemented

in place. All four monitoring wells comply with the requirements of the B.C. Groundwater Protection Regulation. Well logs are provided as an attachment and Table I summarizes select well details. Figure I depicts the location of all new and existing monitoring wells included in the groundwater monitoring program.

Well Identification	Completion Date	Well Completion Depth (mbtoc)	Well Surface Completion	Screened Interval (mbgs)	Aquifer Lithology	Water Level May 19, 2021 (mbtoc)
MW-8	May 4, 2021	6.52	Flush Mount	5.2 – 6.7	Sand & Gravel	2.35
MW-9	May 5, 2021	21.1	Flush Mount	18.2 – 21.2	Sand & Gravel some fines at depth	dry
MW-10	May 6, 2021	27.1	Flush Mount	25.7 – 27.2	Sand & Gravel some fines at depth	24.54
MW-11	May 7, 2021	30.6	Above Ground Monument	27.1 – 29.7	Sand and Silt	24.32

Table 1 – Summary of Select Monitoring Well Details	Table	I – I	Summary	of Sele	ect Mor	itoring	Well	Details
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Note: mbtoc- meters below top of casing; mbgs- meters below ground surface.

Well lithology was logged by WWAL field staff during drilling. Lithology observed in monitoring wells was relatively similar, consisting of sand, gravel or sand and gravel. At wells MW-9, MW-10 and MW-11 some finer sediments (silt and/or clay seams) were observed at depths ranging from 15 m to 26 m (48 ft to 88 ft). Lithology in the new monitoring wells is similar to reported lithology in existing monitoring wells included the program. Detailed well logs with lithology are included as an attachment.

MONITORING WELL DEVELOPMENT AND SAMPLING METHODS

The monitoring wells were developed by surging with a Waterra surge block, tubing and foot valve until approximately ten times the well volume was removed and water removed was relatively clear. The monitoring wells were disinfected with chlorine bleach approximately 4 to 7 hours prior to sample collection. The bleach was agitated using a bailer dedicated to that well and water was purged into a bucket away from the well head. Groundwater quality samples were collected within 3 to 5 hours of well development when the water ran relatively clear and no longer smelled of chlorine. WWAL field staff noted slight turbidity in water samples collected at the wells, which is common in newly installed wells and is expected to dimmish over time with additional sampling. The samples were labelled and stored in an ice-filled cooler, then transported to CARO Analytical, in Kelowna B.C. for chemical analyses within 24-hours of sample collection.

Monitoring well MW-9 has remained dry since installation and could not be developed or sampled at this time.

During an initial site visit in March 2021, WWAL staff found approximately I m of water in pre-existing monitoring well Town MW-6, which had previously been considered dry. Further, the well depth was measured to be approximately 4 m (13 ft) shallower than reported on the well log; we interpreted this to mean that fine sediments had accumulated in the bottom of the well over time. WWAL field staff attempted to bail out and re-develop MW-6 on two occasions using a small pump and waterra tubing/foot valve. This resulted in the removal of 0.4 m of sediment from the well.

WATER QUALITY SAMPLING RESULTS

Table 2 below summarizes the water quality results from monitoring wells MW-8, MW-10, and MW-11 collected on May 19, 2021. Water quality samples were also collected from pre-existing monitoring well Town MW-6 on May 19, 2021 as this well had recently been re-developed and had not been sampled since it was reported dry in 2003. A copy of the laboratory water quality results are attached to this report.

Reclaimed wastewater associated parameters chloride, nitrate, and sodium are slightly at all sampled locations, however, all below applicable Canadian Drinking Water Quality Guidelines (GCDWQ). Nitrate is elevated at MW-10 and MW-11 and to a lesser extent at MW-6 at 4.63 mg/L, 3.13 mg/L and 1.99 mg/L, respectively. Total coliform bacteria was not detected at any of the newly installed monitoring well but was detected a 5 MPN/100 mL at MW-6. *E.coli* bacteria were not detected at any of the sampled locations.

A duplicate sample was collected at monitoring well MW-11 during the sampling event on May 19, 2021 for QA/QC purposes. The Relative Percent Difference (RPD) of each of the sampled parameters with results above detection limits was calculated. Most parameters indicated RPD values lower than 10%, with the majority of the parameters falling below 5%. The RPD for total dissolved phosphorus was 28% and total kjeldahl nitrogen (TKN) was above 50%. WWAL asked the laboratory to re-analyze the samples for dissolved phosphorus and TKN to establish if there was laboratory error introduced during the previous analysis. The RPD for the re-run samples were 21.6 % (dissolved phosphorus) and 49.1 % (TKN). Caro Laboratory staff indicated that one of the samples was slightly more turbid, which likely caused the discrepancy between sample concentration values. Overall, we deem the sampling methodology used and results obtained to be acceptable. In the future, best efforts should be made to collect samples with as low turbidity as possible.

Table 2 – Summary of Water Quality Results							
Field Parameter	Units	GCDWQ	MW-6 (pre-existing well)	MW-8	MW-10	MW-11	
рН	pH units	7.0 - 10.5	7.8	7.83	8.11	7.0	
Electrical Conductivity	μS/cm	None	980	849	788	1031	
Temperature	°C	AO≤ 15°C	13.1	11.9	12.4	14.0	
Oxidation Reduction Potential	RmV	None	710	74	151	719	
Laboratory Parameter							
Chloride	mg/L	AO≤250	91.6	83.3	90.9	157	
Total Dissolved Phosphorus	mg/L	None	0.0557	0.117	0.0239	0.0264	
Total Phosphorus (as P)	mg/L	None	0.251	0.185	0.0497	0.088	
Ammonia	mg/L	None	0.067	<0.050	<0.050	<0.050	
Nitrate as N	mg/L	MAC=10	1.99	0.945	4.63	3.13	
Nitrite as N	mg/L	MAC=1	<0.010	<0.010	<0.010	<0.010	
Nitrate as N + Nitrite as N	mg/L	None	1.99	0.945	4.63	3.14	
Total Nitrogen	mg/L	None	2.62	1.24	4.91	3.38	
Total Kjeldahl Nitrogen	mg/L	None	0.625	0.292	0.282	0.241	
Conductivity	μS/cm	None	1060	905	978	1220	
рН	pH units	7.0 - 10.5	7.02	6.94	7.31	7.04	
Hardness	mg/L	None	345	312	343	470	
Calcium (total)	mg/L	None	80.7	89.4	82.5	111	
Magnesium (total)	mg/L	None	34.7	21.4	33.2	46.7	
Sodium (total)	mg/L	AO≤200	109	83.2	36.7	78.7	
Total Coliform	MPN /100 mL	MAC = None Detected	5	<1	<1	<1	
E. coli	MPN/100 mL	MAC = None Detected	<1	<1	<1	<1	

Note: bolded orange values indicated exceedance of health based MAC guidelines;

CONCLUSIONS AND RECOMMENDATIONS

WWAL oversaw the installation of four monitoring wells for inclusion in the Oliver reclaimed wastewater irrigation system groundwater monitoring program. After installation, WWAL developed the wells to make them suitable for ongoing sampling, and collected initial water quality samples from three of the monitoring wells (MW-8, MW-10, MW11) and one pre-existing monitoring well MW-6 (not sampled since at least 2003). Monitoring well MW-9 has been dry since installation and could not be developed and sampled at this time.

We recommend the following:

- RI Incorporate the four new monitoring wells into the environmental monitoring program. Continue to complete monthly water level measurements of all wells and biannual sampling.
- R2 Rehabilitated monitoring well Town MW-6 has a fairly limited water column and was observed to recharge slowly after being purged. Much of the screened interval of the well is filled with sediment, making this well more prone to producing turbid water during sampling. While most of the program monitoring wells are purged and sampled with waterra tubing and foot valves, we recommend Town MW-6 be purged and sampled with a bailer. This well should be first purged and

then sampled on the following day. Care should be taken to lower and remove the bailer slowly when sampling to obtain the clearest samples possible.

Further, MW-6 should be disinfected with bleach approximately 24 hours prior to purging and collecting water samples during the next sampling event to eliminate total coliform bacteria found to be present after the recent sampling.

Morgan Jackson, B.Sc. Environmental Scientist

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Ryan Rhodes, P.Geo. Hydrogeologist

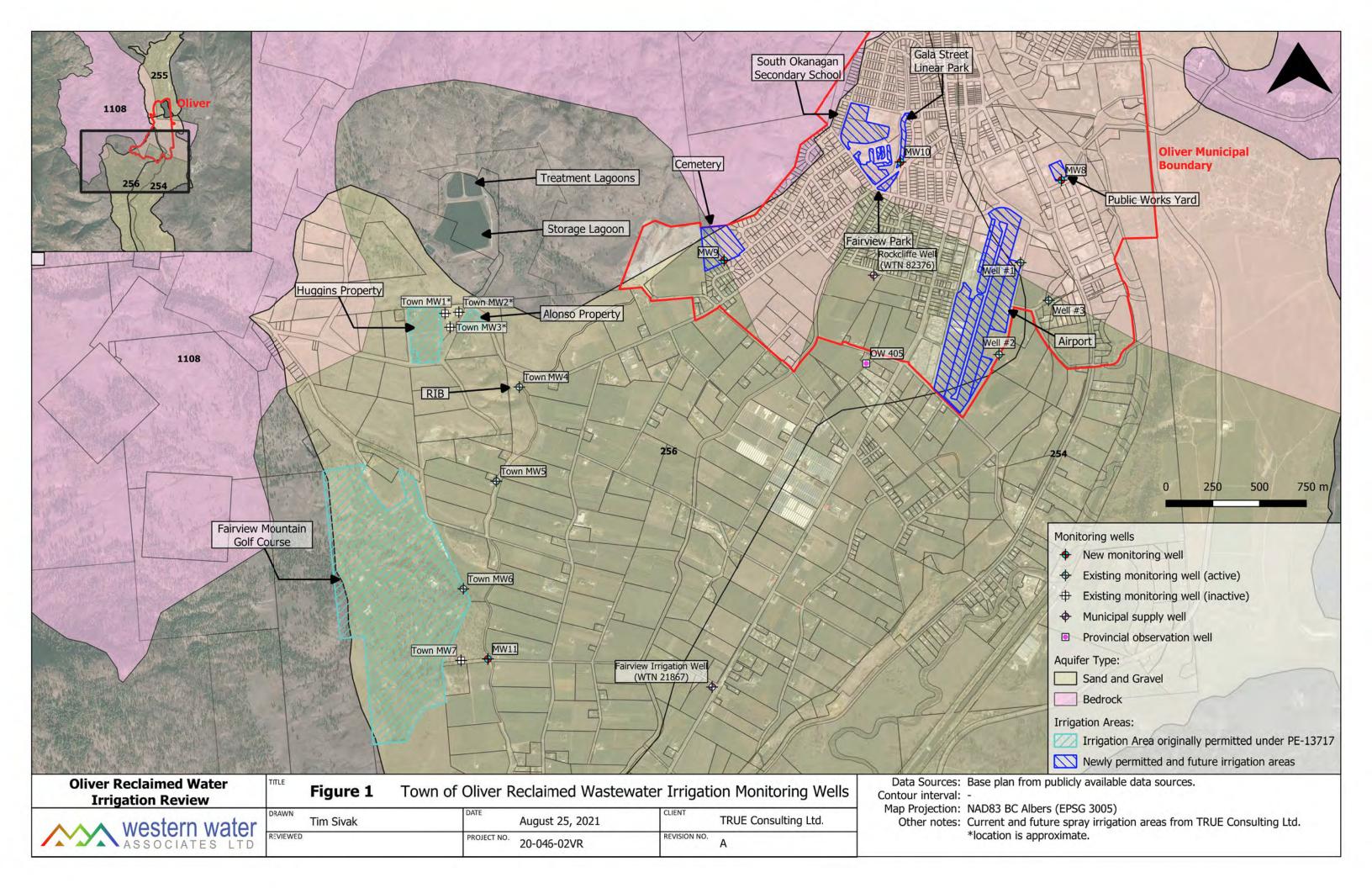
Attachments:

Figure I – Location of Oliver Reclaimed Water Environmental Monitoring Wells Well Logs Laboratory Analytical Reports

REFERENCES

Western Water Associates Ltd. 2021. Hydrogeological Review of the Town of Oliver Reclaimed Wastewater Irrigation Groundwater Monitoring Program. Report prepared for the Town of Oliver and TRUE Consulting Ltd., January 28, 2021.

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MONIT	Western water ASSOCIATES LTD in Hydrogeology and Water Resources Management ORING WELL ID: MW-8 CT: Town of Oliver Monitoring Well Insta T: Town of Oliver		SHEET 1 of D: May 4, 2021 N: Public Works Yard IBER: 20-046-02VR
DEPTH (m)	LITHOLOGY DESCRIPTION	WELL CONSTUCTION	WELL COMPLETION DETAILS
0 	Ground Surface SAND and GRAVEL, with some cobbles, coarse grained sand, small to large sub-rounded gravel, loose, poorly sorted, dry, brown.		Flushmount box, cemented in place 0.1 m - 5.2 m below ground surface (bgs) Blank 2 inch diameter PVC with J-plug cap 0.2 m - 0.3 m bgs 10-20 Filter sand 0.3 m - 1.2 m Surface seal, Enviroplug medium bentonite chips
23	SAND with some silt, minor clay, fine grained sand, loose, poorly sorted, dry, brown to grey. Organics (wood flecks) and mottling 2.3 m to 3 m.		1.2 m - 1.8 m bgs Sand and Crush Water level 2.45 m (8.0 ft) below top of casing (btoc)
4	SAND and SILT, fine grained sand, loose, poorly sorted, moist to wet at 5.2 m, dark grey		1.8 m - 4.6 m bgs Bentonite chips 4.6 m - 5.2 m bgs 10- 20 Filter sand

 $5.2\ m$ - $6.7\ m$ bgs 2 inch diameter 10 slot PVC screen 1.5 m (5 ft) length with bottom plug

 SANDY SILT, with clay seams, loose, wet, dark grey. Clay seams at approximately 6.7 m and 8.2 m, hard, dry, 1 -2.5 inches in thickness. 		Total Well Depth 6.52 m (21.4 ft) btoc
COORDINATES: 11U 314598.0 m E 5450466.0 m N	ELEVATION: 298 m asl	(gps)
STATIC WATER LEVEL: 2.45 m btoc	DRILLING CONTRACTO	DR: Mud Bay Drilling Ltd.
TOTAL DEPTH: 6.52 m btoc	DRILLING METHOD: So	onic rubber track rig
Drawn By: MJ	Reviewed By: RR	Logged By: MJ

6

7

SAND and GRAVEL

coarse and medium grained sand, small to large rounded gravel, loose, wet, brown.

western water **MONITORING WELL LOG MW-9** S SOCIATES LTD Consultants in Hydrogeology and Water Resources Management **MONITORING WELL ID: MW-9** DATE DRILLED: May 5, 2021 **PROJECT: Town of Oliver Monitoring Well Installation** SITE LOCATION: Cemetary **CLIENT: Town of Oliver** PROJECT NUMBER: 20-046-02VR DEPTH WELL CONSTUCTION LITHOLOGY DESCRIPTION WELL COMPLETION DETAILS (m) Flushmount box, cemented in place **Ground Surface** 0 1 2 SAND and GRAVEL, 0.1 m - 18.1 m below ground surface (bgs) Blank 2 inch medium and coarse grained diameter PVC with J-plug cap sand, small to large rounded to sub-rounded gravel, loose, poorly 0.2 m - 0.6 m bgs 10-20 Filter sand sorted, dry, brown. 0.6 m - 1.5 m bgs Surface seal, Enviroplug medium 3 bentonite chips 5 6 7 8 GRAVEL with some SAND. **9** = 1.5 m - 17.4 m bgs Alternating layers of 1 m bentonite seal with 4.5 m of natural sluff fine grained sand, small to large rounded to sub-rounded 10 gravel, loose, poorly sorted, dry, brown. 12 SAND with GRAVEL 13 coarse and medium grained sand, small to large rounded to sub-rounded gravel, loose, wet, brown. Mottling at 13.7 m 14 (45 ft), approximately 1 cm thick. 15 16 17 17.4 m - 21.2 m bgs 10-20 Filter sand 18 19 18.1 m -21.2 m bgs 2 inch diameter 10 slot PVC screen 3 m (10 ft) length with bottom plug 20 SAND, with some silty clay chunks, fine and medium grained sand, 21 loose, wet, brown. Total Well Depth 21.1 m (69.2 ft) below top of casing (btoc) 22 COORDINATES: 11U 3142761.6 m E 5450263.7 m N ELEVATION: 336 m asl (gps)

STATIC WATER LEVEL: Dry

TOTAL DEPTH: 21.1 m btoc

DRILLING METHOD: Sonic rubber track rig

Drawn	By:	MJ	

Reviewed By: RR

DRILLING CONTRACTOR: Mud Bay Drilling Ltd.

Logged By: MJ



MONITORING WELL LOG MW-10

Consultants in Hydrogeology and Water Resources Management SHEET 1 of 1 **MONITORING WELL ID: MW-10** DATE DRILLED: May 6, 2021 **PROJECT: Town of Oliver Monitoring Well Installation** SITE LOCATION: Gala St. Linear Park **CLIENT: Town of Oliver** PROJECT NUMBER: 20-046-02VR DEPTH LITHOLOGY DESCRIPTION WELL CONSTUCTION WELL COMPLETION DETAILS (m) Flushmount box, cemented in place **Ground Surface** 0 0.1 m - 25.7 m bgs Blank 2 inch diameter PVC with TOPSOIL J-plug cap 1 0.2 m - 0.6 m bgs 10-20 Filter sand 2 GRAVEL with SAND, medium and coarse grained 3 0.6 m - 2.1 m bgs Suface seal, Enviroplug medium sand, small to large rounded to bentonite chips sub-rounded gravel, loose, poorly 4 sorted, dry, brown. Mottling approximately 14.3 m and 21 m 5 (47 ft and 68 ft) below ground surface. 6 8 9 10 11 2.1 m - 25 m bgs Alternating layers of appoximately 1 m bentonite seal with 4.5 m of natural sluff 12-13 14 15 16 17 18 19 20-21 GRAVEL, small to large rounded to 22 sub-rounded gravel, loose, Water level 25.1 m (82.3 ft) below top of casing (btoc) wet brown 23 (May 6, 2021) 24 25 m - 27.2 m bgs 10-20 Filter sand 25 25.7 m - 27.2 m bgs 2 inch diameter 10 slot PVC screen 26 1.5 m (5 ft) length with bottom plug 27 SAND with some SILT, Total Well Depth 27.1 m btoc fine with some medium grained 28 sand, loose, wet, brown. 29 COORDINATES: 11U 313762.5 m E 5450678.4 m N ELEVATION: 326 m asl (gps) STATIC WATER LEVEL: 25.1 m btoc DRILLING CONTRACTOR: Mud Bay Drilling Ltd. TOTAL DEPTH: 27.1 m btoc DRILLING METHOD: Sonic rubber track rig Drawn By: MJ Reviewed By: RR Logged By: MJ



MONITORING WELL LOG MW-11

MONITORING WELL ID: MW-11

PROJECT: Town of Oliver Monitoring Well Installation

CLIENT: Town of Oliver

DATE DRILLED: May 6-7, 2021 SITE LOCATION: West end 332 Ave

PROJECT NUMBER: 20-046-02VR

DEPTH (m)	LITHOLOGY DESCRIPTION	WELL CONSTUCTION	WELL COMPLETION DETAILS
0	Ground Surface SAND with GRAVEL, fine and medium grained sand, small to large rounded to sub-rounded gravel, loose, poorly sorted, dry, brown. SAND, with Silt lenses, fine and medium grained sand, loose, poorly sorted, dry, grey.		 Well stick-up 0.86 m above ground surface (ags) 0.86 m ags - 27.1 m below ground surface (bgs) Blank 2 inch diameter PVC with J-plug cap. Above ground lockabel monument casing, cemented in place 0.7 m ags - 0.6 m bgs 10-20 Filter sand 0.6 m - 6.1 m bgs Surface seal, Enviroplug medium bentonite chips
9 10 11 12 13 14 15 16 17 18 17 18 19	SAND with GRAVEL, fine and medium grained sand, small to large rounded to sub-rounded gravel, loose, poorly sorted, dry, brown. SAND, fine grained, loose, well sorted, dry, brown. SAND with GRAVEL, fine and medium grained sand, small to large rounded to sub-rounded gravel, loose, poorly sorted, dry, brown. SAND, with compact Silt and Clay lenses, fine and medium grained sand, loose, poorly sorted, dry, grey.		6.1 m - 25.6 m bgs Alternating layers of approximately 1 m bentonite seal with 4.5 m of natural sluff
20 21 22 23 24 25 26 27 26 27 28 27 28	SAND with GRAVEL, fine and medium grained sand, small to large rounded to sub-rounded gravel, loose, poorly sorted, dry, brown. SAND, with compact Silt and Clay lenses, fine and medium grained sand, loose, poorly sorted, dry, grey. SAND and SILT, fine grained sand, loose, poorly sorted, moist, brown. Increased moisture at 19.2 m, 20.7 m and21 m (63 ft, 68 ft and 69 ft) bgs. Mottling throughout.		Water level 25.1 m (82.3 ft) below top of casing (btoc) (May 6, 2021) 25.6 m - 29.7 m bgs 10-20 Filter Sand 27.1 m - 29.7 m bgs 2 inch diameter 10 slot PVC screen
29			3 m (10 ft) length with bottom plug
30 31			Total Well Depth 30.6 m btoc
COORDIN	NATES: 11U 311235.0 m E 5448302.0 m N	ELEVATION: 356 m	n asl (gps)
STATIC V	NATER LEVEL: 24.3 m btoc	DRILLING CONTRA	ACTOR: Mud Bay Drilling Ltd.
FOTAL D	EPTH: 30.6 m btoc	DRILLING METHOD	D: Sonic rubber track rig
Drawn By	<u>v.</u> M1	Reviewed By: RR	Logged By: MJ



CERTIFICATE OF ANALYSIS

REPORTED TO	Western Water Associates Ltd 106 - 5145 26th Street Vernon, BC V1T 8G4		
ATTENTION	Morgan Jackson	WORK ORDER	21E2339
PO NUMBER PROJECT PROJECT INFO	20-046-02VR	RECEIVED / TEMP REPORTED COC NUMBER	2021-05-20 09:52 / 11.0°C 2021-06-23 08:49 B099390

Introduction:

CARO Analytical Services is a testing laboratory full of smart, engaged scientists driven to make the world a safer and healthier place. Through our clients' projects we become an essential element for a better world. We employ methods conducted in accordance with recognized professional standards using accepted testing methodologies and quality control efforts. CARO is accredited by the Canadian Association for Laboratories Accreditation (CALA) to ISO/IEC 17025:2017 for specific tests listed in the scope of accreditation approved by CALA.

Big Picture Sidekicks



You know that the sample you collected after snowshoeing to site, digging 5 meters, and racing to get it on a plane so you can submit it to the lab for time sensitive results needed to make important and expensive decisions (whew) is VERY important. We know that too. It's simple. We figure the more you

We've Got Chemistry

enjoy working with our fun and engaged team members; the more likely you are to give us continued opportunities to support you.

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Ahead of the Curve

0

Through research, regulation knowledge, and instrumentation, we are your analytical centre for the technical knowledge you need, BEFORE you need it, so you can stay up to date and in the know.

Note: Sample ID "duplicate" is a duplicate for MW11. Samples with Laboratory ID's ending in "RE1" were rerun at the request of WWAL to evaluate QA/QC.

If you have any questions or concerns, please contact me at bwhitehead@caro.ca

Authorized By:

Brent Whitehead Client Scientist - Team Lead

V undburt

1-888-311-8846 | www.caro.ca

#110 4011 Viking Way Richmond, BC V6V 2K9 | #102 3677 Highway 97N Kelowna, BC V1X 5C3 | 17225 109 Avenue Edmonton, AB T5S 1H7 | #108 4475 Wayburne Drive Burnaby, BC V5G 4X4



5-19 07:30 3.3 A		WORK ORDER REPORTED	21E2339 2021-06-2 Analyzed	3 08:49 Qualifier
5-19 07:30 3.3 A		L Units	Analyzed	Qualifier
3.3 A	O ≤ 250 0 ²			
	O ≤ 250 0 ²			
	O ≤ 250 0 ²			
45 N		10 mg/L	2021-05-21	
	IAC = 10 0.0 ²	10 mg/L	2021-05-21	
10 N	MAC = 1 0.01	10 mg/L	2021-05-21	
12 Nor	e Required 0.50)0 mg/L	N/A	
	•	0	N/A	
24	N/A 0.050)0 mg/L	N/A	
50 Nor	e Required 0.08	50 mg/L	2021-05-25	
05	N/A 2	.0 μS/cm	2021-05-26	
92	N/A 0.05	50 mg/L	2021-05-28	
94	7.0-10.5 0.1	10 pH units	2021-05-26	HT2
85	N/A 0.005	50 mg/L	2021-05-27	
17	N/A 0.005	50 mg/L	2021-05-27	
<1 N	/IAC = 0	1 MPN/100 mL	2021-05-20	HT1
< 1 N	/AC = 0	1 MPN/100 mL	2021-05-20	HT1
9.4 Nor	e Required 0.2	20 mg/L	2021-05-27	
		-	2021-05-27	
		10 mg/L	2021-05-27	
	45 24 50 Non 05 92 94 7 85 17 < 1 M < 1 M 9.4 Non	45 10 0.010 24 N/A 0.050 50 None Required 0.05 95 N/A 2 92 N/A 0.05 94 7.0-10.5 0.1 85 N/A 0.005 17 N/A 0.005 21 MAC = 0 0 94 None Required 0.2 94 None Required 0.2	45 10 0.0100 mg/L 24 N/A 0.0500 mg/L 50 None Required 0.050 mg/L 95 N/A 2.0 µS/cm 92 N/A 0.050 mg/L 94 7.0-10.5 0.10 pH units 85 N/A 0.0050 mg/L 17 N/A 0.0050 mg/L <1	45 10 0.0100 mg/L N/A 24 N/A 0.0500 mg/L N/A 50 None Required 0.050 mg/L 2021-05-25 05 N/A 2.0 μS/cm 2021-05-26 92 N/A 0.050 mg/L 2021-05-26 94 7.0-10.5 0.10 pH units 2021-05-26 85 N/A 0.0050 mg/L 2021-05-27 17 N/A 0.0050 mg/L 2021-05-27 <1

Calculated Parameters

Nitrite (as N)

Hardness, Total (as CaCO3)	343	None Required	0.500 mg/L	N/A	
Nitrate+Nitrite (as N)	4.63	10	0.0100 mg/L	N/A	
Nitrogen, Total	4.91	N/A	0.0500 mg/L	N/A	

MAC = 1

0.010 mg/L

< 0.010

General Parameters

Ammonia, Total (as N)	< 0.050	None Required	0.050 mg/L	2021-05-25	
Conductivity (EC)	978	N/A	2.0 µS/cm	2021-05-26	
Nitrogen, Total Kjeldahl	0.282	N/A	0.050 mg/L	2021-05-28	
рН	7.31	7.0-10.5	0.10 pH units	2021-05-26	HT2
Phosphorus, Total (as P)	0.0497	N/A	0.0050 mg/L	2021-05-27	
Phosphorus, Total Dissolved	0.0239	N/A	0.0050 mg/L	2021-05-27	
					Page 2 of 10

10 age 2 of

2021-05-21



REPORTED TO Western Water Associates Ltd PROJECT 20-046-02VR			WORK ORDER REPORTED		21E2339 2021-06-23 08:49	
Analyte	Result	Guideline	RL	Units	Analyzed	Qualifie
MW-10 (21E2339-02) Matrix: Water	Sampled: 2021-05-19	08:00, Continued				
Microbiological Parameters						
Coliforms, Total	< 1	MAC = 0	1	MPN/100 mL	2021-05-20	HT1
E. coli	< 1	MAC = 0	1	MPN/100 mL	2021-05-20	HT1
Total Metals						
Calcium, total	82.5	None Required	0.20	mg/L	2021-05-27	
Magnesium, total	33.2	None Required	0.010	-	2021-05-27	
Sodium, total	36.7	AO ≤ 200	0.10	mg/L	2021-05-27	
Anions						
Chloride	157	AO ≤ 250	0 10	mg/L	2021-05-21	
Nitrate (as N)	3.13	MAC = 10	0.010	-	2021-05-21	
Nitrite (as N)	0.010	MAC = 1	0.010	mg/L	2021-05-21	
Calculated Parameters						
Hardness, Total (as CaCO3)	470	None Required	0.500	mg/L	N/A	
Nitrate+Nitrite (as N)	3.14	10	0.0100		N/A	
Nitrogen, Total	3.38	N/A	0.0500	mg/L	N/A	
General Parameters						
Ammonia, Total (as N)	< 0.050	None Required	0.050	mg/L	2021-05-25	
Ammonia, Total (as N) Conductivity (EC)	< 0.050 1220	None Required N/A		mg/L μS/cm	2021-05-25 2021-05-26	
				μS/cm		
Conductivity (EC)	1220	N/A	2.0 0.050	μS/cm	2021-05-26	HT2
Conductivity (EC) Nitrogen, Total Kjeldahl	1220 0.241	N/A N/A	2.0 0.050	μS/cm mg/L pH units	2021-05-26 2021-05-28	HT2
Conductivity (EC) Nitrogen, Total Kjeldahl pH	1220 0.241 7.04	N/A N/A 7.0-10.5	2.0 0.050 0.10	μS/cm mg/L pH units mg/L	2021-05-26 2021-05-28 2021-05-26	HT2
Conductivity (EC) Nitrogen, Total Kjeldahl pH Phosphorus, Total (as P) Phosphorus, Total Dissolved	1220 0.241 7.04 0.0880	N/A N/A 7.0-10.5 N/A	2.0 0.050 0.10 0.0050	μS/cm mg/L pH units mg/L	2021-05-26 2021-05-28 2021-05-26 2021-05-27	HT2
Conductivity (EC) Nitrogen, Total Kjeldahl pH Phosphorus, Total (as P) Phosphorus, Total Dissolved	1220 0.241 7.04 0.0880	N/A N/A 7.0-10.5 N/A	2.0 0.050 0.10 0.0050 0.0050	μS/cm mg/L pH units mg/L	2021-05-26 2021-05-28 2021-05-26 2021-05-27	HT2 HT1
Conductivity (EC) Nitrogen, Total Kjeldahl pH Phosphorus, Total (as P) Phosphorus, Total Dissolved Microbiological Parameters	1220 0.241 7.04 0.0880 0.0264	N/A N/A 7.0-10.5 N/A N/A	2.0 0.050 0.10 0.0050 0.0050	μS/cm mg/L pH units mg/L mg/L	2021-05-26 2021-05-28 2021-05-26 2021-05-27 2021-05-27	
Conductivity (EC) Nitrogen, Total Kjeldahl pH Phosphorus, Total (as P) Phosphorus, Total Dissolved <i>Microbiological Parameters</i> Coliforms, Total E. coli	1220 0.241 7.04 0.0880 0.0264 < 1	N/A N/A 7.0-10.5 N/A N/A MAC = 0	2.0 0.050 0.10 0.0050 0.0050	μS/cm mg/L pH units mg/L mg/L MPN/100 mL	2021-05-26 2021-05-28 2021-05-27 2021-05-27 2021-05-27	HT1
Conductivity (EC) Nitrogen, Total Kjeldahl pH Phosphorus, Total (as P) Phosphorus, Total Dissolved <i>Microbiological Parameters</i> Coliforms, Total E. coli	1220 0.241 7.04 0.0880 0.0264 < 1	N/A N/A 7.0-10.5 N/A N/A MAC = 0	2.0 0.050 0.10 0.0050 0.0050 1 1	μS/cm mg/L pH units mg/L mg/L MPN/100 mL	2021-05-26 2021-05-28 2021-05-27 2021-05-27 2021-05-27	HT1
Conductivity (EC) Nitrogen, Total Kjeldahl pH Phosphorus, Total (as P) Phosphorus, Total Dissolved Microbiological Parameters Coliforms, Total E. coli Total Metals	1220 0.241 7.04 0.0880 0.0264 < 1 < 1	N/A N/A 7.0-10.5 N/A N/A MAC = 0 MAC = 0	2.0 0.050 0.10 0.0050 0.0050 1 1	μS/cm mg/L pH units mg/L mg/L MPN/100 mL MPN/100 mL mg/L	2021-05-26 2021-05-28 2021-05-27 2021-05-27 2021-05-20 2021-05-20	HT1

MW-11 (21E2339-03RE1) | Matrix: Water | Sampled: 2021-05-19 08:50

General Parameters					
Nitrogen, Total Kjeldahl	0.267	N/A	0.050 mg/L	2021-06-21	HT1
Phosphorus, Total Dissolved	0.0273	N/A	0.0050 mg/L	2021-06-18	HT1



REPORTED TO PROJECT	Western Water Associate 20-046-02VR	es Ltd			WORK ORDER REPORTED	21E2339 2021-06-2	3 08:49
Analyte		Result	Guideline	RL	Units	Analyzed	Qualifie
Duplicate (21E23	39-04) Matrix: Water Sa	mpled: 2021-05	-19				
Anions							
Chloride		150	AO ≤ 250	0.10	mg/L	2021-05-21	
Nitrate (as N)		3.04	MAC = 10	0.010	mg/L	2021-05-21	
Nitrite (as N)		< 0.010	MAC = 1	0.010	mg/L	2021-05-21	
Calculated Parame	eters						
Hardness, Total (a	as CaCO3)	493	None Required	0.500	mg/L	N/A	
Nitrate+Nitrite (as		3.04	10	0.0100	•	N/A	
Nitrogen, Total		3.50	N/A	0.0500	-	N/A	
General Parameter	'S						
Ammonia, Total (a	as N)	< 0.050	None Required	0.050	ma/L	2021-05-25	
Conductivity (EC)	,	1200	N/A		μS/cm	2021-05-26	
Nitrogen, Total Kje		0.454	N/A	0.050	•	2021-05-28	
pH		7.10	7.0-10.5		pH units	2021-05-26	HT2
Phosphorus, Total	l (as P)	0.0861	N/A	0.0050	mg/L	2021-05-27	
Phosphorus, Total	Dissolved	0.0338	N/A	0.0050	mg/L	2021-05-27	
Total Metals							
Calcium, total		114	None Required	0.20	mg/L	2021-05-27	
Magnesium, total		50.3	None Required	0.010	mg/L	2021-05-27	
Sodium, total		83.8	AO ≤ 200	0.10	mg/L	2021-05-27	
Duplicate (21E23	39-04RE1) Matrix: Water	Sampled: 202	1-05-19				
0							
			N//A	0.050		0004 00 04	
Nitrogen, Total Kje	eldahl	0.398	N/A	0.050	0	2021-06-21	HT1
Nitrogen, Total Kje Phosphorus, Total	eldahl	0.0332	N/A	0.050	0	2021-06-21 2021-06-18	HT1 HT1
Nitrogen, Total Kje Phosphorus, Total MW-6 (21E2339-0	eldahl I Dissolved	0.0332	N/A		0		
Nitrogen, Total Kje Phosphorus, Total /IW-6 (21E2339-0	eldahl I Dissolved	0.0332	N/A	0.0050	0		
Nitrogen, Total Kje Phosphorus, Total //W-6 (21E2339-0 Anions	eldahl I Dissolved	0.0332 ed: 2021-05-19	N/A 07:00	0.0050	mg/L mg/L	2021-06-18	
Nitrogen, Total Kje Phosphorus, Total MW-6 (21E2339-0 Anions Chloride	eldahl I Dissolved	0.0332 ed: 2021-05-19 91.6	N/A 07:00 AO ≤ 250	0.0050	mg/L mg/L mg/L	2021-06-18 2021-05-21	
Nitrogen, Total Kje Phosphorus, Total MW-6 (21E2339-0 Anions Chloride Nitrate (as N) Nitrite (as N)	eldahl I Dissolved 95) Matrix: Water Sample	0.0332 ed: 2021-05-19 91.6 1.99	N/A 07:00 AO ≤ 250 MAC = 10	0.0050	mg/L mg/L mg/L	2021-06-18 2021-05-21 2021-05-21	
Nitrogen, Total Kje Phosphorus, Total Alw-6 (21E2339-0 Anions Chloride Nitrate (as N) Nitrite (as N) Calculated Parame	eldahl I Dissolved 05) Matrix: Water Sample	0.0332 ed: 2021-05-19 91.6 1.99	N/A 07:00 AO ≤ 250 MAC = 10	0.0050	mg/L mg/L mg/L mg/L	2021-06-18 2021-05-21 2021-05-21	
Phosphorus, Total WW-6 (21E2339-0 Anions Chloride Nitrate (as N)	eldahl I Dissolved 95) Matrix: Water Sampl 95: Sters as CaCO3)	0.0332 ed: 2021-05-19 91.6 1.99 < 0.010	N/A 07:00 AO ≤ 250 MAC = 10 MAC = 1	0.0050 0.10 0.010 0.010	mg/L mg/L mg/L mg/L	2021-06-18 2021-05-21 2021-05-21 2021-05-21	

General Parameters

Ammonia, Total (as N)	0.067	None Required	0.050 mg/L	2021-05-25
Conductivity (EC)	1060	N/A	2.0 µS/cm	2021-05-26
Nitrogen, Total Kjeldahl	0.625	N/A	0.050 mg/L	2021-05-28

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Page 4 of 10
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REPORTED TO PROJECT	Western Water Associa 20-046-02VR	ites Ltd			WORK ORDER REPORTED	21E2339 2021-06-2	23 08:49
Analyte		Result	Guideline	RL	Units	Analyzed	Qualifie
MW-6 (21E2339-0	95) Matrix: Water Samı	oled: 2021-05-19	07:00, Continued				
General Parameter	rs, Continued						
рН		7.02	7.0-10.5	0.10	pH units	2021-05-26	HT2
Phosphorus, Total	(as P)	0.251	N/A	0.0050	mg/L	2021-05-27	
Phosphorus, Total	Dissolved	0.0557	N/A	0.0050	mg/L	2021-05-27	
Microbiological Pa	rameters						
Coliforms, Total		5	MAC = 0	1	MPN/100 mL	2021-05-20	HT1
E. coli		< 1	MAC = 0	1	MPN/100 mL	2021-05-20	HT1
Total Metals							
Calcium, total		80.7	None Required	0.20	mg/L	2021-05-27	
Magnesium, total		34.7	None Required	0.010	mg/L	2021-05-27	
Sodium, total		109	AO ≤ 200	0.10	mg/L	2021-05-27	
Sample Qualifie	e rs: nple was prepared and/or a	nalyzed past the rec	commended holding tir	ne.			
HT2 The 1 recomm		holding time (from sampling to	analysis) ha	as been exceed	ed - field	analysis i



APPENDIX 1: SUPPORTING INFORMATION

REPORTED TO	Western Water Associates Ltd
PROJECT	20-046-02VR

WORK ORDER 21E REPORTED 202

21E2339 2021-06-23 08:49

Analysis Description	Method Ref.	Technique A	Accredited	Location
Ammonia, Total in Water	SM 4500-NH3 G* (2017)	Automated Colorimetry (Phenate)	~	Kelowna
Anions in Water	SM 4110 B (2017)	Ion Chromatography	✓	Kelowna
Coliforms, Total in Water	NA / SM 9223 (2017)	Quanti-Tray / Enzyme Substrate Endo Agar	✓	Kelowna
Conductivity in Water	SM 2510 B (2017)	Conductivity Meter	✓	Kelowna
E. coli in Water	NA / SM 9223 (2017)	Quanti-Tray / Enzyme Substrate Endo Agar	✓	Kelowna
Hardness in Water	SM 2340 B* (2017)	Calculation: 2.497 [total Ca] + 4.118 [total Mg] (Est)	✓	N/A
Nitrogen, Total Kjeldahl in Water	SM 4500-Norg D* (2017)	Block Digestion and Flow Injection Analysis	✓	Kelowna
pH in Water	SM 4500-H+ B (2017)	Electrometry	✓	Kelowna
Phosphorus, Total Dissolved in Water	SM 4500-P B.5* (2011) / SM 4500-P F (2017)	Persulfate Digestion / Automated Colorimetry (Ascorbic A	cid) ✓	Kelowna
Phosphorus, Total in Water	SM 4500-P B.5* (2011) / SM 4500-P F (2017)	Persulfate Digestion / Automated Colorimetry (Ascorbic A	cid) ✓	Kelowna
Total Metals in Water	EPA 200.2 / EPA 6020B	HNO3+HCl Hot Block Digestion / Inductively Coupled Plasma-Mass Spectroscopy (ICP-MS)	✓	Richmond

Note: An asterisk in the Method Reference indicates that the CARO method has been modified from the reference method

Glossary of Terms:

RL	Reporting Limit (default)
<	Less than the specified Reporting Limit (RL) - the actual RL may be higher than the default RL due to various factors
AO	Aesthetic Objective
MAC	Maximum Acceptable Concentration (health based)
mg/L	Milligrams per litre
MPN/100 mL	Most Probable Number per 100 millilitres
pH units	pH < 7 = acidic, ph > 7 = basic
μS/cm	Microsiemens per centimetre
EPA	United States Environmental Protection Agency Test Methods
SM	Standard Methods for the Examination of Water and Wastewater, American Public Health Association

Guidelines Referenced in this Report:

BC CSR Schedule 3.2 Drinking Water

Guidelines for Canadian Drinking Water Quality (Health Canada, June 2019)

Note: In some cases, the values displayed on the report represent the lowest guideline and are to be verified by the end user



APPENDIX 1: SUPPORTING INFORMATION

REPORTED TO	Western Water Associates Ltd
PROJECT	20-046-02VR

WORK ORDER 21 REPORTED 20

21E2339 2021-06-23 08:49

General Comments:

The results in this report apply to the samples analyzed in accordance with the Chain of Custody document. This analytical report must be reproduced in its entirety. CARO is not responsible for any loss or damage resulting directly or indirectly from error or omission in the conduct of testing. Liability is limited to the cost of analysis. Samples will be disposed of 30 days after the test report has been issued or once samples expire, whichever comes first. Longer hold is possible if agreed to in writing.

Results in **Bold** indicate values that are above CARO's method reporting limits. Any results that are above regulatory limits are highlighted **red**. Please note that results will only be highlighted red if the regulatory limits are included on the CARO report. Any Bold and/or highlighted results do <u>not</u> take into account method uncertainty. If you would like method uncertainty or regulatory limits to be included on your report, please contact your Account Manager:bwhitehead@caro.ca

Please note any regulatory guidelines applied to this report are added as a convenience to the client, at their request, to help provide some initial context to analytical results obtained. Although CARO makes every effort to ensure accuracy of the associated regulatory guideline(s) applied, the guidelines applied cannot be assumed to be correct due to a variety of factors and as such CARO Analytical Services assumes no liability or responsibility for the use of those guidelines to make any decisions. The original source of the regulation should be verified and a review of the guideline (s) should be validated as correct in order to make any decisions arising from the comparison of the analytical data obtained to the relevant regulatory guideline for one's particular circumstances. Further, CARO Analytical Services assumes no liability or responsibility for any loss attributed from the use of these guidelines in any way.



APPENDIX 2: QUALITY CONTROL RESULTS

REPORTED TO	Western Water Associates Ltd	WORK ORDER	21E2339
PROJECT	20-046-02VR	REPORTED	2021-06-23 08:49

The following section displays the quality control (QC) data that is associated with your sample data. Groups of samples are prepared in "batches" and analyzed in conjunction with QC samples that ensure your data is of the highest quality. Common QC types include:

- Method Blank (Blk): A blank sample that undergoes sample processing identical to that carried out for the test samples. Method blank results are used to assess contamination from the laboratory environment and reagents.
- **Duplicate (Dup)**: An additional or second portion of a randomly selected sample in the analytical run carried through the entire analytical process. Duplicates provide a measure of the analytical method's precision (reproducibility).
- Blank Spike (BS): A sample of known concentration which undergoes processing identical to that carried out for test samples, also referred to as a laboratory control sample (LCS). Blank spikes provide a measure of the analytical method's accuracy.
- Matrix Spike (MS): A second aliquot of sample is fortified with with a known concentration of target analytes and carried through the entire analytical process. Matrix spikes evaluate potential matrix effects that may affect the analyte recovery.
- **Reference Material (SRM)**: A homogenous material of similar matrix to the samples, certified for the parameter(s) listed. Reference Materials ensure that the analytical process is adequate to achieve acceptable recoveries of the parameter(s) tested.

Each QC type is analyzed at a 5-10% frequency, i.e. one blank/duplicate/spike for every 10-20 samples. For all types of QC, the specified recovery (% Rec) and relative percent difference (RPD) limits are derived from long-term method performance averages and/or prescribed by the reference method.

Analyte	Result	RL Units	Spike	Source	% REC	REC	% RPD RPD	Qualifier
, maly to	Rooun		Level	Result	/011120	Limit	Limi	

Anions, Batch B1E2150

Blank (B1E2150-BLK1)			Prepared: 202	1-05-21, Analyze	ed: 2021-05-21	
Chloride	< 0.10	0.10 mg/L				
Nitrate (as N)	< 0.010	0.010 mg/L				
Nitrite (as N)	< 0.010	0.010 mg/L				
Blank (B1E2150-BLK2)			Prepared: 202	1-05-21, Analyzo	ed: 2021-05-21	
Chloride	< 0.10	0.10 mg/L				
Nitrate (as N)	< 0.010	0.010 mg/L				
Nitrite (as N)	< 0.010	0.010 mg/L				
LCS (B1E2150-BS1)			Prepared: 202	1-05-21, Analyze	ed: 2021-05-21	
Chloride	15.8	0.10 mg/L	16.0	99	90-110	
Nitrate (as N)	4.00	0.010 mg/L	4.00	100	90-110	
Nitrite (as N)	2.00	0.010 mg/L	2.00	100	85-115	
LCS (B1E2150-BS2)			Prepared: 202	1-05-21, Analyze	ed: 2021-05-21	
Chloride	16.1	0.10 mg/L	16.0	100	90-110	
Onlonde						
Nitrate (as N)	4.01	0.010 mg/L	4.00	100	90-110	

General Parameters, Batch B1E2319

Blank (B1E2319-BLK1)			Prepared: 2021-05-25, Analyzed: 2021-05-25
Ammonia, Total (as N)	< 0.050	0.050 mg/L	
Blank (B1E2319-BLK2)			Prepared: 2021-05-25, Analyzed: 2021-05-25
Ammonia, Total (as N)	< 0.050	0.050 mg/L	
Blank (B1E2319-BLK3)			Prepared: 2021-05-25, Analyzed: 2021-05-25
Ammonia, Total (as N)	< 0.050	0.050 mg/L	
Blank (B1E2319-BLK4)			Prepared: 2021-05-25, Analyzed: 2021-05-25
Ammonia, Total (as N)	< 0.050	0.050 mg/L	
Blank (B1E2319-BLK5)			Prepared: 2021-05-25, Analyzed: 2021-05-25
Ammonia, Total (as N)	< 0.050	0.050 mg/L	



Nitrogen, Total Kjeldahl

APPENDIX 2: QUALITY CONTROL RESULTS

PROJECT	Western Water Assoc 20-046-02VR	ciates Ltd				WORK REPOR	ORDER TED	21E2 2021	2339 -06-23	08:49
Analyte		Result	RL Units	Spike Level	Source Result	% REC	REC Limit	% RPD	RPD Limit	Qualifier
General Parameters,	Batch B1E2319, Cont	inued								
LCS (B1E2319-BS1))			Prepared	: 2021-05-2	5, Analyze	d: 2021-0	5-25		
Ammonia, Total (as N)		1.04	0.050 mg/L	1.00		104	90-115			
LCS (B1E2319-BS2)				Prepared	: 2021-05-2	5 Analyze	d [.] 2021-0	5-25		
Ammonia, Total (as N)	·	0.980	0.050 mg/L	1.00		98	90-115			
LCS (B1E2319-BS3)			ŭ	Prenared	: 2021-05-2	5 Analyza	d. 2021-0	5_25		
Ammonia, Total (as N)		0.943	0.050 mg/L	1.00	. 2021-03-20	94	90-115	5-25		
		0.945	0.000 mg/L		0004 05 0			5 05		
LCS (B1E2319-BS4)		0.000	0.050		: 2021-05-2			5-25		
Ammonia, Total (as N)		0.963	0.050 mg/L	1.00		96	90-115			
LCS (B1E2319-BS5)					: 2021-05-2			5-25		
Ammonia, Total (as N)		1.08	0.050 mg/L	1.00		108	90-115			
Duplicate (B1E2319	-DUP4)	Sou	rce: 21E2339-01	Prepared	: 2021-05-2	5, Analyze	d: 2021-0	5-25		
Ammonia, Total (as N)		< 0.050	0.050 mg/L		< 0.050				15	
Matrix Spike (B1E23	319-MS4)	Sou	rce: 21E2339-01	Prepared	: 2021-05-2	5, Analyze	d: 2021-0	5-25		
Ammonia, Total (as N)		0.204	0.050 mg/L	0.250	< 0.050	82	75-125			
Blank (B1E2448-BL Conductivity (EC)	K1)	< 2.0	2.0 µS/cm	Prepared	: 2021-05-26	6, Analyze	d: 2021-0	5-26		
Conductivity (EC)			· · · · · · · · · · · · · · · · · · ·	Prepared	: 2021-05-26 : 2021-05-26	δ, Analyze	d: 2021-0			
Conductivity (EC) LCS (B1E2448-BS1) Conductivity (EC)	·	< 2.0 1410	2.0 μS/cm 2.0 μS/cm	Prepared 1410	: 2021-05-26	6, Analyze	d: 2021-0 95-105	5-26		
Conductivity (EC)	·		· · · · · · · · · · · · · · · · · · ·	Prepared 1410		6, Analyze	d: 2021-0 95-105	5-26		
Conductivity (EC) LCS (B1E2448-BS1) Conductivity (EC) Reference (B1E2444 pH General Parameters, Blank (B1E2546-BL	3-SRM1) Batch B1E2546	7.00	2.0 µS/cm 0.10 pH units	Prepared 1410 Prepared 7.01	: 2021-05-26	5, Analyze 100 5, Analyze 100	d: 2021-0 95-105 d: 2021-0 98-102	5-26 5-26		
Conductivity (EC) LCS (B1E2448-BS1) Conductivity (EC) Reference (B1E2444 pH General Parameters, Blank (B1E2546-BL Phosphorus, Total (as	B-SRM1) Batch B1E2546 K1)	1410 7.00 < 0.0050	2.0 μS/cm 0.10 pH units 0.0050 mg/L	Prepared 1410 Prepared 7.01	: 2021-05-26 : 2021-05-26	5, Analyze 100 5, Analyze 100	d: 2021-0 95-105 d: 2021-0 98-102	5-26 5-26		
Conductivity (EC) LCS (B1E2448-BS1) Conductivity (EC) Reference (B1E2444 pH General Parameters, Blank (B1E2546-BL Phosphorus, Total (as Phosphorus, Total Diss	B-SRM1) Batch B1E2546 K1) D) olved	7.00	2.0 µS/cm 0.10 pH units	Prepared 1410 Prepared 7.01 Prepared	: 2021-05-26 : 2021-05-26 : 2021-05-26	5, Analyze 100 5, Analyze 100 5, Analyze	d: 2021-0 95-105 d: 2021-0 98-102 d: 2021-0	5-26 5-26 5-27		
Conductivity (EC) LCS (B1E2448-BS1) Conductivity (EC) Reference (B1E2444 pH General Parameters, Blank (B1E2546-BL Phosphorus, Total Diss Blank (B1E2546-BL	B-SRM1) Batch B1E2546 K1) Dived K2)	1410 7.00 < 0.0050 < 0.0050	2.0 µS/cm 0.10 pH units 0.0050 mg/L 0.0050 mg/L	Prepared 1410 Prepared 7.01 Prepared	: 2021-05-26 : 2021-05-26	5, Analyze 100 5, Analyze 100 5, Analyze	d: 2021-0 95-105 d: 2021-0 98-102 d: 2021-0	5-26 5-26 5-27		
Conductivity (EC) LCS (B1E2448-BS1) Conductivity (EC) Reference (B1E2444 pH General Parameters, Blank (B1E2546-BL Phosphorus, Total Diss Blank (B1E2546-BL Phosphorus, Total (as l	B-SRM1) Batch B1E2546 K1) D) olved K2) D)	1410 7.00 < 0.0050 < 0.0050 < 0.0050	2.0 µS/cm 0.10 pH units 0.0050 mg/L 0.0050 mg/L	Prepared 1410 Prepared 7.01 Prepared	: 2021-05-26 : 2021-05-26 : 2021-05-26	5, Analyze 100 5, Analyze 100 5, Analyze	d: 2021-0 95-105 d: 2021-0 98-102 d: 2021-0	5-26 5-26 5-27		
Conductivity (EC) LCS (B1E2448-BS1) Conductivity (EC) Reference (B1E2444 pH General Parameters, Blank (B1E2546-BL Phosphorus, Total Diss Blank (B1E2546-BL	Batch B1E2546 K1) olved K2) olved	1410 7.00 < 0.0050 < 0.0050	2.0 µS/cm 0.10 pH units 0.0050 mg/L 0.0050 mg/L	Prepared 1410 Prepared 7.01 Prepared Prepared	: 2021-05-26 : 2021-05-26 : 2021-05-26	5, Analyze 100 5, Analyze 100 5, Analyze 5, Analyze	d: 2021-0 95-105 d: 2021-0 98-102 d: 2021-0 d: 2021-0	5-26 5-26 5-27 5-27		
Conductivity (EC) LCS (B1E2448-BS1) Conductivity (EC) Reference (B1E2444 pH General Parameters, Blank (B1E2546-BL Phosphorus, Total (as Phosphorus, Total Diss Blank (B1E2546-BL Phosphorus, Total (as	B-SRM1) Batch B1E2546 K1) D) olved K2) D) olved	1410 7.00 < 0.0050 < 0.0050 < 0.0050	2.0 µS/cm 0.10 pH units 0.0050 mg/L 0.0050 mg/L	Prepared 1410 Prepared 7.01 Prepared Prepared	: 2021-05-26 : 2021-05-26 : 2021-05-26 : 2021-05-26	5, Analyze 100 5, Analyze 100 5, Analyze 5, Analyze	d: 2021-0 95-105 d: 2021-0 98-102 d: 2021-0 d: 2021-0	5-26 5-26 5-27 5-27		
Conductivity (EC) LCS (B1E2448-BS1) Conductivity (EC) Reference (B1E2444 pH General Parameters, Blank (B1E2546-BL Phosphorus, Total (as Phosphorus, Total Diss Blank (B1E2546-BL Phosphorus, Total (as Phosphorus, Total (as Phosphorus, Total (as) Phosphorus, Total Diss LCS (B1E2546-BS1)	Batch B1E2546 K1) D) olved K2) D) olved D) D)	1410 7.00 < 0.0050 < 0.0050 < 0.0050 < 0.0050	2.0 μS/cm 0.10 pH units 0.0050 mg/L 0.0050 mg/L 0.0050 mg/L	Prepared 1410 Prepared 7.01 Prepared Prepared	: 2021-05-26 : 2021-05-26 : 2021-05-26 : 2021-05-26	5, Analyze 100 5, Analyze 100 5, Analyze 5, Analyze 5, Analyze	d: 2021-0 95-105 d: 2021-0 98-102 d: 2021-0 d: 2021-0 d: 2021-0	5-26 5-26 5-27 5-27		
Conductivity (EC) LCS (B1E2448-BS1) Conductivity (EC) Reference (B1E2444 pH General Parameters, Blank (B1E2546-BL Phosphorus, Total (as Phosphorus, Total Diss Blank (B1E2546-BL Phosphorus, Total (as Phosphorus, Total (as Phosphorus, Total (as Phosphorus, Total (as	B-SRM1) Batch B1E2546 K1) D) olved K2) D) olved	1410 7.00 < 0.0050 < 0.0050 < 0.0050 < 0.0050 0.100	2.0 μS/cm 0.10 pH units 0.0050 mg/L 0.0050 mg/L 0.0050 mg/L 0.0050 mg/L	Prepared 1410 Prepared 7.01 Prepared Prepared 0.100 0.100	: 2021-05-26 : 2021-05-26 : 2021-05-26 : 2021-05-26	5, Analyze 100 5, Analyze 6, Analyze 6, Analyze 100 100	d: 2021-0 95-105 d: 2021-0 98-102 d: 2021-0 d: 2021-0 d: 2021-0 d: 2021-0 85-115	5-26 5-27 5-27 5-27		
Conductivity (EC) LCS (B1E2448-BS1) Conductivity (EC) Reference (B1E2444 pH General Parameters, Blank (B1E2546-BL Phosphorus, Total (as Phosphorus, Total (as	Batch B1E2546 K1) D) olved K2) D) olved D) olved D) D) D) D) D) D) D) D) D)	1410 7.00 < 0.0050 < 0.0050 < 0.0050 < 0.0050 0.100 0.100 0.100	2.0 μS/cm 0.10 pH units 0.0050 mg/L 0.0050 mg/L 0.0050 mg/L 0.0050 mg/L 0.0050 mg/L 0.0050 mg/L 0.0050 mg/L	Prepared 1410 Prepared 7.01 Prepared Prepared 0.100 0.100 Prepared 0.100	: 2021-05-26 : 2021-05-26 : 2021-05-26 : 2021-05-26 : 2021-05-26	5, Analyze 100 5, Analyze 100 5, Analyze 5, Analyze 100 100 5, Analyze 97	d: 2021-0 95-105 d: 2021-0 98-102 d: 2021-0 d: 2021-0 d: 2021-0 85-115 85-115 d: 2021-0 85-115	5-26 5-27 5-27 5-27		
Conductivity (EC) LCS (B1E2448-BS1) Conductivity (EC) Reference (B1E2444 pH General Parameters, Blank (B1E2546-BL Phosphorus, Total (as Phosphorus, Total Diss Blank (B1E2546-BL Phosphorus, Total Diss LCS (B1E2546-BS1) Phosphorus, Total (as Phosphorus, Total (as Phosphorus, Total Diss LCS (B1E2546-BS2) Phosphorus, Total (as Phosphorus, Total Diss	Batch B1E2546 K1) D Olived K2) D Olived D D Olived D D Olived D D Olived D D D Olived D D D D D D D D D D D D D D D D D D D	1410 7.00 < 0.0050 < 0.0050 < 0.0050 < 0.0050 0.100 0.100	2.0 μS/cm 0.10 pH units 0.0050 mg/L 0.0050 mg/L 0.0050 mg/L 0.0050 mg/L 0.0050 mg/L	Prepared 1410 Prepared 7.01 Prepared Prepared 0.100 0.100 Prepared	: 2021-05-26 : 2021-05-26 : 2021-05-26 : 2021-05-26 : 2021-05-26	5, Analyze 100 5, Analyze 100 5, Analyze 5, Analyze 100 100 5, Analyze	d: 2021-0 95-105 d: 2021-0 98-102 d: 2021-0 d: 2021-0 d: 2021-0 85-115 85-115 d: 2021-0	5-26 5-27 5-27 5-27		
Conductivity (EC) LCS (B1E2448-BS1) Conductivity (EC) Reference (B1E2444 pH General Parameters, Blank (B1E2546-BL Phosphorus, Total (as Phosphorus, Total Diss Blank (B1E2546-BL Phosphorus, Total Oiss LCS (B1E2546-BS1) Phosphorus, Total Diss LCS (B1E2546-BS2) Phosphorus, Total (as Phosphorus, Total Oiss LCS (B1E2546-BS2) Phosphorus, Total Oiss CS (B1E2546-BS2) Phosphorus, Total Oiss CS (B1E2546-BS2) Phosphorus, Total Oiss CS (B1E2546-BS2) Phosphorus, Total Oiss CS (B1E2546-BS2) CS (B1E25	Batch B1E2546 K1) P) olved K2) P) olved P) olved P) olved Batch B1E2548	1410 7.00 < 0.0050 < 0.0050 < 0.0050 < 0.0050 0.100 0.100 0.100	2.0 μS/cm 0.10 pH units 0.0050 mg/L 0.0050 mg/L 0.0050 mg/L 0.0050 mg/L 0.0050 mg/L 0.0050 mg/L 0.0050 mg/L	Prepared 1410 Prepared 7.01 Prepared Prepared 0.100 0.100 Prepared 0.100 0.100	: 2021-05-26 : 2021-05-26 : 2021-05-26 : 2021-05-26 : 2021-05-26 : 2021-05-26	5, Analyze 100 5, Analyze 100 5, Analyze 6, Analyze 100 100 5, Analyze 97 97	d: 2021-0 95-105 d: 2021-0 98-102 d: 2021-0 d: 2021-0 d: 2021-0 85-115 85-115 d: 2021-0 85-115 85-115 85-115	5-26 5-27 5-27 5-27 5-27 5-27		
Conductivity (EC) LCS (B1E2448-BS1) Conductivity (EC) Reference (B1E2444 pH General Parameters, Blank (B1E2546-BL Phosphorus, Total (as Phosphorus, Total (as Phosphorus, Total Diss LCS (B1E2546-BS1) Phosphorus, Total (as Phosphorus, Total (Batch B1E2546 K1) >) olved K2) >) olved >) olved >) olved >) olved (C) >) olved (C) (C) (C) (C) (C) (C) (C) (C)	1410 7.00 < 0.0050 < 0.0050 < 0.0050 < 0.0050 0.100 0.100 0.100	2.0 μS/cm 0.10 pH units 0.0050 mg/L 0.0050 mg/L 0.0050 mg/L 0.0050 mg/L 0.0050 mg/L 0.0050 mg/L 0.0050 mg/L	Prepared 1410 Prepared 7.01 Prepared Prepared 0.100 0.100 Prepared 0.100 0.100	: 2021-05-26 : 2021-05-26 : 2021-05-26 : 2021-05-26 : 2021-05-26	5, Analyze 100 5, Analyze 100 5, Analyze 6, Analyze 100 100 5, Analyze 97 97	d: 2021-0 95-105 d: 2021-0 98-102 d: 2021-0 d: 2021-0 d: 2021-0 85-115 85-115 d: 2021-0 85-115 85-115 85-115	5-26 5-27 5-27 5-27 5-27 5-27		

Caring About Results, Obviously.

0.050 mg/L

< 0.050



APPENDIX 2: QUALITY CONTROL RESULTS

REPORTED TO PROJECT	Western Water Associ 20-046-02VR	iates Ltd				WORK REPOR	ORDER	21E2 2021	2339 -06-23	08:49
Analyte		Result	RL Units	Spike Level	Source Result	% REC	REC Limit	% RPD	RPD Limit	Qualifie
General Parameters,	, Batch B1E2548, Conti	nued								
LCS (B1E2548-BS1))			Prepared	I: 2021-05-2	6, Analyze	d: 2021-0	5-28		
Nitrogen, Total Kjeldah		1.01	0.050 mg/L	1.00		101	85-115			
LCS (B1E2548-BS2))			Prenarec	I: 2021-05-2	6 Analyza	d. 2021-0	5-28		
Nitrogen, Total Kjeldah	•	0.998	0.050 mg/L	1.00	1. 202 1-03-2	100 100	85-115	0-20		
General Parameters,										
Blank (B1F2166-BL	K1)			Prepared	l: 2021-06-1	8, Analyze	d: 2021-0	6-21		
Nitrogen, Total Kjeldah	I	< 0.050	0.050 mg/L							
Blank (B1F2166-BLI	K2)			Prepared	I: 2021-06-1	8, Analyze	d: 2021-0	6-21		
Nitrogen, Total Kjeldah	•	< 0.050	0.050 mg/L			, ,				
LCS (B1F2166-BS1)			U *	Prenareo	l: 2021-06-1	8 Analyza	d. 2021-0	6-21		
Nitrogen, Total Kjeldah		1.03	0.050 mg/L	1.00	1. 2021-00-1	103	85-115	10-21		
		1.03	0.050 mg/L							
LCS (B1F2166-BS2)				Prepared	1: 2021-06-1	8, Analyze	d: 2021-0	6-21		
Nitrogen, Total Kjeldah	1	1.03	0.050 mg/L	1.00		103	85-115			
	ameters, Batch B1E2012		0.000g	Prepareo	l: 2021-05-2	0, Analyze	d: 2021-0	5-20		
Microbiological Para Blank (B1E2012-BL Coliforms, Total E. coli	ameters, Batch B1E2012 K1)		1 MPN/100 m 1 MPN/100 m	ıL IL		· · · · · · · · · · · · · · · · · · ·				
Microbiological Para Blank (B1E2012-BL Coliforms, Total E. coli Blank (B1E2012-BL	ameters, Batch B1E2012 K1)	2 <1 <1 <1	1 MPN/100 m 1 MPN/100 m	nL nL Preparec	l: 2021-05-2 l: 2021-05-2	· · · · · · · · · · · · · · · · · · ·				
Microbiological Para Blank (B1E2012-BL Coliforms, Total E. coli	ameters, Batch B1E2012 K1)	2 < 1	1 MPN/100 m	nL nL Preparec		· · · · · · · · · · · · · · · · · · ·				
Microbiological Para Blank (B1E2012-BL Coliforms, Total E. coli Blank (B1E2012-BL	ameters, Batch B1E2012 K1) K2)	2 <1 <1 <1	1 MPN/100 m 1 MPN/100 m	nL nL Preparec		0, Analyze	d: 2021-0	95-20		
Microbiological Para Blank (B1E2012-BL Coliforms, Total E. coli Blank (B1E2012-BL E. coli Blank (B1E2012-BL Coliforms, Total	ameters, Batch B1E2012 K1) K2)	2 <1 <1 <1 <1	1 MPN/100 m 1 MPN/100 m 1 MPN/100 m 1 MPN/100 m	IL Preparec IL Preparec IL	l: 2021-05-2	0, Analyze	d: 2021-0	95-20		
Microbiological Para Blank (B1E2012-BL Coliforms, Total E. coli Blank (B1E2012-BL E. coli Blank (B1E2012-BL	ameters, Batch B1E2012 K1) K2)	2 < 1 < 1 < 1 < 1	1 MPN/100 m 1 MPN/100 m 1 MPN/100 m	IL Preparec IL Preparec IL	l: 2021-05-2	0, Analyze	d: 2021-0	95-20		
Microbiological Para Blank (B1E2012-BL Coliforms, Total E. coli Blank (B1E2012-BL E. coli Blank (B1E2012-BL Coliforms, Total	ameters, Batch B1E2012 K1) K2) K3)	2 <1 <1 <1 <1	1 MPN/100 m 1 MPN/100 m 1 MPN/100 m 1 MPN/100 m	IL Preparec IL Preparec IL IL	l: 2021-05-2	0, Analyze 0, Analyze	d: 2021-0 d: 2021-0	15-20 15-20		
Microbiological Para Blank (B1E2012-BL Coliforms, Total E. coli Blank (B1E2012-BL E. coli Blank (B1E2012-BL Coliforms, Total E. coli	ameters, Batch B1E2012 K1) K2) K3)	2 <1 <1 <1 <1	1 MPN/100 m 1 MPN/100 m 1 MPN/100 m 1 MPN/100 m	IL Preparec IL Preparec IL IL Preparec	l: 2021-05-2 l: 2021-05-2	0, Analyze 0, Analyze	d: 2021-0 d: 2021-0	15-20 15-20		
Microbiological Para Blank (B1E2012-BL Coliforms, Total E. coli Blank (B1E2012-BL E. coli Blank (B1E2012-BL Coliforms, Total E. coli Blank (B1E2012-BL E. coli Fotal Metals, Batch	ameters, Batch B1E2012 K1) K2) K3) K4) B1E2552	2 <1 <1 <1 <1 <1 <1 <1 <1 <1	1 MPN/100 m 1 MPN/100 m 1 MPN/100 m 1 MPN/100 m 1 MPN/100 m	IL Preparec IL Preparec IL IL Preparec IL	l: 2021-05-2 l: 2021-05-2	0, Analyze 0, Analyze 0, Analyze	d: 2021-0 d: 2021-0 d: 2021-0	15-20 15-20 15-20		
Microbiological Para Blank (B1E2012-BL Coliforms, Total E. coli Blank (B1E2012-BL E. coli Blank (B1E2012-BL Coliforms, Total E. coli Blank (B1E2012-BL E. coli Fotal Metals, Batch Blank (B1E2552-BL Calcium, total	ameters, Batch B1E2012 K1) K2) K3) K4) B1E2552	2 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1	1 MPN/100 m 1 MPN/100 m 1 MPN/100 m 1 MPN/100 m 1 MPN/100 m 1 MPN/100 m	IL Preparec IL Preparec IL IL Preparec IL	I: 2021-05-2 I: 2021-05-2 I: 2021-05-2	0, Analyze 0, Analyze 0, Analyze	d: 2021-0 d: 2021-0 d: 2021-0	15-20 15-20 15-20		
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CARO Analytical Services FINAL Analytical Testing Report Work Order: 21E2339 Report Date: 2021-06-23 08:49:58

Client Western Water Associates Ltd Attention Morgan Jackson Project 20-046-02VR Project Info [none]

Note: This is not the original data. Please refer to PDF / Hardcopy report.

												Sample Re-Anal		1
LAB ID						21E2339-05	21E2339-01	21E2339-02	21E2339-03	21E2339-04		21E2339-03RE1	21E2339-04RE1	
											Relative			
											Percent			Relative
										Duplicate	Difference			Percent
CLIENT ID						MW-6	MW-8	MW-10	MW-11	(MW11)	(%)	MW-11	Duplicate (MW11)	Difference (S
DATE SAMPLED						2021-05-19	2021-05-19	2021-05-19	2021-05-19	2021-05-19		2021-05-19	2021-05-19	
DATE RECEIVED						2021-05-20	2021-05-20	2021-05-20	2021-05-20	2021-05-20				
MATRIX						Water	Water	Water	Water	Water		Water	Water	
General Method	Analyte	Units	RL	Std (CDWQG)	itd (CSR2D)	W)								
Anions	Chloride	mg/L	1	AO<=250	250	91.6	83.3	90.9	157	150	4.5%	1		1
Anions	Nitrate (as N)	mg/L	0.01	MAC=10	10	1.99	0.945	4.63	3.13	3.04	2.9%			
Anions	Nitrite (as N)	mg/L	0.01	MAC=1	10	< 0.010	<0.010	<0.010	0.01	<0.010	NA			
Calculated Parameters	Hardness, Total (as CaCO3)	mg/L	0.5	None Required	N/A	345	312	343	470	493	4.9%			
Calculated Parameters	Nitrate+Nitrite (as N)	mg/L	0.01	N/A	10	1.99	0.945	4.63	3.14	3.04	3.2%			
Calculated Parameters	Nitrogen, Total	mg/L	0.05	N/A	N/A	2.62	1.24	4.91	3.38	3.5	3.6%			
General Parameters	Ammonia, Total (as N)	mg/L	0.05	None Required	N/A	0.067	<0.050	< 0.050	< 0.050	< 0.050	NA			
General Parameters	Nitrogen, Total Kjeldahl	mg/L	0.05	N/A	N/A	0.625	0.292	0.282	0.241	0.454	88.4%	0.267	0.398	49.1%
General Parameters	Phosphorus, Total (as P)	mg/L	0.005	N/A	N/A	0.251	0.185	0.0497	0.088	0.0861	2.2%			
General Parameters	Phosphorus, Total Dissolved	mg/L	0.005	N/A	N/A	0.0557	0.117	0.0239	0.0264	0.0338	28.0%	0.0273	0.0332	21.6%
General Parameters	pH	pH units	0.1	7.0-10.5	N/A	7.02	6.94	7.31	7.04	7.1	0.9%			
General Parameters	Conductivity (EC)	uS/cm	2	N/A	N/A	1060	905	978	1220	1200	1.6%			
Microbiological Parameters	Coliforms, Total	MPN/100 mL	1	MAC = 0	N/A	5	<1	<1	<1		NA			
Microbiological Parameters	E. coli	MPN/100 mL	1	MAC = 0	N/A	<1	<1	<1	<1		NA			
Total Metals	Calcium, total	mg/L	0.2	None Required	N/A	80.7	89.4	82.5	111	114	2.7%	1		
Total Metals	Magnesium, total	mg/L	0.01	None Required	N/A	34.7	21.4	33.2	46.7	50.3	7.7%	1		
Total Metals	Sodium, total	mg/L	0.1	AO<=200	200	109	83.2	36.7	78.7	83.8	6.5%			
1												_		
CDWQG - Guidelines for Canadian Dri	nking Water Quality (Health Canada, June	2019)									RPD values	>25% flagged.		
CSR2DW - BC CSR Schedule 3.2 Drinki	ng Water													

APPENDIX I

Groundwater Monitoring Data

				Average	
Monitoring Well	Year	Minimum	Maximum	Level*	Level Range
		Level (mbtoc)	. ,	(mbtoc)	(m)
	2007	9.59	10.68	10.18	1.09
	2008	10.52	10.79	10.69	0.27
	2009	10.77	11.40	10.93	0.63
	2010	10.31	11.03	10.76	0.72
	2011	10.33	10.80	10.55	0.47
	2012	9.84	10.78	10.50	0.94
	2013	9.78	10.44	10.11	0.66
Well #1	2014	9.98	10.58	10.33	0.60
Air Cadet	2015	10.01	10.51	10.28	0.50
	2016	10.21	10.5	10.36	0.29
	2017	9.9	10.59	10.32	0.69
	2018	9.65	10.29	10.03	0.64
	2019	9.72	10.62	10.26	0.9
	2020	9.62	10.51	10.22	0.89
	2021	9.24	10.4	9.8	1.16
	2022	10.16	10.85	10.51	0.69
	2007	5.89	6.40	6.10	0.51
	2008	6.11	6.38	6.25	0.27
	2009	5.83	6.54	6.20	0.71
	2010	5.69	6.35	6.04	0.66
	2011	5.84	6.34	6.09	0.50
	2012	5.84	6.54	6.20	0.70
	2013	5.62	6.24	5.91	0.62
Well #2	2014	5.84	6.27	6.08	0.43
Rodeo Grounds	2015	5.69	6.66	6.08	0.97
	2016	5.66	5.97	5.82	0.31
	2017	5.98	6.3	6.16	0.32
	2018	5.81	6.24	5.99	0.43
	2019	6.18	6.96	6.61	0.78
	2020	7.07	7.46	7.27	0.39
	2021	7.48	7.78	7.62	0.3
	2022	7.79	8.10	7.94	0.31
	2007	1.52	2.19	1.81	0.67
	2008	1.50	2.34	1.78	0.84
	2009	1.47	2.05	1.77	0.58
	2010	1.45	1.64	1.54	0.19
	2011	1.31	1.55	1.46	0.24
	2012	1.38	1.54	1.46	0.16
	2013	1.20	1.39	1.27	0.19
Well #3	2014	1.11	1.65	1.37	0.54
91A Street	2015	1.21	1.66	1.41	0.45
	2016	1.13	1.43	1.28	0.30
	2017	1.06	1.38	1.23	0.32
	2018	0.87	1.51	1.2	0.64
	2019	1.24	1.78	1.45	0.54
	2020	1.18	1.72	1.44	0.54
	2021	1.2	2.1	1.7	0.9
	2022	1.51	2.16	1.73	0.65

*Depth indicates the measurement from the top of casing to the water level.

TOWN OF OLIVER GROUNDWATER MONITORING WELL #1 (AIR CADET)

		Anions		Calculate	d Parameters		General Parameters					Total Metals	
Sample	Chloride	Nitrate	Nitrite	Hardness	Nitrate+Nitrite	Ammonia	BOD	Conductivity	Phosphorus	Phosphorus	Calcium	Magnesium	Sodium
Date		(as N)	(as N)	Total	(as N)	Total	5-day	(EC)	Total	Total	Total	Total	Total
				(as CaCO3)		(as N)	Carbonaceous		(as P)	Dissolved			
11-Apr	16.90	9.3	0.011	319	9027.0	<0.050	11.2	698	0.176	0.03	100	16.6	17.6
7-Sep	22.2	8.3	<0.010	320	8.3	< 0.050	<6.1	684	0.109	0.0962	101	16.3	18.6

GROUND WATER MONITORING WELL #2 (RODEO GROUNDS)

		Anions		Calculate	d Parameters		Ge	neral Paramet	ers		Total Metals		
Sample Date	Chloride	Nitrate (as N)	Nitrite (as N)	Hardness Total	Nitrate+Nitrite (as N)	Ammonia Total	BOD 5-day		Phosphorus	Phosphorus	Calcium Total	Magnesium Total	Sodium Total
Dale		(as N)	(as N)	(as CaCO3)	· · ·	(as N)	Total 5-day (EC) Total Total (as N) Carbonaceous (as P) Dissolved				Total	Total	Total
11-Apr	7.14	0.324	<0.010	1970	0.324	0.068	<7.5	581	11.20	0.0068	548	146	20.5
7-Sep	7.51	0.872	<0.010	2980	0.872	<0.050	8.2	539	11.1	0.013	928	161.0	23.6

GROUND WATER MONITORING WELL #3 (MAPLE AVENUE)

		Anions		Calculate	d Parameters		Ge	neral Paramet	ers		Total Metals		
Sample	Chloride	Nitrate	Nitrite	Hardness	Nitrate+Nitrite	Ammonia	BOD	Conductivity	Phosphorus	Phosphorus	Calcium	Magnesium	Sodium
Date		(as N)	(as N)	Total	(as N)	Total	5-day	(EC)	Total	Total	Total	Total	Total
				(as CaCO3)		(as N)	Carbonaceous		(as P)	Dissolved			
11-Apr	8.48	0.01	<0.010	559	<0.0200	0.191	<7.5	778	6.5	0.0064	139	51.3	15.7
7-Sep	9.04	0.089	<0.010	1260	0.0886	0.141	<6.1	806	5.67	0.013	353	91.9	19

GROUND WATER MONITORING WELL #4 (SAND PIT)

		Anions		Calculate	d Parameters		General Parameters					Total Metals	
Sample Date	Chloride	Nitrate (as N)	Nitrite (as N)	Hardness Total	Nitrate+Nitrite (as N)	Ammonia Total	BOD 5-day	Conductivity (EC)	Phosphorus Total	Phosphorus Total	Calcium Total	Magnesium Total	Sodium Total
		. ,	. ,	(as CaCO3)	. ,	(as N)	Carbonaceous		(as P)	Dissolved			
11-Apr	119	3.51	<0.010	991	3.51	<0.050	<7.5	1820	1.27	0.119	250	88.8	81.2
7-Sep	121	1.35	<0.010	1610	1.35	<0.050	<6.1	1710	23.7	0.101	465	110	92

*** Test results high due to draining effluent water two weeks before testing into the infiltration to lower Topping Lake

GROUND WATER MONITORING WELL #5 (Choke Cherry)

		Anions		Calculate	d Parameters	General Parameters						Total Metals		
Sample	Chloride	Nitrate	Nitrite	Hardness	Nitrate+Nitrite	Ammonia	BOD	Conductivity	Phosphorus	Phosphorus	Calcium	Magnesium	Sodium	
Date		(as N)	(as N)	Total	(as N)	Total	5-day	(EC)	Total	Total	Total	Total	Total	
				(as CaCO3)		(as N)	Carbonaceous		(as P)	Dissolved				
11-Apr	13.5	0.796	<0.010	292	0.796	<0.050	<7.5	676	0.446	0.0059	84.7	19.5	9.87	
7-Sep	16.1	1.17	<0.010	442	1.17	<0.050	<6.1	660	2.01	0.0121	134	26.1	15.9	

Fairview Gold Course

		Anions		Calculate	d Parameters		Ge	neral Paramet	ers		Total Metals		
Sample	Chloride Nitrate Nitrite		Hardness	Nitrate+Nitrite	Ammonia	BOD	Conductivity Phosphorus		Phosphorus	Calcium	Magnesium	Sodium	
Date		(as N)	(as N)	Total	(as N)	Total	5-day	(EC)	Total	Total	Total	Total	Total
				(as CaCO3)		(as N)	Carbonaceous		(as P)	Dissolved			
11-Apr	95.2	2.76	<0.010	369	2.76	<0.050	<7.5	1180	0.113	0.103	77.7	42.4	94.5
7-Sep	95.7	2.80	0.01	395	2.81	<0.050	<6.1	1150	0.117	0.1	90.9	40.8	102

Public Works Yard

		Anions		Calculate	d Parameters	General Parameters						Total Metals		
Sample	Chloride	Nitrate	Nitrite	Hardness	Nitrate+Nitrite	Ammonia	BOD	Conductivity	Phosphorus	Phosphorus	Calcium	Magnesium	Sodium	
Date		(as N)	(as N)	Total	(as N)	Total	5-day	(EC)	Total	Total	Total	Total	Total	
				(as CaCO3)		(as N)	Carbonaceous		(as P)	Dissolved				
11-Apr	48.7	2.58	<0.010	278	2.58	<0.050	11.1	770	0.137	0.118	74.4	22.3	30.4	
7-Sep	87.8	1.34	0.132	353	1.47	0.737	<6.1	941	0.484	0.438	98.7	25.7	48.2	

Linear Park

			Anions		Calculate	d Parameters	General Parameters						Total Metals		
San	nple	Chloride	Nitrate	Nitrite	Hardness	Nitrate+Nitrite	Ammonia	BOD	Conductivity	Phosphorus	Phosphorus	Calcium	Magnesium	Sodium	
Da	ate		(as N)	(as N)	Total	(as N)	Total	5-day	(EC)	Total	Total	Total	Total	Total	
					(as CaCO3)		(as N)	Carbonaceous		(as P)	Dissolved				
1	1-Apr	37.9	3.18	<0.010	312	3.18	<0.050	<7.5	729	0.127	0.0271	76	29.6	22.4	
	7-Sep	85.1	3.90	0.046	674	3.94	<0.050	<6.1	713	8.56	0.0327	191	47.9	62.8	

End of Road 5

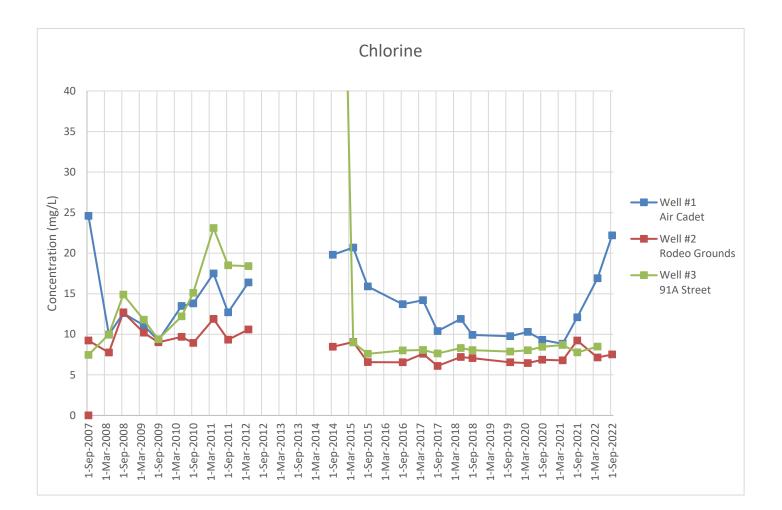
		Anions		Calculate	d Parameters		Ge	neral Paramet	ers		Total Metals		
Sample	Chloride	Nitrate	Nitrite	Hardness	Nitrate+Nitrite	Ammonia	BOD	Conductivity	Phosphorus	Phosphorus	Calcium	Magnesium	Sodium
Date		(as N)	(as N)	Total	(as N)	Total	5-day	(EC)	Total	Total	Total	Total	Total
				(as CaCO3)		(as N)	Carbonaceous		(as P)	Dissolved			
11-Apr	114	4.13	<0.010	470	4.13	<0.050	9.5	1090	0.008	0.0053	95.9	55.9	17.8
7-Sep	115	4.30	0.044	498	4.34	<0.050	<6.1	1080	0.0133	0.0097	108	55.1	18.3

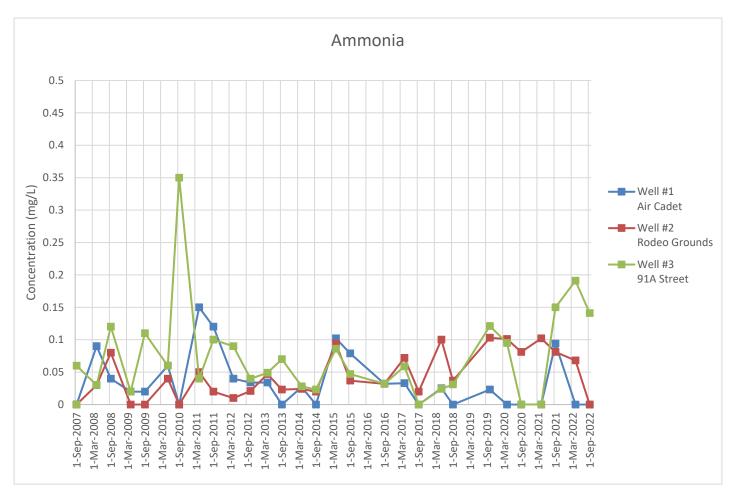
Monitoring Well	Sample Date	Chloride	Ammonia	Nitrate + Nitrite	Total Hardness	Sodium
J	19-Sep-2007	24.6	< 0.02	7.71	535	13.9
	9-Apr-2008	9.97	0.09	2.84	773	24.1
	11-Sep-2008	12.6	0.04	1.3	817	21.7
	7-Apr-2009	11.1	0.02	0.7	1220	27.3
	18-Sep-2009	9.23	0.02	2.3	437	17.7
	19-May-2010 7-Sep-2010	13.5 13.8	0.06 < 0.02	12.7 12	383	22.1
	28-Apr-2011	17.5	0.15	12.1	217	9.33
	28-Sep-2011	12.7	0.13	7.87	400	9.33 18.4
	24-Apr-2012	16.4	0.04	7.59	464	20.0
	16-Oct-2012		0.034	9.7	481	19.8
	9-Apr-2013		0.034	10.1	384	18.5
	9-Sep-2013		< 0.020	20.2	383	17
Well #1	16-Apr-2014	40.0	0.027	21.6	542	18.1
Air Cadet	4-Sep-2014 14-Apr-2015	<u>19.8</u> 20.7	< 0.020 0.102	23.9 24.4	402 485	<u> </u>
	16-Sep-2015	15.9	0.079	20.5	590	23.5
		1010		2010		2010
	13-Sep-2016	13.7	0.032	15	386	19.1
	10-Apr-2017	14.2	0.033	12	388	19.5
	11-Sep-2017	10.4	<0.020	6.97	392	18
	14-May-2018	11.9	0.025	6.75	363	19.1
	10-Sep-2018 28-Oct-2019	<u>9.92</u> 9.77	<0.020 0.023	7.97	344 388	<u> </u>
	6-Apr-2020	10.3	<0.023	13	331	19.6
	1-Sep-2020	9.31	<0.050	11.1	378	19.4
	22-Apr-2021	8.83	<0.050	11	316	17.1
	13-Sep-2021	12.1	0.094	9.67	303	17.6
	11-Apr-2022	16.9	< 0.050	9027	319	17.6
	7-Sep-2022	22.2	<0.050	8.3	320	18.6
	19-Sep-2007	9.24	< 0.02	0.25	2330	22.7
	9-Apr-2008 11-Sep-2008	7.76 12.7	0.03 0.08	0.5 1.14	1690 890	23.7 21.7
	7-Apr-2009	10.2	< 0.02	1.14	346	15.2
	18-Sep-2009	9.01	< 0.02	0.36	677	19.1
	19-May-2010	9.69	0.04	0.08		
	7-Sep-2010	8.93	< 0.02	0.26	686	22.3
	28-Apr-2011	11.9	0.05	0.05	531	9.13
	28-Sep-2011	9.33	0.02	2.18	491	16.1
	24-Apr-2012	10.6	0.01	0.749	572	17.4
	16-Oct-2012		0.021	0.263	661	17.8
	9-Apr-2013		0.047	0.121	384	18.4
	9-Sep-2013 16-Apr-2014		0.023	0.115	889 392	<u>18</u> 15.9
Well #2	4-Sep-2014	8.47	0.02	0.584	370	15.9
Rodeo Grounds	14-Apr-2015	9.05	0.094	0.865	494	18.5
	16-Sep-2015	6.56	0.037	0.3	1120	31.6
	-	-	-	-	-	-
	13-Sep-2016	6.54	0.032	0.628	1110	19.2
	10-Apr-2017	7.6 6.1	0.072 0.02	0.343 0.124	914 959	20.4 17.1
	11-Sep-2017 14-May-2018	7.2	0.02	0.124	2550	20.3
	10-Sep-2018	7.07	0.037	0.138	2090	18.9
	28-Oct-2019	6.55	0.103	0.385	2440	20.8
	6-Apr-2020	6.44	0.101	0.212	394	17.2
	1-Sep-2020	6.86	0.081	0.173	1540	18.9
	22-Apr-2021	6.78	0.102	0.312	1410	17.5
	21-Sep-2021 11-Apr-2022	<u>9.24</u> 7.14	0.081 0.068	0.045	<u> </u>	20.4 20.5
	7-Sep-2022	7.14 7.51	<0.050	0.324	2980	20.5 23.6
	19-Sep-2022	7.46	0.06	0.05	7340*	15.1
	9-Apr-2008	10	0.03	0.05	972	27.5
	11-Sep-2008	14.9	0.12	0.04	5010	38.4
	7-Apr-2009	11.8	0.02	0.026	1270	31.6
	18-Sep-2009	9.39	0.11	< 0.02	1070	24.6
	19-May-2010	12.2	0.06	< 0.02		
	7-Sep-2010	15.1	0.35	0.35	2300	37.7
	28-Apr-2011	23.1	0.04	0.44	633	15.3
	28-Sep-2011	18.5	0.1	0.32	1160	36.8
	24-Apr-2012	18.4	0.09	0.270	1470	36.9
	16-Oct-2012		0.04	0.033	924	31.6
	9-Apr-2013		0.049	0.074	834	23.9
	9-Sep-2013		0.07	0.101	1430	24.6
Well #3	16-Apr-2014	125	0.028 0.023	0.058 0.032	399 438	16.9 21.8
91A Street	4-Sep-2014 14-Apr-2015	8.99	0.023	0.032	438 631	18.9
JIA JUEEL	16-Sep-2015	8.99 7.59	0.086	0.035	496	18.5
	10-340-2013	/ : \ M				

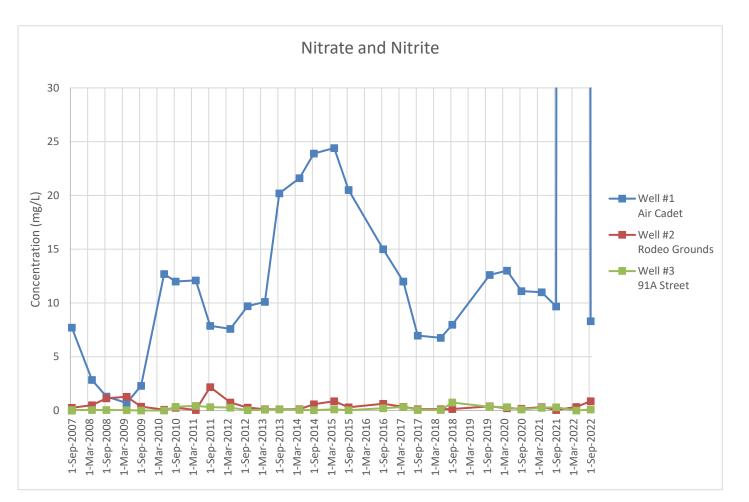
TABLE 2-2: HISTORICAL SUMMARY OF WATER QUALITY ANALYSIS FOR THE AIRPORT MONITORING WELLS

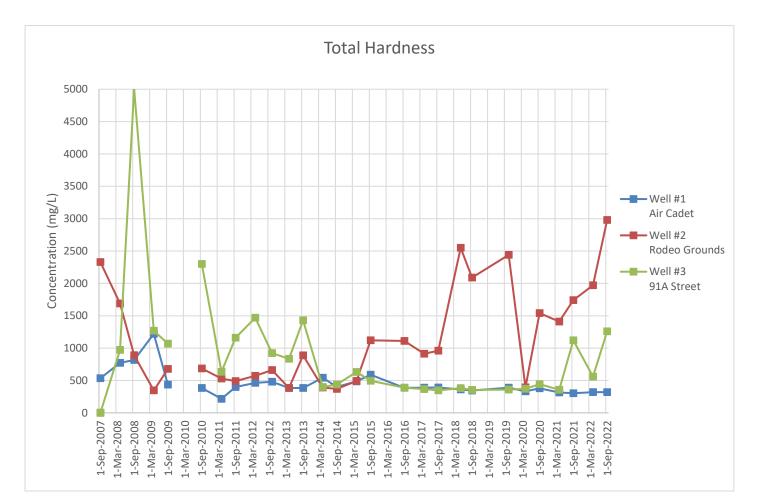
13-Sep-2016	8.01	0.032	0.214	389	17.2
10-Apr-2017	8.07	0.059	0.334	366	16.7
11-Sep-2017	7.64	<0.020	0.042	346	15.2
14-May-2018	8.31	0.024	0.0507	381	15.4
10-Sep-2018	8.05	0.031	0.739	355	14.4
28-Oct-2019	7.87	0.121	0.349	360	16
6-Apr-2020	8.03	0.095	0.315	371	16.3
1-Sep-2020	8.47	<0.050	0.0929	443	16.5
22-Apr-2021	8.68	<0.050	0.25	356	15.2
21-Sep-2021	7.77	0.15	0.307	1120	15.1
11-Apr-2022	8.48	0.191	<0.0200	559	15.7
7-Sep-2022	9.04	0.141	0.0886	1260	19

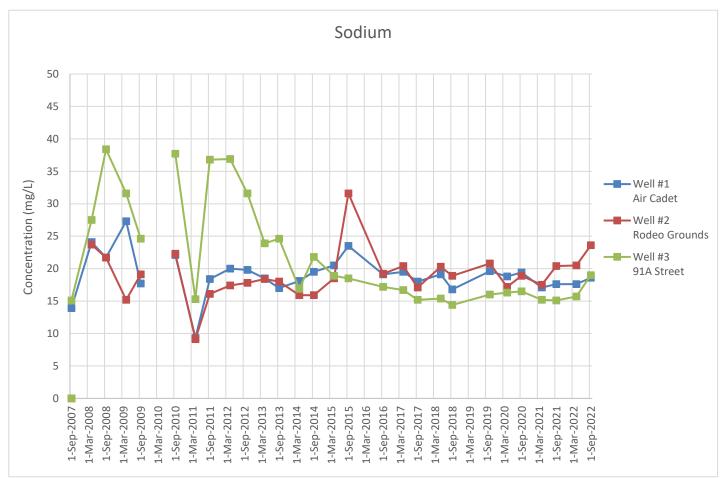
* Suspected error.







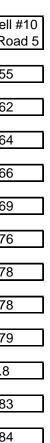




TOWN OF OLIVER

GROUND WATER MONITORING WELL READINGS (Note: The value recorded indicates the measurement from the top of casing to the water level expressed in meters.)

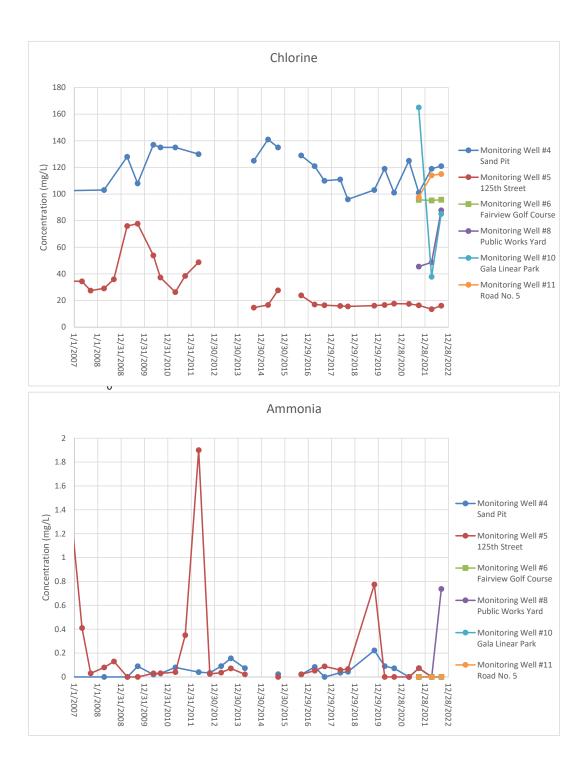
 _					T () M (//0	T (1) (1) (1) (1)			T () A (H (H //	T	T () M //0	
	_			Maple Ave		Test Well #4	Test Well #5	Test Well #6	Test Well #7	Test Well #8	Test Well #9	
Month	Day	(Well #1)	(Well #2)	(Well #3)	(Corner 350th/T.L.)	(Sand Pit)		(Golf Course)	(Road #5 West)	Cemetery	Linear Park	End of Roa
	17	10.56	7.79	1.61	fanad off	0.70	9.79	12.01	2 000	21.44 (dm)	25.0	04 E E
January	17	10.50	1.19	1.01	fenced off	9.72	9.79	12.91	3.000	21.44 (dry)	25.8	24.55
February	18	10.67	7.83 (dry)	1.51	fenced off	9.15	9.95	13.08	3.01	21.23 (dry)	25.7	24.62
	<u>.</u>	40		4.50		0.00			0.07	<u></u>	<u> </u>	
March	21	10.77	7.79	1.53	fenced off	8.66	10.11	13.21	3.35	21.05	25.74	24.64
April	11	10.74	7.81	1.6	fenced off	8.65	10.13	13.13	3	21.06 (dry)	25.69	24.66
							-	-				
Мау	30	10.85	7.89	1.64	fenced off	8.84	9.84	13.4	2.63	21.05 (dry)	26	24.69
June	27	10.8	7.9	1.6	fenced off	9.1	7.98	13.29	2	21.3	26.12	24.76
July	28	10.55	7.95	1.69	fenced off	9.84	7.61	13.24	2.19	21.06	26.23	24.78
August	22	10.22	7.99	1.85	fenced off	10.49	7.78	13.18	2.58	21.06	26.46	24.78
August	22	10.22	1.99	1.00	lenced on	10.49	1.10	13.10	2.30	21.00	20.40	24.70
September	7	10.16	8.01	1.95	fenced off	10.62	7.96	13.04	2.81	21.06	26.59	24.79
	47	40.40	0.07	0.40	for a set off	40.00	0.5	40.07	0.00	04.00	00.45	04.0
October	17	10.18	8.07	2.16	fenced off	10.38	8.5	12.87	2.96	21.09	26.45	24.8
November	14	10.19	8.08	1.82	fenced off	9.03	8.82	12.99	2.94	21.1	26.28	24.83
					· · · · · · · · · · · · · · · · · · ·				· · · · · · · · · · · · · · · · · · ·			
December	6	10.4	8.1	1.76	fenced off	9.69	9.02	13.1	2.99	21.1	26.14	24.84

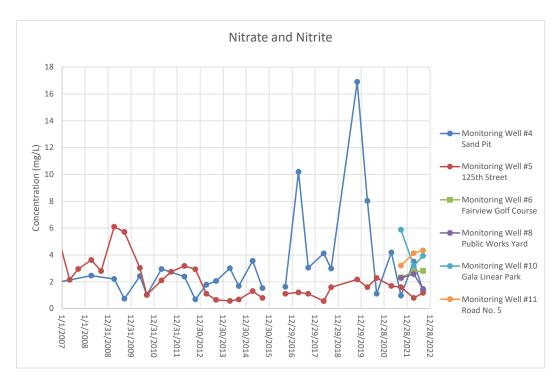


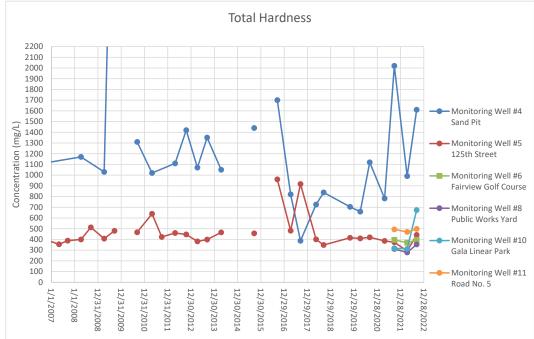
Monitoring Well	Sample Date	Chloride	Ammonia	Nitrate + Nitrite	Total Hardness	Sodium
U	22-Apr-03	72	0.05	0.52	1060	55.8
	30-Sep-03	94	0.08	0.39	1370	80.3
	20-Apr-04	111	0.04	0.97	1130	73.1
	4-Sep-04	123	0.02	0.35	3280	108
	12-Apr-05	102	<0.01	1.44	1060	85.1
	9-Apr-08	103	< 0.02	2.46	1170	104
	7-Apr-09	128	< 0.02	2.21	1030	103
	16-Sep-09 19-May-10	108 137	0.09	0.74 2.43	4980	125
	7-Sep-10	137	0.02	1.02	1310	128
	28-Apr-11	135	0.03	2.95	1020	128
	24-Apr-12	130	0.08	2.39	1110	108
	16-Oct-12	100	0.034	0.691	1420	119
	9-Apr-13		0.091	1.78	1070	118
	9-Sep-13		0.156	2.06	1350	146
	16-Apr-14		0.130	3.02	1050	140
Monitoring Well #4	4-Sep-14	125	0.075	1.68	1050	127
Sand Pit	14-Apr-15	141		3.56		127
	16-Sep-15	135	0.023	3.56 1.53	1440	120
	10-Sep-15	100	0.023	1.00	1440	127
	13-Sep-16	129	0.021	1.63	1700	19.2
	10-Apr-17	129	0.021	10.2	820	108
	11-Sep-17	121	<0.084	3.05	387	11.5
	14-May-18	111	0.020	4.12	725	100
	10-Sep-18	96	0.035	2.99	838	87.1
	28-Oct-19	103	0.043	16.9	704	93
	6-Apr-20	119	0.091	8.03	659	93
	1-Sep-20	101	0.072	1.11	1120	86.9
	22-Apr-21	125	< 0.072	4.19	782	81.7
		125	0.073		2020	97.1
	21-Sep-21 11-Apr-22	101	<0.073	0.967 3.51	991	
	7-Sep-22	121	<0.050	1.35	1610	81.2 92
	22-Apr-03	36.1	< 0.050	3.9	367	29.5
	30-Sep-03	29.2	0.02	3.9	391	29
	20-Apr-04	30.4	0.02	3.6	395	23.8
	4-Sep-04	22.3	0.02	6.52	447	32.4
	12-Apr-05	34.2	< 0.01	5.81	409	25.5
	7-Sep-05	46.5	<0.01	12.4	537	25.7
	15-Jun-06	34.8	<0.01	8.62	543	27
	21-Sep-06	34.6	1.65	6.05	399	28
	1-May-07	34.4	0.41	2.15	355	26
	13-Sep-07	27.5	0.03	2.95	388	30.2
	9-Apr-08	29.1	0.08	3.62	399	35.9
	11-Sep-08	36	0.13	2.8	512	33.7
	7-Apr-09	76	< 0.02	6.1	407	35.1
	16-Sep-09	77.7	< 0.02	5.72	480	21.6
	19-May-10	53.9	0.03	3.03	467	20.2
	7-Sep-10 28-Apr-11	37.3 26.3	0.03	1.03 2.1	467 639	29.2 41
	28-Sep-11	26.3 38.5	0.04	2.1	423	41
	26-Sep-11 24-Apr-12	48.8	1.9	3.19	423	22.4
Monitoring Well #5	16-Oct-12	-10.0	0.025	2.94	446	19.3
125th Street	9-Apr-13		0.025	1.11	381	15.9
	9-Sep-13		0.030	0.652	398	12.4
	16-Apr-14		0.071	0.577	465	13.1
	4-Sep-14	14.7	0.022	0.683	400	14
	14-Apr-15	14.7		1.31		14.7
	16-Sep-15	27.7	< 0.020	0.794	456	31.6
	10 Ocp-13	-	-	-	-	-
	13-Sep-16	23.9	0.022	1.11	960	20.4
	13-3eb-10	20.9	0.022	1.11	300	20.4

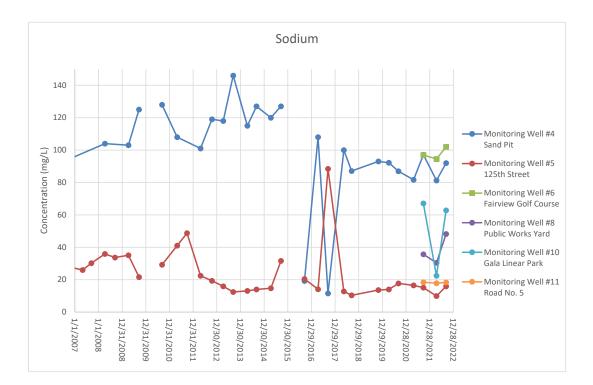
TABLE 2-4: HISTORICAL SUMMARY OF WATER QUALITY ANALYSIS FOR FAIRVIEW MONITORING WELLS

	10-Apr-17	17	0.052	1.21	481	14.1
	11-Sep-17	16.5	0.089	1.11	917	88.4
	14-May-18	16	0.058	0.569	400	12.8
	10-Sep-18	15.6	0.066	1.59	348	10.3
	28-Oct-19	16.1	0.774	2.18	415	13.6
	6-Apr-20	16.7	<0.050	1.6	409	14
	1-Sep-20	17.7	<0.050	2.28	419	17.7
	22-Apr-21	17.5	<0.050	1.69	386	16.5
	21-Sep-21	16.4	0.073	1.6	374	15.1
	11-Apr-22	13.5	<0.050	0.796	292	9.87
	7-Sep-22	16.1	<0.050	1.17	442	15.9
Monitoring Well #6	21-Sep-21	95.6	<0.050	2.33	396	96.9
Fairview Golf Course	11-Apr-22	95.2	<0.050	2.76	369	94.5
	7-Sep-22	95.7	<0.050	2.81	395	102
Monitoring Well #8	21-Sep-21	45.5	<0.050	2.28	311	35.7
Public Works Yard	11-Apr-22	48.7	<0.050	2.58	278	30.4
Tuble Works Tard	7-Sep-22	87.8	0.737	1.47	353	48.2
Monitoring Well #10	21-Sep-21	165	<0.050	5.89	317	67.1
Gala Linear Park	11-Apr-22	37.9	<0.050	3.18	312	22.4
	7-Sep-22	85.1	<0.050	3.94	674	62.8
Monitoring Well #11	21-Sep-21	97.7	<0.050	3.21	493	18.4
Road No. 5	11-Apr-22	114	<0.050	4.13	470	17.8
11000 110. 0	7-Sep-22	115	<0.050	4.34	498	18.3











REPORTED TO Oliver, Town of PROJECT Ground Water Monite	oring		WORK ORDER REPORTED	22D1701 2022-04-2	2 16:08
Analyte	Result	RL	Units	Analyzed	Qualifie
MW1 - Air Cadet (22D1701-01) Matrix:	Water Sampled <mark>: 2022-04-11 1</mark>	4:00			FILT, PRES
Anions					
Chloride	16.9	0.10	mg/L	2022-04-19	
Nitrate (as N)	9.26	0.010	mg/L	2022-04-19	HT1
Nitrite (as N)	0.011	0.010	mg/L	2022-04-19	HT1
Calculated Parameters					
Hardness, Total (as CaCO3)	319	0.500	mg/L	N/A	
Nitrate+Nitrite (as N)	9.27	0.0200		N/A	
General Parameters					
Ammonia, Total (as N)	< 0.050	0.050	ma/L	2022-04-20	
BOD, 5-day Carbonaceous	11.2		mg/L	2022-04-19	
Conductivity (EC)	698	177449A	µS/cm	2022-04-21	
Phosphorus, Total (as P)	0.176	0.0050	and the second sec	2022-04-20	
Phosphorus, Total Dissolved	0.0300	0.0050		2022-04-20	
Total Metals	100000000				
Calcium, total	100	0.20	mg/L	2022-04-20	
Magnesium, total	16.6	0.010		2022-04-20	
Sodium, total	17.6	Note that the second	mg/L	2022-04-20	
MW2 - Maple Avenue (22D1701-02) M	atrix: Water Sampled: 2022-04	4-11 14:55			FILT, PRES
Chloride	8.48	0.10	mg/L	2022-04-19	
Nitrate (as N)	0.010		mg/L	2022-04-19	HT1
Nitrite (as N)	< 0.010		mg/L	2022-04-19	HT1
Calculated Parameters			mg/L	N/A	
	559	0.500			
Calculated Parameters Hardness, Total (as CaCO3) Nitrate+Nitrite (as N)	559 < 0.0200			N/A	
Hardness, Total (as CaCO3)	and the second	0.500		Age in Male and the second	
Hardness, Total (as CaCO3) Nitrate+Nitrite (as N) General Parameters	< 0.0200	0.0200	mg/L	Age in Male and the second	
Hardness, Total (as CaCO3) Nitrate+Nitrite (as N) General Parameters Ammonia, Total (as N)	and the second	0.0200		N/A	
Hardness, Total (as CaCO3) Nitrate+Nitrite (as N) General Parameters	< 0.0200	0,0200 0.050 2.0	mg/L mg/L mg/L	N/A 2022-04-20	
Hardness, Total (as CaCO3) Nitrate+Nitrite (as N) General Parameters Ammonia, Total (as N) BOD, 5-day Carbonaceous	< 0.0200 0.191 < 7.5	0,0200 0.050 2.0	mg/L mg/L μS/cm	N/A 2022-04-20 2022-04-19	
Hardness, Total (as CaCO3) Nitrate+Nitrite (as N) General Parameters Ammonia, Total (as N) BOD, 5-day Carbonaceous Conductivity (EC)	< 0.0200 0.191 < 7.5 778	0.0200 0.050 2.0 2.0	mg/L mg/L mg/L µS/cm mg/L	N/A 2022-04-20 2022-04-19 2022-04-21	
Hardness, Total (as CaCO3) Nitrate+Nitrite (as N) General Parameters Ammonia, Total (as N) BOD, 5-day Carbonaceous Conductivity (EC) Phosphorus, Total (as P)	< 0.0200 0.191 < 7.5 778 6.50	0.0200 0.050 2.0 2.0 0.0050	mg/L mg/L mg/L µS/cm mg/L	N/A 2022-04-20 2022-04-19 2022-04-21 2022-04-20	
Hardness, Total (as CaCO3) Nitrate+Nitrite (as N) General Parameters Ammonia, Total (as N) BOD, 5-day Carbonaceous Conductivity (EC) Phosphorus, Total (as P) Phosphorus, Total Dissolved Total Metals	< 0.0200 0.191 < 7.5 778 6.50 0.0064	0,0200 0.050 2.0 2.0 0.0050 0.0050	mg/L mg/L μS/cm mg/L mg/L	N/A 2022-04-20 2022-04-19 2022-04-21 2022-04-20 2022-04-20	
Hardness, Total (as CaCO3) Nitrate+Nitrite (as N) General Parameters Ammonia, Total (as N) BOD, 5-day Carbonaceous Conductivity (EC) Phosphorus, Total (as P) Phosphorus, Total Dissolved	< 0.0200 0.191 < 7.5 778 6.50	0,0200 0.050 2.0 2.0 0.0050 0.0050 0.0050	mg/L mg/L mg/L µS/cm mg/L	N/A 2022-04-20 2022-04-19 2022-04-21 2022-04-20	



PROJECT	Oliver, Town of Ground Water Monitor	ring		WORK ORDER REPORTED	22D1701 2022-04-2:	2 16:08
Analyte		Result	RL	Units	Analyzed	Qualifie
MW3 - Rodeo Gro	ounds (22D1701-03) M	atrix: Water Sampled: 2022-	04-11 14:40		8	FILT, PRES
Anions						
Chloride		7.14	0.10	mg/L	2022-04-19	
Nitrate (as N)		0.324	0.010	mg/L	2022-04-19	HT1
Nitrite (as N)		< 0.010	0.010	mg/L	2022-04-19	HT1
Calculated Parame	eters					
Hardness, Total (a	as CaCO3)	1970	0.500	mg/L	N/A	
Nitrate+Nitrite (as		0.324	0.0200	mg/L	N/A	
General Parameter	'S					
Ammonia, Total (a	as N)	0.068	0.050	mg/L	2022-04-20	
BOD, 5-day Carbo		< 7.5		mg/L	2022-04-19	
Conductivity (EC)		581		µS/cm	2022-04-21	
Phosphorus, Total		11.2	0.0050	mg/L	2022-04-20	
Phosphorus, Total		0.0068	0.0050	mg/L	2022-04-20	
Total Metals						
Calcium, total		548	0.20	mg/L	2022-04-20	
Magnesium, total		146	0.010		2022-04-20	
Sodium, total	1	20.5		mg/L	2022-04-20	
MMA Test Mall	#4 (Sandpit) (22D1701-	04) Matrix: Water Sampled:	2022-04-11 13:00			FILT,
WWW4 - Test Wells						
Anions		440	0.10	mall	2022 04 10	PRES
Anions Chloride		119		mg/L	2022-04-19	PRES
Anions Chloride Nitrate (as N)		3.51	0.010	mg/L	2022-04-19	PRES HT1
Anions Chloride Nitrate (as N) Nitrite (as N)	afore			mg/L		PRES
Anions Chloride Nitrate (as N) Nitrite (as N) Calculated Parame		3.51 < 0.010	0.010 0.010	mg/L mg/L	2022-04-19 2022-04-19	PRES HT1
Anions Chloride Nitrate (as N) Nitrite (as N) Calculated Parame Hardness, Total (a	as CaCO3)	3.51 < 0.010 991	0.010 0.010 0.500	mg/L mg/L mg/L	2022-04-19 2022-04-19 N/A	PRES HT1
Anions Chloride Nitrate (as N) Nitrite (as N) Calculated Parame Hardness, Total (a Nitrate+Nitrite (as	as CaCO3) s N)	3.51 < 0.010	0.010 0.010	mg/L mg/L mg/L	2022-04-19 2022-04-19	PRES HT1
Anions Chloride Nitrate (as N) Nitrite (as N) Calculated Parame Hardness, Total (a Nitrate+Nitrite (as General Parameter	as CaCO3) s N) <i>rs</i>	3.51 < 0.010 991 3.51	0.010 0.010 0.500 0.0200	mg/L mg/L mg/L mg/L	2022-04-19 2022-04-19 N/A N/A	PRES HT1
Anions Chloride Nitrate (as N) Nitrite (as N) Calculated Paramete Hardness, Total (a Nitrate+Nitrite (as General Paramete Ammonia, Total (a	as CaCO3) s N) <i>rs</i> as N)	3.51 < 0.010 991 3.51 < 0.050	0.010 0.010 0.500 0.0200 0.050	mg/L mg/L mg/L mg/L	2022-04-19 2022-04-19 N/A N/A 2022-04-20	PRES HT1
Anions Chloride Nitrate (as N) Nitrite (as N) Calculated Parame Hardness, Total (a Nitrate+Nitrite (as General Parameter Ammonia, Total (a BOD, 5-day Carb	as CaCO3) s N) <i>rs</i> as N) ionaceous	3.51 < 0.010 991 3.51 < 0.050 < 7.5	0.010 0.010 0.500 0.0200 0.050 2.0	mg/L mg/L mg/L mg/L mg/L	2022-04-19 2022-04-19 N/A N/A 2022-04-20 2022-04-19	PRES HT1
Anions Chloride Nitrate (as N) Nitrite (as N) Calculated Parame Hardness, Total (a Nitrate+Nitrite (as General Parameter Ammonia, Total (a BOD, 5-day Carb Conductivity (EC)	as CaCO3) 3 N) rs as N) ionaceous)	3.51 < 0.010 991 3.51 < 0.050 < 7.5 1820	0.010 0.010 0.500 0.0200 0.050 2.0 2.0	mg/L mg/L mg/L mg/L mg/L mg/L μS/cm	2022-04-19 2022-04-19 N/A N/A 2022-04-20 2022-04-19 2022-04-21	PRES HT1
Anions Chloride Nitrate (as N) Nitrite (as N) Calculated Parame Hardness, Total (a Nitrate+Nitrite (as General Parameter Ammonia, Total (a BOD, 5-day Carb Conductivity (EC) Phosphorus, Tota	as CaCO3) s N) rs as N) oonaceous) al (as P)	3.51 < 0.010 991 3.51 < 0.050 < 7.5 1820 1.27	0.010 0.010 0.500 0.0200 0.050 2.0 2.0 2.0 0.0050	mg/L mg/L mg/L mg/L mg/L μS/cm mg/L	2022-04-19 2022-04-19 N/A N/A 2022-04-20 2022-04-19 2022-04-21 2022-04-20	PRES HT1
Anions Chloride Nitrate (as N) Nitrite (as N) Calculated Paramete Hardness, Total (a Nitrate+Nitrite (as General Parameter Ammonia, Total (a BOD, 5-day Carb Conductivity (EC) Phosphorus, Tota Phosphorus, Tota	as CaCO3) s N) rs as N) oonaceous) al (as P)	3.51 < 0.010 991 3.51 < 0.050 < 7.5 1820	0.010 0.010 0.500 0.0200 0.050 2.0 2.0	mg/L mg/L mg/L mg/L mg/L μS/cm mg/L	2022-04-19 2022-04-19 N/A N/A 2022-04-20 2022-04-19 2022-04-21	PRES HT1
Anions Chloride Nitrate (as N) Nitrite (as N) Calculated Parame Hardness, Total (a Nitrate+Nitrite (as General Parameter Ammonia, Total (a BOD, 5-day Carb Conductivity (EC) Phosphorus, Tota Phosphorus, Tota Total Metals	as CaCO3) s N) rs as N) oonaceous) al (as P)	3.51 <0.010 991 3.51 <0.050 <7.5 1820 1.27 0.119	0.010 0.010 0.500 0.0200 0.050 2.0 0.0050 0.0050	mg/L mg/L mg/L mg/L mg/L μS/cm mg/L mg/L mg/L	2022-04-19 2022-04-19 N/A N/A 2022-04-20 2022-04-21 2022-04-21 2022-04-20 2022-04-20	PRES HT1
Anions Chloride Nitrate (as N) Nitrite (as N) Calculated Paramete Hardness, Total (a Nitrate+Nitrite (as General Parameter Ammonia, Total (a BOD, 5-day Carb Conductivity (EC) Phosphorus, Tota Phosphorus, Tota	as CaCO3) s N) rs as N) oonaceous) al (as P) al Dissolved	3.51 < 0.010 991 3.51 < 0.050 < 7.5 1820 1.27	0.010 0.010 0.500 0.0200 0.050 2.0 2.0 0.0050 0.0050 0.0050	mg/L mg/L mg/L mg/L mg/L μS/cm mg/L	2022-04-19 2022-04-19 N/A N/A 2022-04-20 2022-04-19 2022-04-21 2022-04-20	PRES HT1



REPORTED TO PROJECT	Oliver, Town of Ground Water Monitoring	1		WORK ORDER REPORTED	22D1701 2022-04-2:	2 16:08
Analyte		Result	RL	Units	Analyzed	Qualifie
MW5 - Test Well (#5 (Chokecherry) (22D170	1-05) Matrix: Water Sam	pled: 2022-04-11 11:2	20		FILT, PRES
Anions						
Chloride		13.5	0.10	mg/L	2022-04-19	
Nitrate (as N)		0.796	0.010	mg/L	2022-04-19	HT1
Nitrite (as N)		< 0.010	0.010	mg/L	2022-04-19	HT1
Calculated Parame	eters					
Hardness, Total (a	as CaCO3)	292	0.500	mg/L	N/A	
Nitrate+Nitrite (as		0.796	0.0200		N/A	
General Paramete	rs					
Ammonia, Total (a	as N)	< 0.050	0.050	mg/L	2022-04-20	
BOD, 5-day Carb		< 7.5	2.0	mg/L	2022-04-19	
Conductivity (EC)		676	2.0	µS/cm	2022-04-21	
Phosphorus, Tota	X	0.446	0.0050	mg/L	2022-04-20	
Phosphorus, Tota		0.0059	0.0050		2022-04-20	
Total Metals						
Calcium, total		84.7	0.20	mg/L	2022-04-20	
Magnesium, total	1	19.5	0.010		2022-04-20	
Sodium, total		9.87	and the second se	mg/L	2022-04-20	
MW6 - Fairview	Gold Course (22D1701-06)) Matrix: Water Sampled:	2022-04-11 12:00			FILT, PRES
Anions		8				
Chloride		95.2	0.10	mg/L	2022-04-19	
Nitrate (as N)		2.76	0.010	mg/L	2022-04-19	HT1
Nitrite (as N)		< 0.010	0.010	mg/L	2022-04-19	HT1
Calculated Param	eters					
Hardness, Total ((as CaCO3)	369	0.500	mg/L	N/A	
Nitrate+Nitrite (a		2,76	0.0200	and the second se	N/A	
General Paramete	ers			0		
Ammonia, Total ((as N)	< 0.050	0.050	mg/L	2022-04-20	
BOD, 5-day Carl		< 7.5		mg/L	2022-04-19	
Conductivity (EC		1180		µS/cm	2022-04-21	
Phosphorus, Tota		0.113	0.0050	Contraction of the Contraction o	2022-04-20	
		0.103	0.0050	mg/L	2022-04-20	
Phosphorus, Tota						
Phosphorus, Tota Total Metals						
Total Metals		77.7	0.20	mg/L	2022-04-20	
	1	77.7 42.4	the second se	mg/L mg/L	2022-04-20	



PROJECT	Oliver, Town of Ground Water Moni	toring		WORK ORDER REPORTED	22D1701 2022-04-22	2 16:08
Analyte		Result	RL	Units	Analyzed	Qualifie
/W7 - Public Wor	rks Yard (22D1701-0	7) Matrix: Water Sampled: 202	2-04-11 10:25			FILT, PRES
Anions						
Chloride		48.7	0.10	mg/L	2022-04-19	
Nitrate (as N)		2.58	0.010	mg/L	2022-04-19	HT1
Nitrite (as N)		< 0.010	0.010	mg/L	2022-04-19	HT1
Calculated Parame	ters					
Hardness, Total (a	s CaCO3)	278	0.500	mg/L	N/A	
Nitrate+Nitrite (as		2.58	0.0200	mg/L	N/A	
General Parameters	s					
Ammonia, Total (a	s N)	< 0.050	0.050	mg/L	2022-04-20	
BOD, 5-day Carbo		11,1	200 H 11 H 10 H	mg/L	2022-04-19	
Conductivity (EC)	, additional and a second s	770		μS/cm	2022-04-22	
Phosphorus, Total	(as P)	0.137	0.0050		2022-04-20	
Phosphorus, Total		0.118	0.0050		2022-04-20	
Total Metals		2010/2020				
Calcium, total		74.4	0.20	mg/L	2022-04-20	
Magnesium, total		22.3	0.010	1000 H201000	2022-04-20	
Sodium, total		30.4		mg/L	2022-04-20	
			4 40.45			
MW9 - Linear Par	rk (22D1701-08) Ma	trix: Water Sampled: 2022-04-1	1 10:45			FILT, PRES
MW9 - Linear Par	rk (22D1701-08) Ma	trix: Water Sampled: 2022-04-1	1 10:45			FILT, PRES
Anions	rk (22D1701-08) Ma			mg/L	2022-04-19	
Anions Chloride	rk (22D1701-08) Ma	37.9 3,18	0.10	mg/L mg/L	2022-04-19 2022-04-19	
Anions	rk (22D1701-08) Ma	37.9	0.10	mg/L		PRES
Anions Chloride Nitrate (as N) Nitrite (as N)		37.9 3.18	0.10	mg/L	2022-04-19	PRES HT1
Anions Chloride Nitrate (as N) Nitrite (as N) Calculated Parame	eters	37.9 3.18 < 0.010	0.10 0.010 0.010	mg/L mg/L	2022-04-19 2022-04-19	PRES HT1
Anions Chloride Nitrate (as N) Nitrite (as N) Calculated Parame Hardness, Total (a	eters as CaCO3)	37.9 3.18 < 0.010 312	0.10 0.010 0.010 0.500	mg/L mg/L mg/L	2022-04-19	PRES HT1
Anions Chloride Nitrate (as N) Nitrite (as N) Calculated Parame Hardness, Total (a Nitrate+Nitrite (as	eters as CaCO3) i N)	37.9 3.18 < 0.010	0.10 0.010 0.010	mg/L mg/L mg/L	2022-04-19 2022-04-19 N/A	PRES HT1
Anions Chloride Nitrate (as N) Nitrite (as N) Calculated Parameter Hardness, Total (a Nitrate+Nitrite (as General Parameter	eters as CaCO3) s N) rs	37.9 3.18 < 0.010 312 3.18	0.10 0.010 0.010 0.500 0.0200	mg/L mg/L mg/L mg/L	2022-04-19 2022-04-19 N/A N/A	PRES HT1
Anions Chloride Nitrate (as N) Nitrite (as N) Calculated Paramete Hardness, Total (a Nitrate+Nitrite (as General Parameter Ammonia, Total (a	eters as CaCO3) s N) rs as N)	37.9 3.18 < 0.010 312 3.18 < 0.050	0.10 0.010 0.010 0.500 0.0200 0.0200	mg/L mg/L mg/L mg/L	2022-04-19 2022-04-19 N/A N/A 2022-04-20	PRES HT1
Anions Chloride Nitrate (as N) Nitrite (as N) Calculated Parame Hardness, Total (a Nitrate+Nitrite (as General Parameter Ammonia, Total (a BOD, 5-day Carb	eters as CaCO3) s N) rs as N) onaceous	37.9 3.18 < 0.010 312 3.18 < 0.050 < 7.5	0.10 0.010 0.500 0.0200 0.050 2.0	mg/L mg/L mg/L mg/L mg/L	2022-04-19 2022-04-19 N/A N/A 2022-04-20 2022-04-19	PRES HT1
Anions Chloride Nitrate (as N) Nitrite (as N) Calculated Parame Hardness, Total (a Nitrate+Nitrite (as General Parameter Ammonia, Total (a BOD, 5-day Carb Conductivity (EC)	eters as CaCO3) i N) rs as N) onaceous	37.9 3.18 < 0.010 312 3.18 < 0.050 < 7.5 729	0.10 0.010 0.500 0.500 0.0200 0.050 2.0 2.0	mg/L mg/L mg/L mg/L mg/L μS/cm	2022-04-19 2022-04-19 N/A N/A 2022-04-20	PRES HT1
Anions Chloride Nitrate (as N) Nitrite (as N) Calculated Parame Hardness, Total (a Nitrate+Nitrite (as General Parameter Ammonia, Total (a BOD, 5-day Carb Conductivity (EC) Phosphorus, Tota	eters as CaCO3) : N) rs as N) onaceous) il (as P)	37.9 3.18 < 0.010 312 3.18 < 0.050 < 7.5 729 0.127	0.10 0.010 0.010 0.500 0.0200 0.0200 0.050 2.0 2.0 0.0050	mg/L mg/L mg/L mg/L mg/L μS/cm mg/L	2022-04-19 2022-04-19 N/A N/A 2022-04-20 2022-04-19 2022-04-22	PRES HT1
Anions Chloride Nitrate (as N) Nitrite (as N) Calculated Parameter Hardness, Total (a Nitrate+Nitrite (as General Parameter Ammonia, Total (a BOD, 5-day Carb Conductivity (EC) Phosphorus, Tota Phosphorus, Tota	eters as CaCO3) : N) rs as N) onaceous) il (as P)	37.9 3.18 < 0.010 312 3.18 < 0.050 < 7.5 729	0.10 0.010 0.500 0.500 0.0200 0.050 2.0 2.0	mg/L mg/L mg/L mg/L mg/L μS/cm mg/L	2022-04-19 2022-04-19 N/A N/A 2022-04-20 2022-04-20 2022-04-22 2022-04-22	PRES HT1
Anions Chloride Nitrate (as N) Nitrite (as N) Calculated Parame Hardness, Total (a Nitrate+Nitrite (as General Parameter Ammonia, Total (a BOD, 5-day Carb Conductivity (EC) Phosphorus, Tota Phosphorus, Tota Total Metals	eters as CaCO3) : N) rs as N) onaceous) il (as P)	37.9 3.18 < 0.010 312 3.18 < 0.050 < 7.5 729 0.127 0.0271	0.10 0.010 0.010 0.500 0.0200 0.0200 0.050 2.0 2.0 0.0050 0.0050	mg/L mg/L mg/L mg/L mg/L mg/L mg/L mg/L	2022-04-19 2022-04-19 N/A N/A 2022-04-20 2022-04-20 2022-04-20 2022-04-20	PRES HT1
Anions Chloride Nitrate (as N) Nitrite (as N) Calculated Parameter Hardness, Total (a Nitrate+Nitrite (as General Parameter Ammonia, Total (a BOD, 5-day Carb Conductivity (EC) Phosphorus, Tota Phosphorus, Tota	eters as CaCO3) ; N) rs as N) onaceous) onaceous) il (as P) il Dissolved	37.9 3.18 < 0.010 312 3.18 < 0.050 < 7.5 729 0.127	0.10 0.010 0.010 0.500 0.0200 0.0200 0.050 2.0 2.0 0.0050 0.0050 0.0050	mg/L mg/L mg/L mg/L mg/L μS/cm mg/L	2022-04-19 2022-04-19 N/A N/A 2022-04-20 2022-04-20 2022-04-22 2022-04-22	PRES HT1



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REPORTED TO PROJECT	Oliver, Town of Ground Water Monitoring			WORK ORDER REPORTED	22D1701 2022-04-2	2 16:08
Analyte		Result	RL	Units	Analyzed	Qualifie
MW10 - End of Ro	oad 5 (22D1701-09) Matrix:	Water Sampled: 2022-0	04-11 11:45			FILT, PRES
Anions						
Chloride		114	0.10	mg/L	2022-04-19	
Nitrate (as N)		4.13	0.010	mg/L	2022-04-19	HT1
Nitrite (as N)		< 0.010	0.010	mg/L	2022-04-19	HT1
Calculated Parame	iters					
Hardness, Total (a	as CaCO3)	470	0.500	mg/L	N/A	
Nitrate+Nitrite (as	N)	4.13	0.0200	mg/L	N/A	
General Parameter	's					
Ammonia, Total (a	as N)	< 0.050	0.050	mg/L	2022-04-20	
BOD, 5-day Carbo	onaceous	9.5	2.0	mg/L	2022-04-19	
Conductivity (EC)		1090	2.0	µS/cm	2022-04-22	
Phosphorus, Tota	I (as P)	0.0080	0.0050	mg/L	2022-04-20	
Phosphorus, Tota	I Dissolved	0.0053	0.0050	mg/L	2022-04-20	
Total Metals						
Calcium, total		95.9	0.20	mg/L	2022-04-20	
Magnesium, total	1	55.9	0.010	mg/L	2022-04-20	
wagnesium, total						

 Sample Qualifiers:

 FILT
 The sample has been filtered for TDP in the laboratory. Results may not reflect conditions at the time of sampling.

 HT1
 The sample was prepared and/or analyzed past the recommended holding time.

 PRES
 Sample has been preserved for NH3, TP, TDP in the laboratory and the holding time has been extended.



APPENDIX 1: SUPPORTING INFORMATION

REPORTED TO PROJECT	Oliver, Town Ground Wate	of er Monitoring	WORK ORDER REPORTED	22D1701 2022-04-2	2 16:08
Analysis Descri	ption	Method Ref.	Technique	Accredited	Location
Ammonia, Total in	Water	SM 4500-NH3 G* (2017)	Automated Colorimetry (Phenate)	4	Kelowna
Anions in Water		SM 4110 B (2017)	Ion Chromatography	~	Kelowna
Biochemical Oxyg Carbonaceous in		SM 5210 B (2017)	Dissolved Oxygen Meter	1	Kelowna
Conductivity in Wa	ater	SM 2510 B (2017)	Conductivity Meter	×	Kelowna
Hardness in Wate	r	SM 2340 B* (2017)	Calculation: 2.497 [total Ca] + 4.118 [total Mg] (Est)	✓	N/A
Phosphorus, Total Water	Dissolved in	SM 4500-P B.5* (2011) / SM 4500-P F (2017)	Persulfate Digestion / Automated Colorimetry (Ascorbic Acid)	~	Kelowna
Phosphorus, Total	l in Water	SM 4500-P B.5* (2011) / SM 4500-P F (2017)	Persulfate Digestion / Automated Colorimetry (Ascorbic Acid)	~	Kelowna
Total Metals in Wa	ater	EPA 200.2 / EPA 6020B	HNO3+HCI Hot Block Digestion / Inductively Coupled Plasma-Mass Spectroscopy (ICP-MS)	~	Richmond

Note: An asterisk in the Method Reference indicates that the CARO method has been modified from the reference method

Glossary of	Terms:
RL	Reporting Limit (default)
<	Less than the specified Reporting Limit (RL) - the actual RL may be higher than the default RL due to various factors
mg/L	Milligrams per litre
µS/cm	Microsiemens per centimetre
EPA	United States Environmental Protection Agency Test Methods
SM	Standard Methods for the Examination of Water and Wastewater, American Public Health Association

General Comments:

The results in this report apply to the samples analyzed in accordance with the Chain of Custody document. This analytical report must be reproduced in its entirety. CARO is not responsible for any loss or damage resulting directly or indirectly from error or omission in the conduct of testing. Liability is limited to the cost of analysis. Samples will be disposed of 30 days after the test report has been issued or once samples expire, whichever comes first. Longer hold is possible if agreed to in writing. The quality control (QC) data is available upon request

Please note any regulatory guidelines applied to this report are added as a convenience to the client, at their request, to help provide some initial context to analytical results obtained. Although CARO makes every effort to ensure accuracy of the associated regulatory guideline(s) applied, the guidelines applied cannot be assumed to be correct due to a variety of factors and as such CARO Analytical Services assumes no liability or responsibility for the use of those guidelines to make any decisions. The original source of the regulation should be verified and a review of the guideline (s) should be validated as correct in order to make any decisions arising from the comparison of the analytical data obtained to the relevant regulatory guideline for one's particular circumstances. Further, CARO Analytical Services assumes no liability or responsibility for any loss attributed from the use of these guidelines in any way.



CERTIFICATE OF ANALYSIS

REPORTED TO	Oliver, Town of 5971 Sawmill Road, PO Box 638 Oliver, BC V0H 1T0		
ATTENTION	Pamela Merkel	WORK ORDER	22D1701
PO NUMBER PROJECT PROJECT INFO	Ground Water Monitoring B.6.	RECEIVED / TEMP REPORTED COC NUMBER	2022-04-13 09:15 / 3.7°C 2022-04-22 16:08 No Number

Introduction:

CARO Analytical Services is a testing laboratory full of smart, engaged scientists driven to make the world a safer and healthier place. Through our clients' projects we become an essential element for a better world. We employ methods conducted in accordance with recognized professional standards using accepted testing methodologies and quality control efforts. CARO is accredited by the Canadian Association for Laboratories Accreditation (CALA) to ISO/IEC 17025:2017 for specific tests listed in the scope of accreditation approved by CALA.

Big Picture Sidekicks



You know that the sample you collected after snowshoeing to site, digging 5 meters, and racing to get it on a plane so you can submit it to the lab for time sensitive results needed to make important and expensive decisions (whew) is VERY important. We know that too. We've Got Chemistry

It's simple. We figure the more you enjoy working with our fun and engaged team members; the more likely you are to give us continued opportunities to support you.

SI

Ahead of the Curve



Through research, regulation knowledge, and instrumentation, we are your analytical centre for the technical knowledge you need, BEFORE you need it, so you can stay up to date and in the know.

If you have any questions or concerns, please contact me at bwhitehead@caro.ca

Authorized By:

Brent Whitehead Account Manager

unthet

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#110 4011 Viking Way Richmond, BC V6V 2K9 | #102 3677 Highway 97N Kelowna, BC V1X 5C3 | 17225 109 Avenue Edmonton, AB T5S 1H7 | #108 4475 Wayburne Drive Burnaby, BC V5G 4X4



Colliver Town of Colliver Ground Water Monitoring			WORK ORDER REPORTED	2211262 2022-09-15	5 16:03
Analyte	Result	RL	Units	Analyzed	Qualifie
/W1 - Air Cadet (22l1262-01) Matrix: Water	Sampled <mark>: 2022-09-07 08:40</mark>				FILT, PRES
Anions					
Chloride	22.2	0.10	CONTRACTOR C	2022-09-10	
Nitrate (as N)	8.30	0.010	and the second se	2022-09-10	
Nitrite (as N)	< 0.010	0.010	mg/L	2022-09-10	
Calculated Parameters					
Hardness, Total (as CaCO3)	320	0.500	mg/L	N/A	
Nitrate+Nitrite (as N)	8.30	0.0100	mg/L	N/A	
General Parameters					
	< 0.050	0.050	mg/L	2022-09-15	
Ammonia, Total (as N) BOD, 5-day Carbonaceous	< 6.1		mg/L	2022-09-15	
Conductivity (EC)	684		µS/cm	2022-09-15	
Phosphorus, Total (as P)	0.109	0.0050	and the second se	2022-09-13	
Phosphorus, Total Dissolved	0.0962	0.0050	mg/L	2022-09-13	
Total Metals					
	101	0.20	mg/L	2022-09-14	
Calcium, total Magnesium, total	16.3	and the second se	mg/L	2022-09-14	
Sodium, total	18.6		mg/L	2022-09-14	
MW2 - Rodeo Grounds (22l1262-02) Matrix	: Water Sampled: 2022-09-07 08:	:05			FILT, PRES
Anions	7.54	0.10	mo/l	2022-09-10	
Chloride	7.51		mg/L mg/L	2022-09-10	
Chloride Nitrate (as N)	0.872	0.010	mg/L		
Chloride Nitrate (as N) Nitrite (as N)		0.010	and the second se	2022-09-10	
Chloride Nitrate (as N) Nitrite (as N) Calculated Parameters	0.872 < 0.010	0.010 0.010	mg/L mg/L	2022-09-10 2022-09-10	
Chloride Nitrate (as N) Nitrite (as N) Calculated Parameters Hardness, Total (as CaCO3)	0.872 < 0.010 2980	0.010 0.010 2.50	mg/L	2022-09-10	
Chloride Nitrate (as N) Nitrite (as N) Calculated Parameters Hardness, Total (as CaCO3) Nitrate+Nitrite (as N)	0.872 < 0.010	0.010 0.010 2.50	mg/L mg/L mg/L	2022-09-10 2022-09-10 N/A	
Chloride Nitrate (as N) Nitrite (as N) Calculated Parameters Hardness, Total (as CaCO3) Nitrate+Nitrite (as N) General Parameters	0.872 < 0.010 2980 0.872	0.010 0.010 2.50 0.0100	mg/L mg/L mg/L mg/L	2022-09-10 2022-09-10 N/A	
Chloride Nitrate (as N) Nitrite (as N) Calculated Parameters Hardness, Total (as CaCO3) Nitrate+Nitrite (as N) General Parameters Ammonia, Total (as N)	0.872 < 0.010 2980 0.872 < 0.050	0.010 0.010 2.50 0.0100 0.050	mg/L mg/L mg/L	2022-09-10 2022-09-10 N/A N/A	
Chloride Nitrate (as N) Nitrite (as N) Calculated Parameters Hardness, Total (as CaCO3) Nitrate+Nitrite (as N) General Parameters Ammonia, Total (as N) BOD, 5-day Carbonaceous	0.872 < 0.010 2980 0.872 < 0.050 8.2	0.010 0.010 2.50 0.0100 0.050 2.0	mg/L mg/L mg/L mg/L mg/L	2022-09-10 2022-09-10 N/A N/A 2022-09-15	
Chloride Nitrate (as N) Nitrite (as N) Calculated Parameters Hardness, Total (as CaCO3) Nitrate+Nitrite (as N) General Parameters Ammonia, Total (as N) BOD, 5-day Carbonaceous Conductivity (EC)	0.872 < 0.010 2980 0.872 < 0.050 8.2 539	0.010 0.010 2,50 0.0100 0.050 2.0 2.0	mg/L mg/L mg/L mg/L mg/L mg/L	2022-09-10 2022-09-10 N/A N/A 2022-09-15 2022-09-15	
Chloride Nitrate (as N) Nitrite (as N) Calculated Parameters Hardness, Total (as CaCO3) Nitrate+Nitrite (as N) General Parameters Ammonia, Total (as N) BOD, 5-day Carbonaceous Conductivity (EC) Phosphorus, Total (as P)	0.872 < 0.010 2980 0.872 < 0.050 8.2 539 11.1	0.010 0.010 2.50 0.0100 0.050 2.0 2.0 0.0050	mg/L mg/L mg/L mg/L mg/L mg/L mg/L	2022-09-10 2022-09-10 N/A N/A 2022-09-15 2022-09-15 2022-09-15	
Chloride Nitrate (as N) Nitrite (as N) Calculated Parameters Hardness, Total (as CaCO3) Nitrate+Nitrite (as N) General Parameters Ammonia, Total (as N) BOD, 5-day Carbonaceous Conductivity (EC) Phosphorus, Total (as P) Phosphorus, Total Dissolved	0.872 < 0.010 2980 0.872 < 0.050 8.2 539	0.010 0.010 2.50 0.0100 0.050 2.0 2.0 0.0050	mg/L mg/L mg/L mg/L mg/L mg/L mg/L mg/L	2022-09-10 2022-09-10 N/A N/A 2022-09-15 2022-09-15 2022-09-15 2022-09-13	
Chloride Nitrate (as N) Nitrite (as N) Calculated Parameters Hardness, Total (as CaCO3) Nitrate+Nitrite (as N) General Parameters Ammonia, Total (as N) BOD, 5-day Carbonaceous Conductivity (EC) Phosphorus, Total (as P) Phosphorus, Total Dissolved Total Metals	0.872 < 0.010 2980 0.872 < 0.050 8.2 539 11.1 0.0132	0.010 0.010 2.50 0.0100 0.050 2.0 2.0 0.0050	mg/L mg/L mg/L mg/L mg/L mg/L mg/L μS/cm mg/L mg/L mg/L mg/L	2022-09-10 2022-09-10 N/A N/A 2022-09-15 2022-09-15 2022-09-13 2022-09-13	RS
Chloride Nitrate (as N) Nitrite (as N) Calculated Parameters Hardness, Total (as CaCO3) Nitrate+Nitrite (as N) General Parameters Ammonia, Total (as N) BOD, 5-day Carbonaceous Conductivity (EC) Phosphorus, Total (as P) Phosphorus, Total Dissolved	0.872 < 0.010 2980 0.872 < 0.050 8.2 539 11.1	0.010 0.010 2.50 0.0100 0.050 2.0 2.0 0.0050 0.0050 0.0050	mg/L mg/L mg/L mg/L mg/L mg/L mg/L mg/L	2022-09-10 2022-09-10 N/A N/A 2022-09-15 2022-09-15 2022-09-15 2022-09-13	RS



REPORTED TO PROJECT	Oliver, Town of Ground Water Monitoring	I		WORK ORDER REPORTED	2211262 2022-09-15	5 16:03
Analyte		Result	RL	Units	Analyzed	Qualifie
MW3 - Maple Gro	ounds (22l1262-03) Matrix	:: Water Sampled: 2022-0	9-07 07:55			FILT, PRES
Anions						
Chloride		9.04	0.10	mg/L	2022-09-10	
Nitrate (as N)		0.089	0.010	mg/L	2022-09-10	
Nitrite (as N)	1	< 0.010	0.010	mg/L	2022-09-10	
Calculated Parame	eters					
Hardness, Total (a	as CaCO3)	1260	0.500	mg/L	N/A	
Nitrate+Nitrite (as		0.0886	0.0100	mg/L	N/A	
General Parameter	rs					
		0.141	0.050	ma/L	2022-09-15	
Ammonia, Total (a BOD, 5-day Carb	Contraction of the Contraction o	< 6.1		mg/L	2022-09-15	
Conductivity (EC)	and a local design of the second s	806		µS/cm	2022-09-15	
Phosphorus, Tota		5.67	0.0050	1. Note without	2022-09-13	
Phosphorus, Tota		0.0130	0.0050	and and the other states of the states of th	2022-09-13	
Total Metals						
		0.50	0.20	mg/L	2022-09-14	
Calcium, total		353	0.20		2022-09-14	
Magnesium, total Sodium, total		91.9 19.0		mg/L	2022-09-14	
MW4 - Test Well	#4 - Sand Pit (22l1262-04)	Matrix: Water Sampled	: 2022-09-07 09:25	۵. ۲		FILT, PRES
Anions						THE
		121	0.10	mg/L	2022-09-10	
Chloride		121		mg/L mg/L	2022-09-10 2022-09-10	
			0.010			
Chloride Nitrate (as N)	ieters	1.35	0.010	mg/L	2022-09-10	
Chloride Nitrate (as N) Nitrite (as N) Calculated Param		1.35 < 0.010	0.010 0.010	mg/L	2022-09-10	
Chloride Nitrate (as N) Nitrite (as N)	(as CaCO3)	1.35	0.010 0.010	mg/L mg/L mg/L	2022-09-10 2022-09-10	
Chloride Nitrate (as N) Nitrite (as N) Calculated Param Hardness, Total ((as CaCO3) is N)	1.35 < 0.010 1610	0.010 0.010 0.500	mg/L mg/L mg/L	2022-09-10 2022-09-10 N/A	
Chloride Nitrate (as N) Nitrite (as N) Calculated Param Hardness, Total (Nitrate+Nitrite (as	(as CaCO3) s N) ers	1.35 < 0.010 1610	0.010 0.010 0.500 0.0100	mg/L mg/L mg/L	2022-09-10 2022-09-10 N/A	
Chloride Nitrate (as N) Nitrite (as N) Calculated Param Hardness, Total (Nitrate+Nitrite (ar General Paramete	(as CaCO3) is N) ers (as N)	1.35 < 0.010 1610 1.35	0.010 0.010 0.500 0.0100 0.050	mg/L mg/L mg/L mg/L	2022-09-10 2022-09-10 N/A N/A	
Chloride Nitrate (as N) Nitrite (as N) Calculated Param Hardness, Total (Nitrate+Nitrite (as General Paramete Ammonia, Total (BOD, 5-day Cart	(as CaCO3) is N) ers (as N) bonaceous	1.35 < 0.010 1610 1.35 < 0.050	0.010 0.010 0.500 0.0100 0.050 2.0	mg/L mg/L mg/L mg/L	2022-09-10 2022-09-10 N/A N/A 2022-09-15	
Chloride Nitrate (as N) Nitrite (as N) Calculated Param Hardness, Total (Nitrate+Nitrite (a: General Paramete Ammonia, Total ((as CaCO3) is N) ers (as N) bonaceous	1.35 < 0.010 1610 1.35 < 0.050 < 6.1	0.010 0.010 0.500 0.0100 0.050 2.0 2.0	mg/L mg/L mg/L mg/L mg/L	2022-09-10 2022-09-10 N/A N/A 2022-09-15 2022-09-15	
Chloride Nitrate (as N) Nitrite (as N) Calculated Param Hardness, Total (Nitrate+Nitrite (a: General Paramete Ammonia, Total (BOD, 5-day Cart Conductivity (EC	(as CaCO3) is N) ers (as N) bonaceous C) ial (as P)	1.35 < 0.010 1610 1.35 < 0.050 < 6.1 1710	0.010 0.010 0.500 0.0100 0.050 2.0 2.0 0.0550 0.0550	mg/L mg/L mg/L mg/L mg/L mg/L µS/cm	2022-09-10 2022-09-10 N/A N/A 2022-09-15 2022-09-15 2022-09-15	
Chloride Nitrate (as N) Nitrite (as N) Calculated Param Hardness, Total (Nitrate+Nitrite (a: General Paramete Ammonia, Total (BOD, 5-day Cart Conductivity (EC Phosphorus, Tota	(as CaCO3) is N) ers (as N) bonaceous C) ial (as P)	1.35 < 0.010 1610 1.35 < 0.050 < 6.1 1710 23.7	0.010 0.010 0.500 0.0100 0.050 2.0 2.0 0.0550 0.0550	mg/L mg/L mg/L mg/L mg/L mg/L μS/cm mg/L	2022-09-10 2022-09-10 N/A N/A 2022-09-15 2022-09-15 2022-09-15 2022-09-13	
Chloride Nitrate (as N) Nitrite (as N) Calculated Param Hardness, Total (Nitrate+Nitrite (a: General Paramete Ammonia, Total (BOD, 5-day Cart Conductivity (EC Phosphorus, Tota Phosphorus, Tota	(as CaCO3) is N) ers (as N) bonaceous C) ial (as P)	1.35 < 0.010 1610 1.35 < 0.050 < 6.1 1710 23.7 0.101	0.010 0.010 0.500 0.0100 0.050 2.0 0.0050 0.0050	mg/L mg/L mg/L mg/L mg/L mg/L μS/cm mg/L mg/L mg/L	2022-09-10 2022-09-10 N/A N/A 2022-09-15 2022-09-15 2022-09-15 2022-09-13	
Chloride Nitrate (as N) Nitrite (as N) Calculated Param Hardness, Total (Nitrate+Nitrite (as General Paramete Ammonia, Total (BOD, 5-day Cart Conductivity (EC Phosphorus, Total Phosphorus, Total	(as CaCO3) is N) ers (as N) bonaceous c) tal (as P) tal Dissolved	1.35 < 0.010 1610 1.35 < 0.050 < 6.1 1710 23.7	0.010 0.010 0.500 0.0100 0.050 2.0 2.0 0.0050 0.0050 0.0050	mg/L mg/L mg/L mg/L mg/L mg/L μS/cm mg/L	2022-09-10 2022-09-10 N/A N/A 2022-09-15 2022-09-15 2022-09-13 2022-09-13	



REPORTED TO PROJECT	Oliver, Town of Ground Water Moni	toring		WORK ORDER REPORTED	2211262 2022-09-15	5 16:03
Analyte		Result	RL	Units	Analyzed	Qualifie
MW5 - Test Well a	#5 - Chokecherry (22	1262-05) Matrix: Water Sampl	ed: 2022-09-07 09:3	5		FILT, PRES
Anions	_	2				
Chloride		16.1	0.10	mg/L	2022-09-10	
Nitrate (as N)		1.17	0.010	mg/L	2022-09-10	
Nitrite (as N)		< 0.010	0.010	mg/L	2022-09-10	
Calculated Parame	eters					
Hardness, Total (a	as CaCO3)	442	0.500	mg/L	N/A	
Nitrate+Nitrite (as		1.17	0.0100	mg/L	N/A	
General Paramete	rs					
Ammonia, Total (a	as N)	< 0.050	0.050	mg/L	2022-09-15	
BOD, 5-day Carb		< 6.1		mg/L	2022-09-15	
Conductivity (EC)	the second se	660		µS/cm	2022-09-15	
Phosphorus, Tota		2.01	0.0050		2022-09-13	
Phosphorus, Tota		0.0121	0.0050		2022-09-13	
Total Metals						
Calcium, total		134	0.20	mg/L	2022-09-14	
Magnesium, total	1	26.1		mg/L	2022-09-14	
Sodium, total	•	15.9		mg/L	2022-09-14	
MW6 - Fairview	Golf Course (22I1262	-06) Matrix: Water Sampled: 2	022-09-07 09:45			FILT, PRES
Chloride		95.7	0.10	mg/L	2022-09-10	
Nitrate (as N)		2.80		mg/L	2022-09-10	
Nitrite (as N)		0.010	0.010	mg/L	2022-09-10	
	neters					
Calculated Param				mall	N/A	
	(as CaCO3)	395	0.500	ing/L	INTA	
Hardness, Total	And the second se	395 2.81		mg/L	N/A	
20	is N)					
Hardness, Total Nitrate+Nitrite (a	s N) ers		0.0100			
Hardness, Total Nitrate+Nitrite (a General Paramete	is N) ers (as N)	2.81	0.0100) mg/L	N/A	
Hardness, Total Nitrate+Nitrite (a General Paramete Ammonia, Total	s N) ers (as N) bonaceous	2.81 < 0.050	0.0100 0.050 2.0 2.0) mg/L) mg/L) mg/L) µS/cm	N/A 2022-09-15 2022-09-15 2022-09-15	
Hardness, Total Nitrate+Nitrite (a General Paramete Ammonia, Total BOD, 5-day Car	s N) ers (as N) bonaceous C)	2.81 < 0.050 < 6.1	0.0100 0.050 2.0 2.0 0.0050) mg/L) mg/L) mg/L) µS/cm) mg/L	N/A 2022-09-15 2022-09-15 2022-09-15 2022-09-13	
Hardness, Total Nitrate+Nitrite (a General Paramete Ammonia, Total BOD, 5-day Carl Conductivity (EC	is N) ers (as N) bonaceous C) tal (as P)	2,81 < 0.050 < 6.1 1150	0.0100 0.050 2.0 2.0 0.0050) mg/L) mg/L) mg/L) µS/cm	N/A 2022-09-15 2022-09-15 2022-09-15	
Hardness, Total Nitrate+Nitrite (a General Paramete Ammonia, Total BOD, 5-day Car Conductivity (EC Phosphorus, Tot	is N) ers (as N) bonaceous C) tal (as P)	2.81 < 0.050 < 6.1 1150 0.117	0.0100 0.050 2.0 2.0 0.0050) mg/L) mg/L) mg/L) µS/cm) mg/L	N/A 2022-09-15 2022-09-15 2022-09-15 2022-09-13	
Hardness, Total Nitrate+Nitrite (a General Paramete Ammonia, Total BOD, 5-day Car Conductivity (EC Phosphorus, Tot Phosphorus, Tot Total Metals	is N) ers (as N) bonaceous C) tal (as P)	2.81 < 0.050 < 6.1 1150 0.117	0.0100 0.050 2.0 0.0050 0.0050) mg/L) mg/L) mg/L) µS/cm) mg/L	N/A 2022-09-15 2022-09-15 2022-09-15 2022-09-13	
Hardness, Total Nitrate+Nitrite (a General Paramete Ammonia, Total BOD, 5-day Car Conductivity (EC Phosphorus, Tot Phosphorus, Tot	is N) ers (as N) bonaceous C) tal (as P) tal Dissolved	2.81 < 0.050 < 6.1 1150 0.117 0.100	0.0100 0.050 2.0 0.0050 0.0050 0.0050	 mg/L mg/L mg/L mg/L µS/cm mg/L mg/L mg/L 	N/A 2022-09-15 2022-09-15 2022-09-15 2022-09-13 2022-09-13	



REPORTED TOOliver, Town ofPROJECTGround Water Mor	hitoring		WORK ORDER REPORTED	2211262 2022-09-1	5 16:03
Analyte	Result	RL	Units	Analyzed	Qualifie
MW7 - Public Works Yard (22l1262-0	7) Matrix: Water Sampled: 202	2-09-07 07:40			FILT, PRES
Anions					
Chloride	87.8	0.10	mg/L	2022-09-10	
Nitrate (as N)	1.34	0.010	mg/L	2022-09-10	
Nitrite (as N)	0.132	0.010	mg/L	2022-09-10	
Calculated Parameters					
Hardness, Total (as CaCO3)	353	0.500	mg/L	N/A	
Nitrate+Nitrite (as N)	1.47	0.0100	mg/L	N/A	
General Parameters					
Ammonia, Total (as N)	0.737	0.050	mg/L	2022-09-15	
BOD, 5-day Carbonaceous	< 6.1		mg/L	2022-09-15	
Conductivity (EC)	941		μS/cm	2022-09-15	
Phosphorus, Total (as P)	0.484	0.0050	• A Data School and	2022-09-13	
Phosphorus, Total Dissolved	0.438	0.0050	and the second se	2022-09-13	
Total Metals					
Calcium, total	98.7	0.20	mg/L	2022-09-14	
Magnesium, total	25.7		mg/L	2022-09-14	
Sodium, total	48.2		mg/L	2022-09-14	
MW9 - Linear Park (22l1262-08) Ma	trix: Water Sampled: 2022-09-0	7 08:45			FILT, PRES
Anions		0.40		2022-09-10	
Chloride	85.1	to be a set of the set	mg/L mg/L	2022-09-10	
Nitrate (as N)	3.90		mg/L	2022-09-10	
Nitrite (as N)	0.040	0.010	iligre .	2022 00 10	
Calculated Parameters	674	0.500	mg/L	N/A	
Hardness, Total (as CaCO3)	674 3.94	0.0100		N/A	
Nitrate+Nitrite (as N)	3.34	0.0100	ingic		
General Parameters	< 0.050	0.050	mg/L	2022-09-15	
Ammonia, Total (as N)	< 0.050		mg/L mg/L	2022-09-15	
BOD, 5-day Carbonaceous	713		μS/cm	2022-09-15	
Conductivity (EC)	8.56) mg/L	2022-09-13	
Phosphorus, Total (as P)	0.0327) mg/L	2022-09-13	
Phosphorus, Total Dissolved	0.0321	0.0000			
Total Metals	1282/12			0000 00 44	
	191	0.20) mg/L	2022-09-14	
Calcium, total				0000 00 44	
Calcium, total Magnesium, total Sodium, total	47.9	0.010) mg/L) mg/L	2022-09-14 2022-09-14	



REPORTED TO PROJECT	Oliver, Town of Ground Water Monitori	ng		WORK ORDER REPORTED	2211262 2022-09-1	5 16:03
Analyte		Result	RL	Units	Analyzed	Qualifie
MW10 - Rd #5 (22	W10 - Rd #5 (22l1262-09) Matrix: Water Sampled: 2022-09-07 10:00					FILT, PRES
Anions						
Chloride		115	0.10	mg/L	2022-09-10	
Nitrate (as N)		4.30	0.010	mg/L	2022-09-10	
Nitrite (as N)		0.044	0.010	mg/L	2022-09-10	
Calculated Parame	eters					
Hardness, Total (a	as CaCO3)	498	0.500	mg/L	N/A	
Nitrate+Nitrite (as		4.34	0.0100	mg/L	N/A	
General Parameter	rs					
Ammonia, Total (a	as N)	< 0.050	0.050	mg/L	2022-09-15	
BOD, 5-day Carb		< 6.1	2.0	mg/L	2022-09-15	
Conductivity (EC)		1080	2.0	µS/cm	2022-09-15	
Phosphorus, Tota		0.0133	0.0050	mg/L	2022-09-13	
Phosphorus, Tota	Dissolved	0.0097	0.0050	mg/L	2022-09-13	
Total Metals						
Calcium, total		108	0.20	mg/L	2022-09-14	
Magnesium, total		55.1	0.010	mg/L	2022-09-14	
Sodium, total		18.3	0.10	mg/L	2022-09-14	

Sample Qualifiers:

FILT The sample has been filtered for TDP in the laboratory. Results may not reflect conditions at the time of sampling.

PRES Sample has been preserved for TDP, TP, NH3 in the laboratory and the holding time has been extended.

RS1 The Reporting Limits for this sample have been raised due to high analyte concentration and/or matrix interference.



APPENDIX 1: SUPPORTING INFORMATION

REPORTED TO PROJECT	Oliver, Town Ground Wate		WORK ORDER REPORTED	2211262 2022-09-1	5 16:03
Analysis Descri	ption	Method Ref.	Technique	Accredited	Location
Ammonia, Total in	Water	SM 4500-NH3 G* (2017)	Automated Colorimetry (Phenate)	1	Kelowna
Anions in Water		SM 4110 B (2017)	Ion Chromatography	✓	Kelowna
Biochemical Oxyg Carbonaceous in V		SM 5210 B (2017)	Dissolved Oxygen Meter	~	Kelowna
Conductivity in Wa	ater	SM 2510 B (2017)	Conductivity Meter	1	Kelowna
Hardness in Water		SM 2340 B* (2017)	Calculation: 2.497 [total Ca] + 4.118 [total Mg] (Est)	~	N/A
Phosphorus, Total Dissolved in Water		SM 4500-P B.5* (2011) / SM 4500-P F (2017)	Persulfate Digestion / Automated Colorimetry (Ascorbic Acid)		Kelowna
Phosphorus, Total in Water SM 4500-P B.5* (SM 4500-P B.5* (2011) / SM 4500-P F (2017)	Persulfate Digestion / Automated Colorimetry (Ascorbic Acid)	×	Kelowna
Total Metals in Wa	ater	EPA 200.2 / EPA 6020B	HNO3+HCI Hot Block Digestion / Inductively Coupled Plasma-Mass Spectroscopy (ICP-MS)	1	Richmond

Note: An asterisk in the Method Reference indicates that the CARO method has been modified from the reference method

Glossary of Terms:

RL	Reporting Limit (default)
<	Less than the specified Reporting Limit (RL) - the actual RL may be higher than the default RL due to various factors
mg/L	Milligrams per litre
µS/cm	Microsiemens per centimetre
EPA	United States Environmental Protection Agency Test Methods
SM	Standard Methods for the Examination of Water and Wastewater, American Public Health Association

General Comments:

The results in this report apply to the samples analyzed in accordance with the Chain of Custody document. This analytical report must be reproduced in its entirety. CARO is not responsible for any loss or damage resulting directly or indirectly from error or omission in the conduct of testing. Liability is limited to the cost of analysis. Samples will be disposed of 30 days after the test report has been issued or once samples expire, whichever comes first. Longer hold is possible if agreed to in writing. The quality control (QC) data is available upon request

Results in **Bold** indicate values that are above CARO's method reporting limits. Any results that are above regulatory limits are highlighted red. Please note that results will only be highlighted red if the regulatory limits are included on the CARO report. Any Bold and/or highlighted results do <u>not</u> take into account method uncertainty. If you would like method uncertainty or regulatory limits to be included on your report, please contact your Account Manager:bwhitehead@caro.ca

Please note any regulatory guidelines applied to this report are added as a convenience to the client, at their request, to help provide some initial context to analytical results obtained. Although CARO makes every effort to ensure accuracy of the associated regulatory guideline(s) applied, the guidelines applied cannot be assumed to be correct due to a variety of factors and as such CARO Analytical Services assumes no liability or responsibility for the use of those guidelines to make any decisions. The original source of the regulation should be verified and a review of the guideline (s) should be validated as correct in order to make any decisions arising from the comparison of the analytical data obtained to the relevant regulatory guideline for one's particular circumstances. Further, CARO Analytical Services assumes no liability or responsibility for any loss attributed from the use of these guidelines in any way.



CERTIFICATE OF ANALYSIS

REPORTED TO	Oliver, Town of 5971 Sawmill Road, PO Box 638 Oliver, BC V0H 1T0		
ATTENTION	Angela Moore	WORK ORDER	2211262
PO NUMBER PROJECT PROJECT INFO	Ground Water Monitoring B.6.	RECEIVED / TEMP REPORTED COC NUMBER	2022-09-08 09:25 / 17.3°C 2022-09-15 16:03 No Number

Introduction:

CARO Analytical Services is a testing laboratory full of smart, engaged scientists driven to make the world a safer and healthier place. Through our clients' projects we become an essential element for a better world. We employ methods conducted in accordance with recognized professional standards using accepted testing methodologies and quality control efforts. CARO is accredited by the Canadian Association for Laboratories Accreditation (CALA) to ISO/IEC 17025:2017 for specific tests listed in the scope of accreditation approved by CALA.

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Big Picture Sidekicks



You know that the sample you collected after snowshoeing to site, digging 5 meters, and racing to get it on a plane so you can submit it to the lab for time sensitive results needed to make important and expensive decisions (whew) is VERY important. We know that too. It's simple. We figure the more you enjoy working with our fun and engaged team members; the more likely you are to give us continued opportunities to support you.

SÀ

Ahead of the Curve



Through research, regulation knowledge, and instrumentation, we are your analytical centre for the technical knowledge you need, BEFORE you need it, so you can stay up to date and in the know.

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If you have any questions or concerns, please contact me at bwhitehead@caro.ca

Authorized By:

Brent Whitehead Account Manager

untheat

1-888-311-8846 | www.caro.ca #110 4011 Viking Way Richmond, BC V6V 2K9 | #102 3677 Highway 97N Kelowna, BC V1X 5C3 | 17225 109 Avenue Edmonton, AB T5S 1H7 | #108 4475 Wayburne Drive Burnaby, BC V5G 4X4

APPENDIX J

Soils Classification & Description



June 23, 2020

Town of Oliver c/o Western Water Associates Ltd. #106-5145 26 Street, Vernon, BC V1T 8G4

RE: OPERATIONAL CERTIFICATE NUMBER PE-13717 SOIL ASSESSMENT PROGRAM – NEW RECLAIMED WATER IRRIGATION AREAS

Attention: Ryan Rhodes, P.Geo.

1. INTRODUCTION

The Town of Oliver (the Town) currently discharges the reclaimed municipal wastewater from its wastewater treatment facility (WWTF) to ground by irrigation under the authorization of Operational Certificate (OC) PE-13717. The Town wishes to expand the area that is authorized for irrigation with reclaimed municipal wastewater and will therefore require an amendment to the OC. Hugh Hamilton, P.Ag., of Hamilton and Associates was retained by Western Water Associates Ltd., on behalf of the Town, to complete a soil assessment to determine whether the lands on planned new irrigation areas are capable of accepting reclaimed wastewater for irrigation purpose. The requirements for the soils assessment are specified in Section 6.9 of the OC.

The assessment was completed through a combination of a review of background information (including soil maps and reports, climate data, land use zoning maps, and aerial photographs), a field reconnaissance completed on June 3, 2020, and data analyses and interpretation. Additional information on methods is contained in Section 4.

2. DESCRIPTION OF THE PLANNED NEW IRRIGATION AREAS

Four irrigation areas are to be added to the approved land base for reclaimed water irrigation:

- The playing fields and park land located between Oliver Elementary School and South Okanagan High School (Figure 1 – maps and photos are at end of report). All of this parcel is currently covered with turfgrass and is irrigated with an underground sprinkler system (Photo 1). There are mature trees around the edges of the fields.
- Oliver Cemetery (Figure 2). The cemetery grounds are primarily vegetated with turfgrass (Photos 3 and 4) and are irrigated with underground sprinklers. Trees (mostly cedar) are planted around the property boundary, and there are some deciduous tree among the monuments.
- Oliver Community Park located immediately east of the Okanagan River on Fairview Road (Figure 3). The park includes three baseball/softball fields, a lawn bowling green, and areas for walking and sitting. The ground cover is turfgrass and there are a number of mature trees in the

areas outside the ball fields and on the small area on the north side of Fairview Road (Photo 5). The park is irrigated with an underground sprinkler system.

 Oliver Municipal Airport (Map 4). The new irrigation area is the strip of industrial-zoned land on the east side of the runway (Photo 7). The fields surrounding the runway to the west are already authorized for reclaimed water irrigation. The new irrigation area is mostly unoccupied although some parts are used for storage and there is one building. It appears that the topsoil was stripped from parts of the site and transported off-site. Vegetation cover is limited (about 25-50% on average) and includes alfalfa, agronomic and native grasses, and invasive species (see Section 4). It is not currently irrigated.

3. EXISTING SOILS, LAND USE AND EXPOSURE POTENTIAL

Soil information for the subject property was obtained from the BC Soil Information Finder Tool (SIFT). Figures 1 to 4 show the spatial distribution of soil types on the planned irrigation sites, and the soil properties are summarized in Table 1. Soils at the school and airport sites are mapped by BC as 100% Rutland soils, which are classified as Orthic Dark Brown Chernozems, developed on glacio-fluvial deposits. They typically are gravelly with a sandy or sandy loam surface texture (Photo 2). Soils at the cemetery are Ponderosa soils developed on alluvial fan deposits with a fluvial veneer. They are classified as Rego Dark Brown Chernozems and are also gravelly within sandy loam. The soils in the park have been developed on fluvial and floodplain deposits. About 90% of the irrigated area is classified as Kinney soils and are Gleyed Regosols (signifying that they are relatively young and that the soil profile is routinely saturated for an extended period). The northwest part of the park as mapped as Cawston soils, a Rego Gleysol (indicating somewhat greater soil profile development but also routinely saturated). The Kinney soils have a sandy loam or loam texture with some silt lenses, while the Cawston soil is a silt loam (Photo 6).

Because the sites are all located within the municipal boundaries, there are no published agricultural capability maps. All of the sites are located outside of the BC Agricultural Land Reserve.

The school grounds are used by the school students of sports and general play when school is in session, and by the public for recreation without restriction at all other times. The cemetery is open to the public and family visits every day during specified hours. Oliver Community Park is always open to public use. The airport lands are located behind a locked gate, so public access is unlikely. Based on the definitions in the BC Reclaimed Water Guidelines (BC Ministry of Environment 2013), the school grounds, park and cemetery would be considered "High Exposure Potential" while the airport is "Low Exposure Potential". The school, park and cemetery also would be considered "high public use lands" as per Section 5.1.2 of the OC, while the airport is "low public use lands". The treatment standard for use of reclaimed water on these sites varies slightly between the regulatory documents (Table 2). The OC requirements are understood to take precedence over the other documents, although Section 5.1.2 says that irrigation shall conform to guidelines developed by BC, so the Reclaimed Water guidelines should also apply (note that it sets limits for *E. coli*, not fecal coliforms).

Soil Name	Rutland	Kinney	Cawston	Ponderosa	
Sites where present	Airport (AP), Schools (SC)	Oliver Community Park (PK)	Oliver Community Park	Cemetery (CM)	
Approximate coverage on sites	AP-100%, SC-100%	PK – 90%	PK- 10%	CM - 100%	
Classification	Orthic Dark Brown Chernozem	Gleyed Regosol	Rego Humic Gleysol	Rego Dark Brown Chernozem	
Parent material	Sandy veneer over glacial- fluvial deposits	Loamy fluvial veneer over sandy floodplain deposits	Fluvial deposits	Fluvial veneer over fluvial fan deposits	
Texture	Sandy loam, loamy sand	Sandy loam/loam with some silt lenses	Silt loam or loam	Gravelly/very gravelly sandy loam or gravelly loam	
Drainage	Rapid	Imperfect	Poor to imperfect	Well to rapid	
Water holding capacity	Low	Moderate to low	High	Low	
Major soil limitations for crops	Stoniness, low available moisture holding capacity, low natural fertility	High water tables near Okanagan River; moderate salinity	Short duration fluctuating groundwater table in sandy & gravelly subsoils during spring freshet	Stoniness; susceptible to soil acidification after several years or irrigation & fertilization	

Table 1 – Soils on the Planned Irrigation Sites

Sources: Government of British Columbia. (2019); Wittneben (1986); Gough et al. (1994).

Table 2 Standards for bacteriological quality of reclaimed water for irrigation

Regulatory Document	School grounds, cemetery & park	Airport
Operational Certificate PE-	Maximum 2.2 MPN/100 mL	Maximum 200 MPN/100 mL
13717	fecal coliforms	fecal coliforms
Reclaimed Water Guideline	1 CFU/100 mL or 2 MPN/ 100 mL	Not specified
(BC MoE 2013)	E. coli	
Municipal Wastewater	Median <1 CFU/100 mL or <2.2	Median <200 CFU/100 mL fecal
•	MPN fecal coliforms; maximum	coliforms; maximum 1,000
Regulation	14 CFU/100 mL	CFU/100 mL

4. RESULTS OF THE ASSESSMENT

4.1 Soil Properties

The field assessment took place on June 3, 2020. The weather was clear and sunny although there had been some rainfall over the previous several days. The field work was completed by Hugh Hamilton, P.Ag. with the assistance of Ryan Rhodes, P.Geo., of Western Water. At each site, several boreholes were completed with a hand auger to a depth of between approximately 0.3 and 0.7 metres. The characteristics of the soil at each location were noted including the thickness of the upper (A or Ap) horizon, presence/depth of roots, soil texture (by hand), soil colour, presence/absence of mottles (iron staining), and the amount of gravel (based on the Soil Classification Working Group, 1998). In most cases it was not possible to auger beyond about 0.5 m depth because of the amount of gravel in the soil. In addition to the boreholes, we noted the vegetation cover and general drainage patterns, and looked for evidence of water ponding or running off the sites from previous irrigation or rainfall.

The soil properties observed in the field were consistent with the existing BC mapping, indicating that the published soil information (SIFT) can be relied upon for irrigation planning. The key exception is the land on the airport site where the topsoil (likely the Ap horizon¹ or the combined A and B horizons appear to have been stripped off in places, exposing the underlying gravelly BC or C horizon that is characteristic of the Rutland soil (Wittneben 1986). This was confirmed by digging a soil pit or the west side of the fence in the alfalfa field that surrounds the runway, where a dark brown Ap horizon (~0.3 m thick) was present (Photo 8). At the airport site there is considerable gravel exposed on the surface among pockets of thin sandy soil. The vegetation cover is sparse (Photos 7, 9 and 10).

The soils in Oliver Community Park were moist but not saturated at the time of the site visit, and no free water was encountered in any of the auger holes. At depths beyond about 0.15 m the soils were greybrown in colour with faint mottling, indicating periodic saturation and reducing conditions. These properties may reflect conditions prior to creation of the park and construction of the dike along the Okanagan River. However, a high water table is likely during spring freshet when the river level is high.

¹ The "p" in the Ap soil horizon descriptor represent the plow layer, where previous cultivation has typically blended the natural A and part of the natural B horizons.

4.2 Capability for Irrigation

Table 3 shows the monthly average irrigation demand for the soils on the planned irrigation sites. These estimates were generated using the BC Irrigation Calculator² for the soil textures confirmed in the field. At the school, cemetery, and park sites the crop is grass, while the crop at the airport was assumed to be alfalfa, like the neighbouring field (alfalfa is currently sporadically present on the new fields – Photo 10). Sprinkler was selected as the irrigation method except at the airport, where a solid set gun was assumed (consistent with the method used on the fields around the runway). The irrigation demand values in Table 3 are presented as cubic metres per hectare per day for the specified month as well as a total volume per hectare for the core May 1 to September 30 irrigation season.

Based on the soil assessment and the irrigation capacity calculations, the school, cemetery, and park sites are all suitable for irrigation with reclaimed water, subject to the regulatory requirements for reclaimed water and assuming best practices are followed for irrigation on public lands (Section 4.3).

It is important to note that the irrigation demand values shown are estimates of average rates based on modelling data and should be used for guidance only. Specific sites may be capable of using more or less water in any specific year depending on the weather. Except for the new areas at the airport, the other sites are currently irrigated, and the Town of Oliver and School Board operators have considerable experience managing the irrigation regime on their sites. In general, the irrigation volumes should be managed to optimize crop growth while meeting the regulations and best practices for the use of reclaimed water. Additional guidance on irrigation operations is provided in the next section.

² On-line at: <u>http://bcwatercalculator.ca/agriculture/irrigation</u>

Site	Community Park – N. Part	Community Park – Middle Part	Community Park – S. Part	Airport*	Cemetery	Schools – N. Side	Schools – S. Side
PID	001486683	006278159	026967201	007629583	n/a	001486683	010562401
Dominant Soil	Cawston	Kinney	Kinney	Rutland	Ponderosa	Rutland	Rutland
Irrigation Period**	Apr 27 – Oct 1	Apr 27 – Oct 1	Apr 27 – Oct 1	Apr 26 – Oct 1	Apr 27 – Oct 1	Apr 29 – Oct 1	Apr 29 – Oct 1
VOLUME PER HECTARE	m³/ha/day	m³/ha/day	m³/ha/day	m³/ha/day	m ³ /ha/day	m³/ha/day	m ³ /ha/day
April	0.68	0.88	0.85	0.88	zero	1.75	0.00
Мау	32	42	42	56	35	42	37
June	56	72	72	96	77	72	71
July	71	91	91	121	99	91	90
August	59	75	75	100	82	75	75
September	37	48	48	64	52	48	48
October	53	67	68	90	75	67	67
TOTAL MAY-SEPT (m ³ /ha)	7,833	10,042	10,042	13,407	10,575	10,043	9,822

Table 3Estimated Average Irrigation Rate by land parcel

*Airport values in Italics would apply if the topsoil were intact. Values shown are not appropriate under current conditions and should not be used. See text Section 4.3 for recommendations.

**Irrigation period is from the BC Agriculture Water Calculator. Note that irrigation typically occurs on few days in both April and October. The total volume per hectare for the core May 1 to September 30 irrigation season is intended to provide guidance for irrigation planning purposes.

4.3 Operational Considerations

Irrigation must follow the conditions specified in the OC. Following are the key clauses that apply to new reclaimed water irrigation on the four sites:

- Section 5.1.2 Disinfection must meet the requirements of the OC (≤2.2 MPN/100 mL fecal coliforms) and the Reclaimed Water Guideline ≤1 CFU/100 mL or ≤2 MPN/ 100 mL *E. coli*).
- Section 5.2 The irrigation period is March 15 to October 31.
- Section 5.3 No reclaimed water shall be applied within 15 m of a stream (e.g. Okanagan River at the park site) or waterbody, or within 30 m of a well used for domestic supply.
- Sections 5.4 and 5.5 No surface runoff of irrigated runoff shall occur, and no water should emerge from slopes located downgradient of the irrigated areas (known as tail water).
- Section 4.5 Spray irrigation water must not drift in the air off-site, e.g. as an aerosol.
- Section 5.7.2 Irrigation should not cause the soils to become saturated or cause soil erosion or instability.

Section 5.7.1 of the OC states that the irrigation rates should follow the 1989 BC Sprinkler Irrigation Manual. That manual was published before the province developed its current irrigation demand models or the BC Agriculture Water Calculator. The irrigation rates shown above in Table 3 are preferred over the single value given for Oliver in the 1989 manual because they are customized for each soil polygon.

In addition, the following practices from the BC Reclaimed Water Guideline (p. 20) should be followed at the **school, cemetery, and park sites**.

- No direct contact shall occur between the reclaimed water and any person while irrigation is underway.
- Residual chlorine should be present in the reclaimed water at the point of use at a concentration of at least 0.5 mg/L.
- There should be signs indicating that reclaimed water is used for irrigation (as per OC Section 3.12.1).
- The movement of irrigation water below the rooting zone to groundwater must be minimized.
- Periodic sampling (i.e. annually) and testing of the reclaimed water for metals and ions (specifically sodium and chloride) should take place, with the results compared to the applicable BC and Canadian water quality guidelines. This is in addition to the testing for BOD, TSS and nutrients under the OC.

At the **airport**, special irrigation management is necessary because of the lack of topsoil and the sparse vegetative cover on the site, which could result in excessive volumes of reclaimed water moving to groundwater rather than being evapotranspired. Irrigation of this site should begin in a limited fashion until it can be demonstrated that irrigation can meet the same guidelines and standards for the other sites, as listed above. The recommended approach is as follows:

• Irrigation of the site should not start before June 15 and should finish by September 10.

- Start with about one-half the prescribed monthly rate from the BC calculator (Table 3; e.g. maximum 60 m³/ha/day in July). Monitor the to see if the alfalfa and grasses on-site respond with increased growth and expanded surface coverage.
- If feasible, apply a layer (approximately 10 cm) of soil, compost or biosolids before beginning
 irrigation in the first year. This is to improve water and nutrient retention and to promote
 vegetative growth. This could begin with a pilot test program on several plots (e.g. three 20 m ×
 20 m plots) to fine-tune the methodology.
- All other conditions in the OC and the Reclaimed Water Guideline must also apply.

If the vegetation cover becomes better established and an organic litter layer builds up on the surface, the length of the irrigation season and the irrigation rate may be increased at the new airport site until they approach the guidelines for a Rutland soil.

5. CONCLUSIONS AND RECOMMENDATIONS

To conclude, the schoolyard, cemetery, and park sites are all suitable for irrigation with reclaimed water, subject to the regulatory requirements for reclaimed water and assuming best practices are followed for irrigation on public lands (as listed in Section 4.3). The airport lands located east of the existing irrigated lands will require special management if they are to be irrigated with reclaimed water, due to the lack of topsoil and the sparse vegetation. Irrigation can proceed within a limited season only (June 15 to September 10), initially using rates that are about one-half of the BC Agriculture Water Calculator. If the vegetative cover improves and a layer of organic litter develops on the surface, then the schedule and irrigation rates may be re-evaluated. If possible, a layer of soil, biosolids or compost should be applied prior to irrigation to improve water and nutrient retention.

6. CLOSURE

This report was prepared exercising the standard of care, skill and diligence which is reasonably expected within the agrology profession involved in the assignment, in the location of the assignment, as measured by professional standards applicable during the performance of the services. No other warranty or guarantee, expressed, implied or statutory, is made or intended by this report.

I trust this completes this assignment to your satisfaction. Please contact the undersigned at (250) 938-3408 if you have any questions or require additional information.

Sincerely, Hamilton and Associates

Hugh Hamilton, Ph.D., P.Ag Senior Scientist

Attachments: Figures 1-4 and Photographs.



REFERENCES

- BC Ministry of Environment 2013. Reclaimed Water Guideline: A companion document to the Municipal Wastewater Regulation. Victoria. 44 pp.
- Gough, N., G. Hughes-Games, and D. Nikkel. 1994. Soil Management Handbook for the Okanagan and Similkameen Valleys. 1st Edition. B.C. Ministry of Agriculture, Fisheries and Food.
- Government of British Columbia. 2019. Soil Information Finder Tool (SIFT). On-line at: https://www2.gov.bc.ca/gov/content/environment/air-land-water/land/soil/soil-information-finder
- Soil Classification Working Group. 1998. The Canadian System of Soil Classification. 3rd Edition. Agriculture and Agri-Food Canada. Ottawa.
- Wittneben, U. 1986. Soils of the Okanagan and Similkameen Valley. Report no. 52, BC Soil Survey. Ministry of Environment. Victoria. 229 pp.

PHOTOGRAPHS



Photo 1. Sports field with turfgrass cover between elementary and high schools.



Photo 2: Typical surface soil (~4-20 cm below surface) at school site.



Photo 3: Lawn area along cemetery boundary, currently irrigated.



Photo 4: Cemetery overview showing unirrigated and irrigated (background) areas.



Photo 5: Oliver Community Park from dike looking northeast.



Photo 6: Example of silty soil in north part of Oliver Community Park



Photo 7: Proposed new irrigation area at airport. Note exposed sub-soil and relatively spare vegetative cover [Land on right side of photo may receive some irrigation water from fields near runway (yellow flowers)].



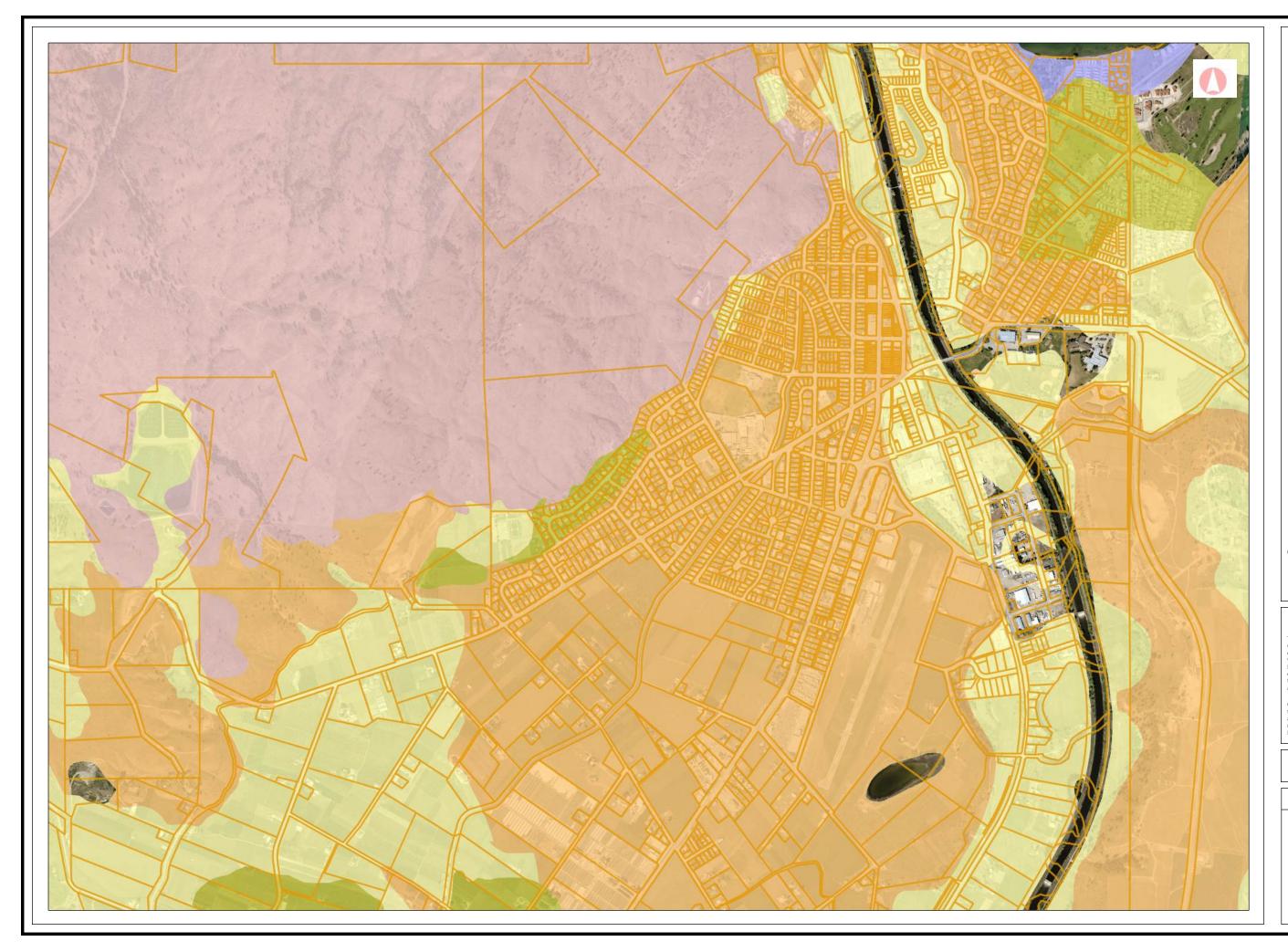
Photo 8: Surface soil in irrigated fields. Note intact dark upper horizon and presence of gravel throughout.

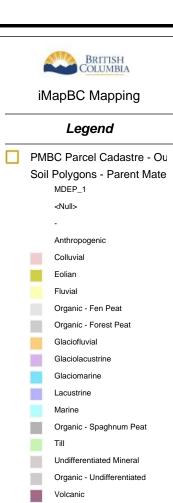


Photo 9: Soil pit on proposed irrigation area at airport. At this location, a residual A/Ap horizon is present. Note fine roots in upper 10 cm.



Photo 10: Ground surface at new airport irrigation area where topsoil may have been partially removed. Note how alfalfa plants are green as their roots obtain moisture from deep within soil.





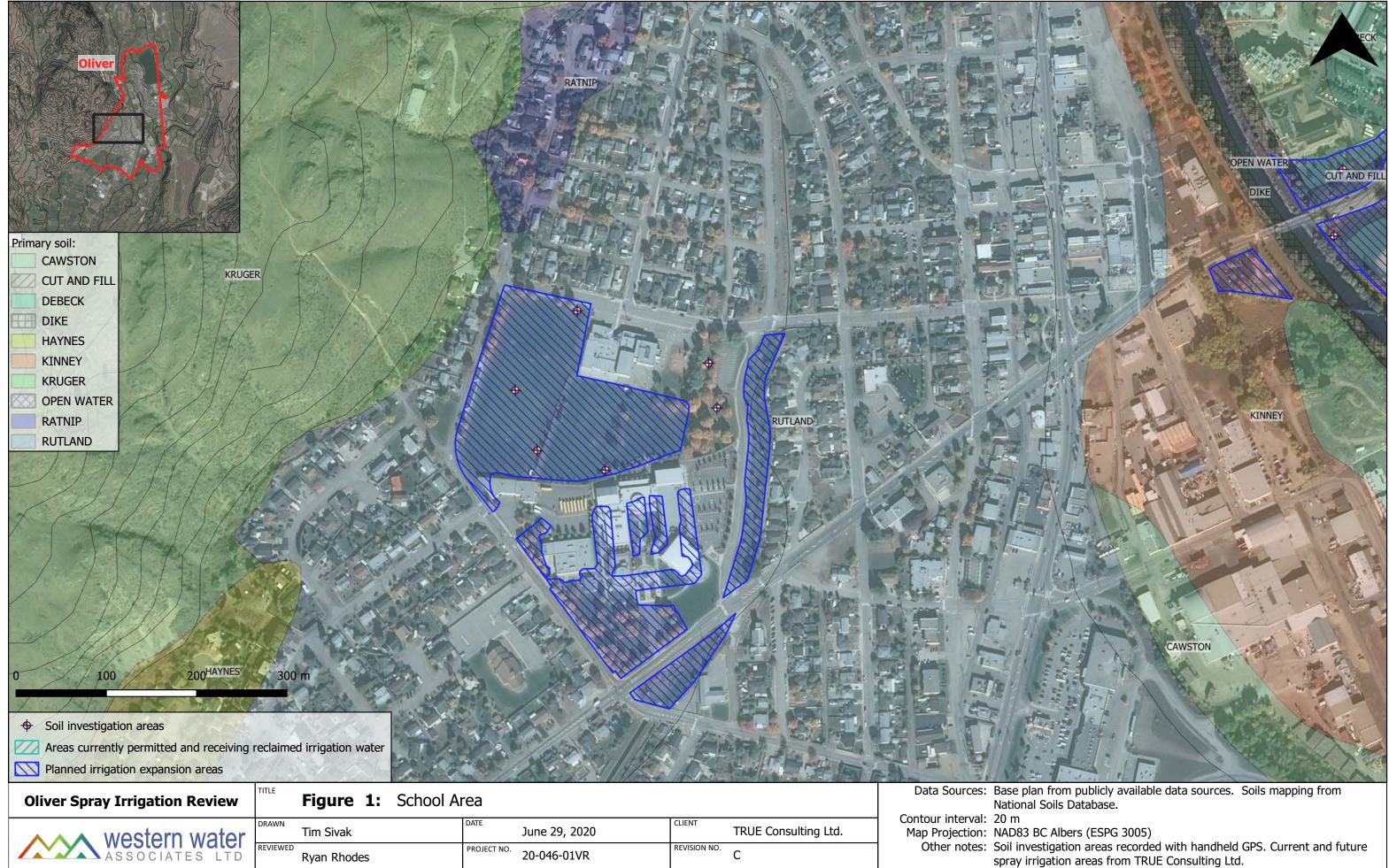
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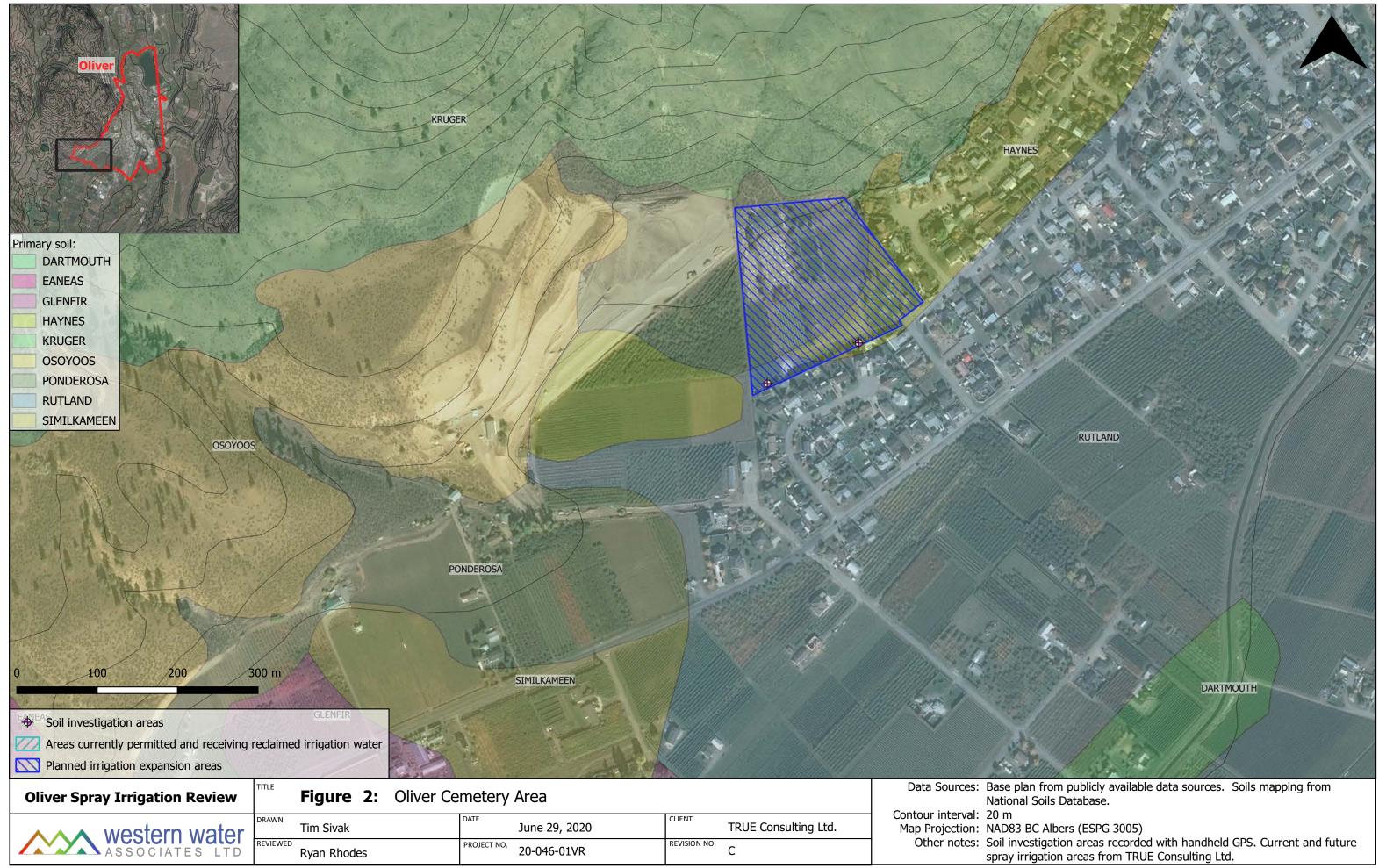
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Key Map of British Columbia





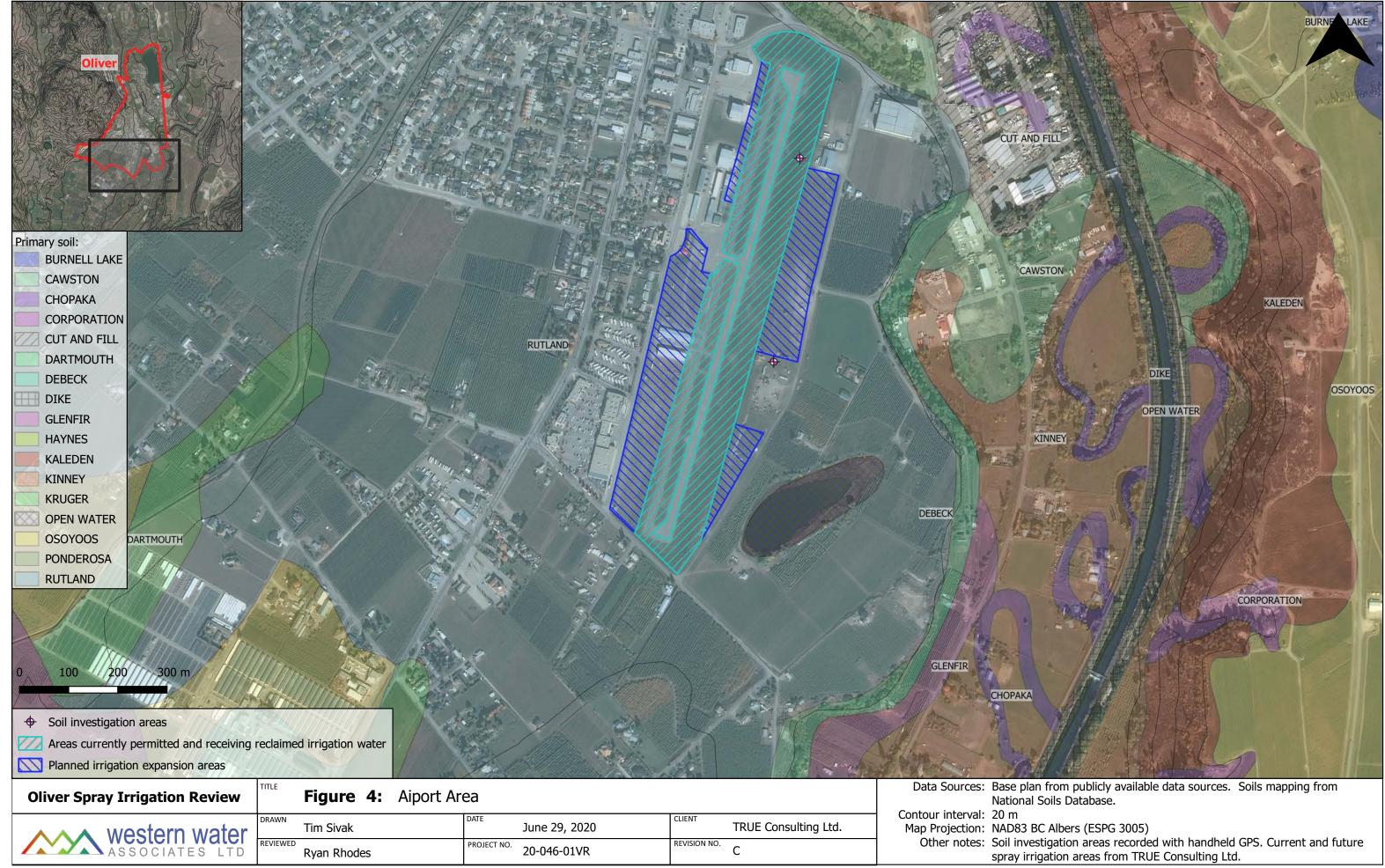


Oliver Oliver <th></th> <th></th> <th>SKAHA HAYNES DEBECK OPEN WATER OPEN WATER CAVSTON DIKE CAVSTON CHOPAKA</th> <th></th>			SKAHA HAYNES DEBECK OPEN WATER OPEN WATER CAVSTON DIKE CAVSTON CHOPAKA	
Oliver Spray Irrigation Review	Figure 3: Oliver Co	ommunity Park & Area		Data Sources: Base plan f
	DRAWN	DATE June 29, 2020	CLIENT TRUE Consulting Ltd.	National So Contour interval: 20 m Map Projection: NAD83 BC
western water ASSOCIATES LTD	Ryan Rhodes	PROJECT NO. 20-046-01VR	REVISION NO. C	Other notes: Soil investig spray irriga



n from publicly available data sources. Soils mapping from Soils Database.

BC Albers (ESPG 3005) estigation areas recorded with handheld GPS. Current and future rigation areas from TRUE Consulting Ltd.



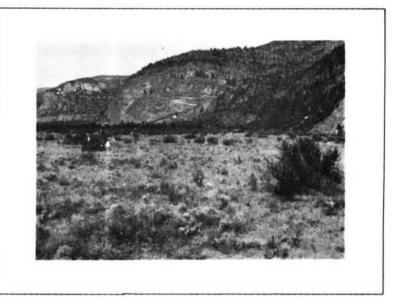
RUTLAND SOILS (R)

GENERAL COMMENTS

Rutland soils occupy significant areas throughout the Okanagan Valley portion of the map area and also near Keremeos in the Similkameen Valley. Topography is usually level to gently sloping although some terrace scarps are extremely sloping. Soils commonly associated with Rutland soils include Faulder, Dartmouth, Keremos, Oyama and Skaha.

The parent material of Rutland soils is a moderately coarse textured veneer between 10 and 25 cm thick which overlies gravelly and stony, very coarse textured glaciofluvial deposits. Surface soil textures are dominantly sandy loam or loamy sand while subsurface and subsoil textures are gravelly sand or gravelly loamy sand. Stones and cobbles are also common. Rutland soils are classifed as Orthic Dark Brown. They are rapidly drained, rapidly pervious, have slow surface runoff and low water holding capacity.

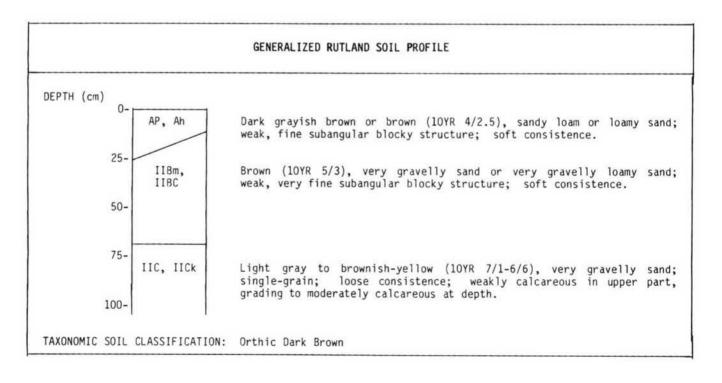
The main agricultural limitations are gravelly and stony textures, rapid permea-

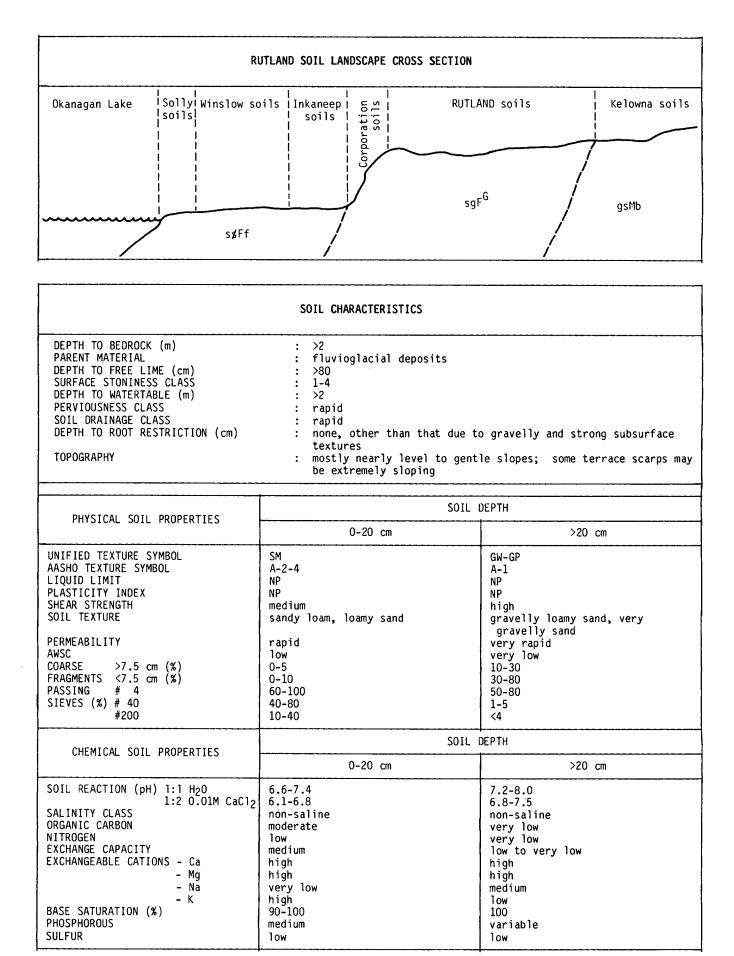


A very gently sloping area of undeveloped Rutland soils northeast of Oliver.

bility and low water holding capacity. Tree fruits and grapes are presently grown in most cultivated and irrigated areas. Typical native vegetation consists of a variety of grasses, sagebrush, rabbitbrush and scattered Ponderosa pine.

Rutland soils are well suited for urban and related uses. They are rapidly drained, have high bearing capacity and generally level topography. The depth of topsoil is shallow. Effluent from septic field installations may be incompletely filtered by the very gravelly, coarse-textured subsoil.





KINNEY SOILS (KY)

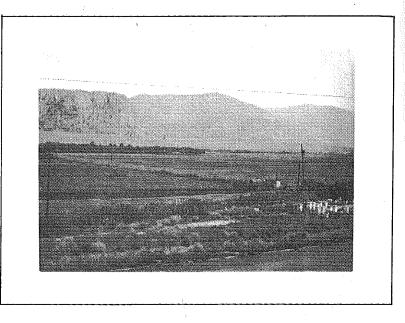
GENERAL COMMENTS

Kinney soils occur on the Okanagan River floodplain between Penticton and Osoyoos Lake. They occupy the slightly higher-lying, nearly level to very gently slopes in association with Chopaka, Cawston and Strutt soils.

Kinney soils have developed in a loamy fluvial veneer, usually between 30 and 80 cm thick, that overlies sandy floodplain deposits. Surface and subsurface textures are sandy loam or loam; the subsoil is loamy sand or sand and sometimes contains thin silty lenses. These Gleyed Regosol soils are imperfectly drained, moderately pervious and have moderate to low water holding capacity. Periodic water tables fluctuate with the level of the Okanagan River.

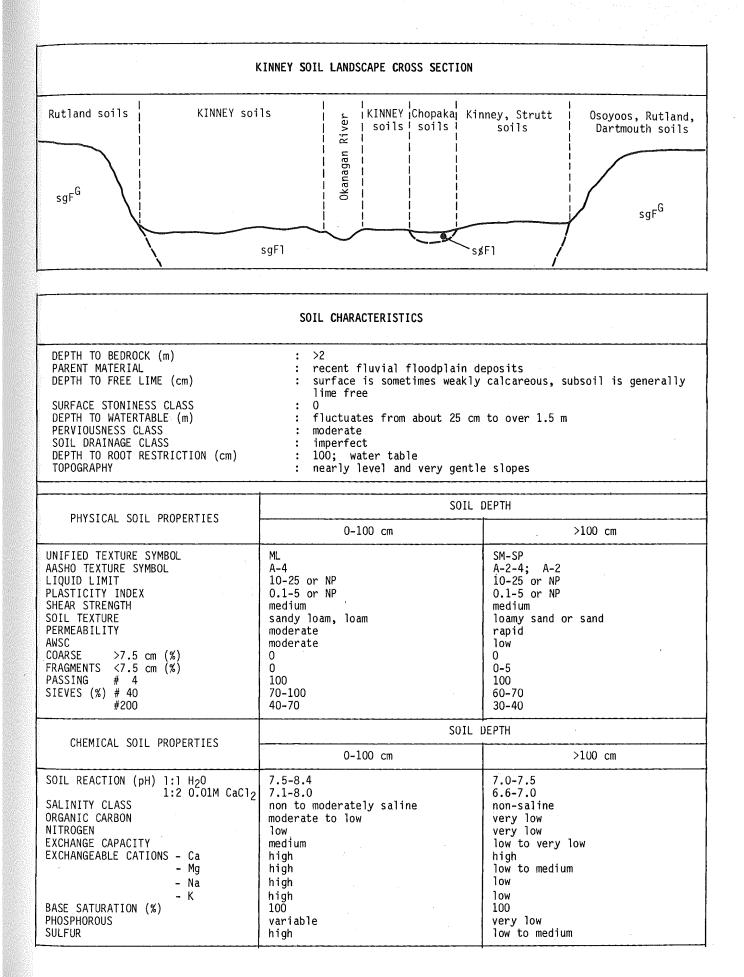
The main agricultural limitations of Kinney soils are moderately high water tables in late spring and in some areas, moderate salinity in the surface and potential for flooding. Cultivated areas are used for pasture and hay production. Natural vegetation occurs in a few areas and consists of black cottonwood, aspen, willow and scattered Ponderosa pine on slightly elevated dryer sites.

Urban uses of Kinney soils are restricted by periodic high water tables and potential for flooding.



Kinney soils occupy the higher areas on the gently undulating central portion of the photo.

GENERALIZED KINNEY SOIL PROFILE			
DEPTH (cm)			
0-	Ap,AC	Dark gray or gray (10YR 4.5/1.5), loam or sandy loam; moderate to strong, fine, pseudo-platy structure breaking to moderate to strong, very fine, angular blocky peds; slightly hard consistence; lower part weakly calcareous; sometimes slightly to moderately saline.	
50-	Cgj	Pale brown (10YR 6/3), sandy loam; massive, breaking to moderate to	
75-		strong, medium, angular blocky peds; slightly hard to hard consis- tence; common, fine, distinct, brownish-yellow (10YR 6/6) mottles.	
100-	IICg	Light gray (10YR 6/1), loamy sand or sand; very weak, very fine, sub- angular blocky structure; very friable consistence; many, medium, distinct, strong brown (7.5YR 5/6) mottles.	
TAXONOMIC SOIL	CLASSIFICATION:	Gleyed Regosol	



CAWSTON SOILS (CA)

GENERAL COMMENTS

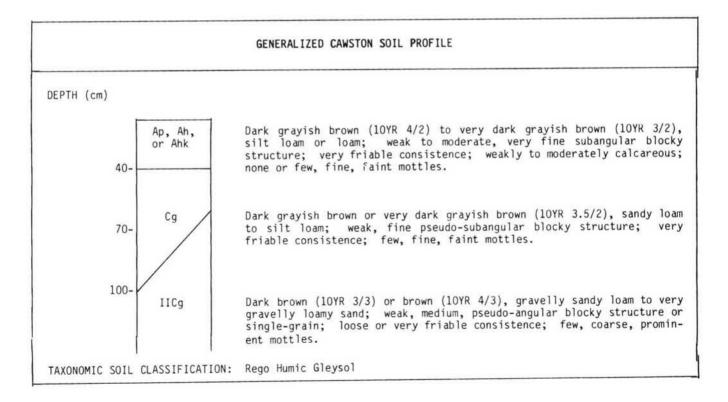
Cawston soils occur on the floodplain of the Similkameen River near Keremeos and Cawston and on the Okanagan River floodplain between Osoyoos Lake and Penticton. These Rego Humic Gleysol soils occupy slightly depressional to very gently sloping lower fluvial terraces, usually in association with Kinney, Chopaka, Gillanders and Keremeos soils.

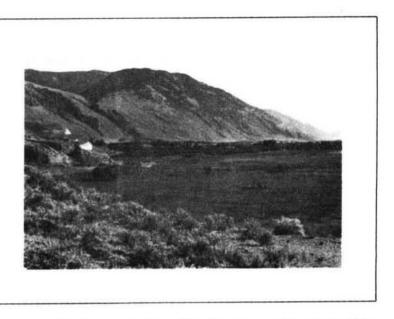
Cawston soils have developed in medium textured recent fluvial deposits generally between 50 and 100 cm thick overlying moderately coarse textured materials. Surface and subsurface textures are silt loam or loam. Subsoil texture are usually gravelly sandy loam or gravelly loamy sand. The soils are poorly to imperfectly drained. They are moderately pervious, have a high water holding capacity and slow surface runoff.

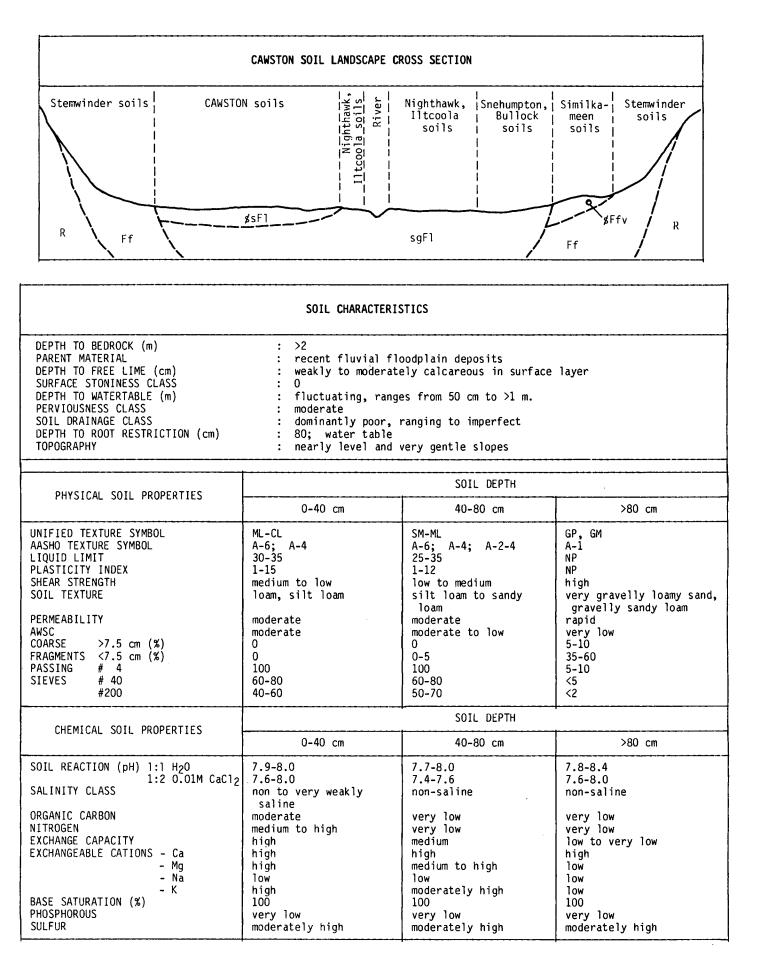
Cawston soils are suited for most agricultural crops, particularly if artificial drainage is installed. Most areas are now cleared and cultivated. The more poorly Cawston soils in association with Chopaka and Keremeos soils occupy the gently undulating middle portion of the photo.

drained areas are mostly used for forage production while the somewhat higher-lying, imperfectly drained areas are used for tree fruits, forages and vegetables. The few, uncleared areas support grasses, cattails, reeds and black cottonwood.

Cawston soils are constrained for urban and similar uses by moderately high water tables which impede basement and other excavations and restrict the operation of septic tank disposal fields.







PONDEROSA SOILS (PO)

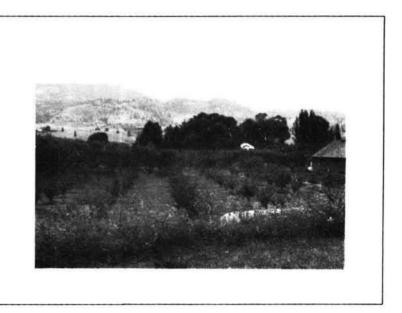
GENERAL COMMENTS

Ponderosa soils occur only in the vicinity of Oliver. They occupy nearly level to moderately sloping areas in association with Rutland, Glenfir, Ratnip and Burnell Lake soils.

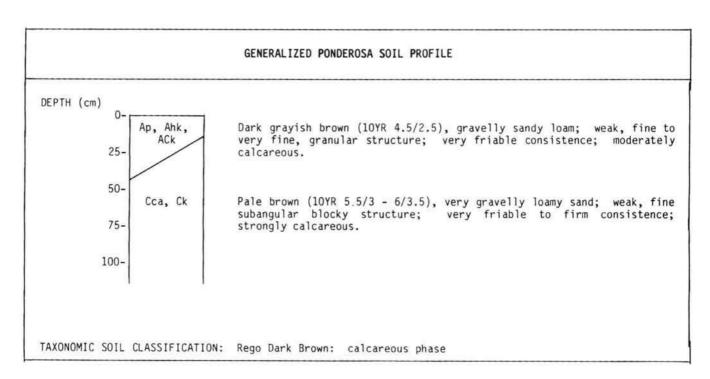
Ponderosa soils have developed in a gravelly, moderately coarse textured fluvial veneer between 10 and 50 cm thick, overlying gravelly coarse textured fluvial fan deposits. Surface and subsurface textures are gravelly or very gravelly sandy loam or gravelly loam; subsoils are very gravelly loamy sand. These Rego Dark Brown: calcareous phase soils are well to rapidly drained, rapidly pervious and have low water holding capacity.

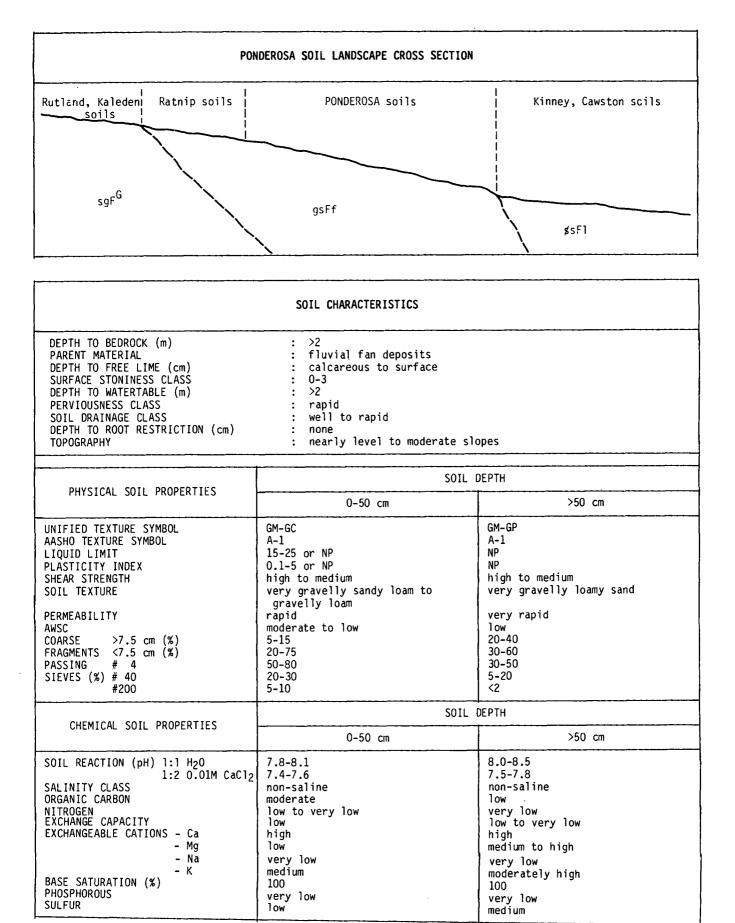
Almost all areas of Ponderosa soils are cleared, cultivated and planted to tree fruits and vineyards. Small, scattered, uncleared areas located on steep slopes support scattered Ponderosa pine, sagebrush and grass in the understory.

Except for a few steeply sloping areas, Ponderosa soils are moderately well suited for most urban and related uses. Incomplete septic tank effluent filtration may occur in the coarse-textured subsoils.



A typical view of moderately sloping Ponderosa soils near Oliver.





APPENDIX K

2019 Oliver Sanitary Sewer System Contingency Plan

Sanitary Sewer System Contingency Plans

Town of Oliver









April 2020 Project No. 306-089



ENGINEERING ■ PLANNING ■ URBAN DESIGN ■ LAND SURVEYING

Distribution List

# of Hard Copies	PDF Required	Association / Company Name
	1	Ministry of Environment
2	1	Town of Oliver
1	1	TRUE Consulting

Revision Log

Revision #	Revised by	Date	Issue / Revision Description

Report Submission

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Vatalie alter

Natalie Alteen, E.I.T. Project Engineer

Report Reviewed By:



Steve Underwood, P. Eng. Project Engineer

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Appendix A – Operation Certificate PE 13717



i

Executive Summary

Enclosed herein are Contingency Plans for system works associated with the Town of Oliver's Sanitary Sewer Treatment System operated under Operational Certificate PE 13717. Per Section 3.7 of the Operational Certificate. This plan addresses the appropriate course of action to be taken in any particular preconceived emergency situation. This plan includes chlorine leaks and any potential point of concern to the collection, treatment and disposal systems.

Attention is given to public safety and the protection of the environment. This plan should be continually updated to reflect the most current operation. Revisions to the Contingency Plan are to be forwarded to the Regional Waste Manager.

This document has been prepared by the Town of Oliver's Operations Department and TRUE Consulting.

ii.

1.0 Berm or Dam Failure at the Wastewater Treatment Plant

In the event of a berm or dam failure at the wastewater treatment plant, the following contingency plan is to be put into action.

At the time that a berm or dam failure at the wastewater treatment plant is discovered, the following procedures will be followed:

- 1. Assess the extent of the damage, leak or failure.
- 2. Do not disturb any physical evidence that may exist.
- 3. Arrange for any temporary measures that may be required such as supporting, ditching, damming, etc.
- 4. Notify the Director of Operations.
- 5. Notify the RCMP if the damage is the result of accident, vandalism or criminal activity.
- 6. Summon a qualified Geo-Technical Engineer to review the design drawings and provide recommendations.
- 7. Notify the CAO, Mayor, and Council.
- 8. Notify the appropriate insurance company for the Town (ie. liability or boiler and machinery insurance).

- Is there any immediate down slope risk to life or property? If so, notify the effected parties immediately.
- Given the location of the leak, does the O & M Manual refer to any alternate operating modes that will minimize the leak or risk of total failure? (ie. Lowering the level in the aeration cells.) If so, follow the instructions in the O & M Manual carefully.



2.0 Blower Failure at Aerated Lagoons

In the event of a blower failure, the following contingency plan is to be put into action.

At the time that a blower failure at the aerated lagoons is discovered, the following procedures will be followed:

- 1. Refer to O & M Manual.
- 2. Assess whether or not the blower(s) can be restarted.
- 3. Summon Sewer Operators as required.
- 4. Take dissolved oxygen (DO) readings in the aeration cells. Begin to monitor and record any reduction in the DO readings.

- Consider how many units are operating or failed vs. how many are required to maintain the DO. ie. Is there standby capacity available? Are any of the blowers operable?
- Assess the DO readings and evaluate how long it may take before degradation of the effluent quality may be noted. Seek professional assistance with this if required.
- Assess whether or not the blower unit or motor will require work at an off-site repair shop. If so, make necessary arrangements to confirm that those repair shops will provide an expedited emergency level of service. eg. AC Motor Electric or Mearl's Machine.
- Does it appear that the failure will cause degradation of the effluent quality? If so, take the following steps:
 - Consider how a temporary aerating system can be devised using gas powered compressors and PVC pipe.
 - Notify the Ministry of Environment.

3.0 Chlorine Leak

In the event of a chlorine leak, the following contingency plan is to be put into action.

At the time that a chlorine leak is discovered, the following procedures will be followed:

- 1. Notify their Supervisor (Director of Operations) and/or the Public Works Office by the fastest means possible. The Director of Operations will then notify the CAO and Mayor and Council.
- 2. The employee who has received training in the emergency and handling procedures of chlorine will take charge of the situation until such time that a more trained and qualified person arrives at the scene who may then take charge.

The person taking charge will:

- 1. Stay calm and assess the situation.
- 2. Establish 2-way communication between the scene and the Public Works office via cell phone or 2-way radio. If a municipal 2-way radio is not at the scene, request the Public Works office to have one sent to the scene immediately. If there is no one available at the Public Works office, contact the Municipal Hall.
- 3. Direct the Public Works Clerk to stay at the radio and the phone until the emergency is over.
- 4. Based on the training of the person in charge and his assessment of the emergency, he will instruct the Public Works Clerk to summon the people and agencies listed below as required by the severity of the situation. The phone numbers of these people have been posted beside the radio base station at the Municipal Hall and the base station at the Fire Hall.
- 5. Evacuate the lower areas and down wind of the chlorine leak.
- 6. Erect barricades to roadways surrounding the chlorine leak, lower areas and down wind of the chlorine leak.

AGENCIES THAT WILL ASSIST IN A CHLORINE EMERGENCY

c)	Provincial Emergency Program*	1-800-663-3456
b)	Police and ambulance	911 or 250-498-3422
a)	Oliver Fire Department	911

- d) Brenntag Canada Inc. Emergency # 1-604-685-5036 (24/7)
- e) Transport Canada Emergency # 1-613-996-6666

*Provincial Emergency Program must be notified

NOTE: SCBA's are maintained by the Oliver Fire Department and available at all times when responding to an emergency situation.



4.0 Effluent Forcemain Leak

In the event of an effluent force main leak the following contingency plan will be put into action.

At the time that an effluent force main leak is discovered, the following procedures will be followed:

- 1. Turn off and lock out all pumps in the High Lift Pump Station.
- 2. Isolate main line valves, where appropriate.
- 3. Assess whether or not the failure has resulted in any damage to the environment or property damage. If so, make the necessary arrangements to minimize the damage.
- 4. Barricade any unsafe areas.
- 5. Refer to the O & M Manual for more information.
- 6. Summon Public Works staff and contractors to make repairs.
- 7. Assess how long the repair time will be and whether or not there is sufficient standby storage capacity in the equalization basin and abandoned concrete holding cells.

- Is traffic control required?
- Has the break occurred within a Provincial road? If so, notify the Ministry of Highways or Highway Maintenance Contractor.
- Has there been damage to the environment? If so, contact the following:
 - Director of Operations.
 - Provincial Emergency Program.
 - Regional Waste Manager.
- Is the available standby storage capacity sufficient to accept the influent flow for the duration of the pipeline repair? If not, consider the following:
 - Will it be necessary to notify the public requesting them to minimize discharge into the sewer system?
 - Will hydro vac tank trucks be required? If so, make standby arrangements.
 - Will arrangements be necessary with neighboring municipalities to accept sewage transported by truck?

4.1 Reclaimed Effluent Forcemain Conversion to Effluent Forcemain

If the storage capacity is not sufficient and the repair will take an extended period of time. The reclaimed effluent forcemain can be used to bypass the break. The following is the start up procedure:

1. Close reclaimed water service valves at:

<u>Check Box</u>

- 1.1 Public Works Yard
- 1.2 Airport Irrigation
- 1.3 Oliver Secondary
- 1.4 Oliver Cemetery
- 1.5 Alonso Vineyard
- 1.6 Fairview Golf Course
- Open normally closed valve in street adjacent to the High Lift Station and close corresponding normally open valve. Valves show on TRUE record drawing 306-961-14 (Detail C).
- 3. Open PRV bypass valve and close PRV isolation valve at Fairview Park. Valve shown on TRUE record drawings 306-961-17 and 306-961-16.
- 4. Open normally closed interconnect valve at Topping lake access and close corresponding normally open valve. Valve shown on TRUE record drawing 306-961-01 (Detail A).
- 5. Restart High Lift Station. Monitor discharge pressure. Note: Flow rate will be reduced. The station will need to run outside of normal operation hours.
- 6. When repair is complete, reverse the above valve sequence. Rinse line with treated effluent through blow-off at High Lift to Equalization Basins. Re-open reclaimed water service supplies.



5.0 Extended Power Outage (Over ½ Hour)

In the event of an extended power outage over $\frac{1}{2}$ hour, the following contingency plan is to be put into action.

- At the time that an extended power outage is discovered, the following procedures will be followed:
- 1. Attempt to contact Fortis at 1-866-436-7847, to find out if they have been advised how long the outage will be?
- 2. Evaluate how the outage may impact the operation of all components of the Sanitary Sewer System.
- 3. Check to see if generator is operating in Sewer Treatment Plant.

- Will it be necessary to take action to prevent property damage or damage to the environment? If so, review the emergency procedure for that particular component of the system.
- Use generator for lift stations, start Rockcliffe and then check the rest of the lift stations.
- Will hydro vac tank trucks be required? If so, make standby arrangements.
- Will arrangements be necessary with neighboring municipalities to accept sewage transported by truck?
- The stationary generator located in the Sewer Treatment Plant (STP) building will
 power the STP, sewer screen, washer compactor, lights, and the influent lift station in
 the event of a power outage.

6.0 Influent Lift Station Failure

In the event of an influent lift station failure, the following contingency plan is to be put into action.

At the time that the influent lift station failure is discovered, the following procedures will be followed:

- 1. Check to see if the back-up generator is operating.
- 2. Assess whether or not the failure has resulted in any damage to the environment or property damage. If so, make the necessary arrangements to minimize the damage.
- 3. Assess the cause of the failure. Is it electrical or mechanical in nature?
- 4. Assess whether or not there is any information in the O & M Manual that would provide any insight into the problem.
- 5. Assess whether or not the station can be restarted.
- 6. Summon Public Works staff, Electrical Contractor and /or power utility for assistance as required.

Considerations:

- Is the failure due to loss of power from the power utility? If so, is the standby generator operating?
- Will it be necessary to notify the public requesting them to minimize discharge into the sewer system?
- Will hydro vac tank trucks be required? If so, make standby arrangements.
- Will arrangements be necessary with neighboring municipalities to accept sewage transported by truck?

Note: Electric Motor & Pump Service in Kelowna maintains a broad inventory of Flygt Pumps for emergency purposes (1-888-837-3677).



Neighbourhood Lift Station Pump Failure 7.0

In the event of a neighborhood lift pump station failure, the following contingency plan is to be put into action.

At the time that a neighborhood lift pump station failure is discovered, the following procedures will be followed:

- 1. If no power contact another Operator and get standby generator on site.
- 2. Assess whether or not the failure has resulted in any damage to the environment or property. If so, make the necessary arrangements to minimize the damage.
- Assess the cause of the failure. Is it electrical or mechanical in nature?
- 4. Assess whether or not there is any information in the O & M Manual that would provide any insight into the problem.
- 5. Assess whether or not the station can be restarted.
- 6. Summon Public Works staff and /or contractors or the power utility for assistance as required.

- Has there been any damage to the environment? If so, notify the Director of Operations and advise that the Provincial Emergency Program ("PEP") and the Ministry of Environment
- Has there been any property damage? If so, notify the Director of Operations (or alternate) to deal with potential liability issues.
- Is there power to the lift station? If not, is it a localized or an area wide outage? Who needs to be summoned to restore the power supply?
- Attempt to contact Fortis at 1-866-436-7847, to find out if they have been advised how long the outage will be?
- What is the rate of flow coming into the pump station?
- How much storage capacity can be utilized in the collection system before damage to the environment or property damage may result?
- As a temporary measure, should the water supply to the neighborhood be temporarily turned off in order to limit the amount of in-flow into the station?
- Will hydro vac trucks / tank trucks be required to haul sewage? If so, make the appropriate arrangements.

8.0 Reclaimed Water Supply Main Leak

In the event of a reclaimed water supply main leak, the following contingency plan is to be put into action.

At the time that a reclaimed water supply main leak is discovered, the following procedures will be followed:

- 1. Isolate the break.
- 2. Isolate the main line valves.
- 3. Barricade any unsafe areas.
- 4. Summon Public Works staff and / or contractors to make repairs.
- 5. Notify all large reclaimed irrigation customers if the break occurs during the irrigation season.

- Is traffic control required?
- Has the break occurred within a Provincial road? If so, notify the Ministry of Highways or Argo Road Maintenance.
- Is there property damage? If so, notify the Director of Operations or alternate.
- Will the break disrupt water supply to any fire hydrants beyond the end of the workday? If so, notify the Fire Department and the owners of any private fire hydrants so that they can notify their insurance company. ie. Fairview Mountain Golf Course and South Okanagan Secondary School (SOSS).



9.0 Major Gravity Main Collapse

In the event of a collapse or a major joint separation, the following contingency plan is to be put into action.

At the time that an effluent force main leak is discovered, the following procedures will be followed:

- 1. Summon Public Works staff to access the situation and turn plug affected main.
- 2. Summon a hydro vac truck to remove buildup of sanitary flow before the plugged affected area.
- 3. Assess whether or not the failure has resulted in any damage to the environment or property damage. If so, make the necessary arrangements to minimize the damage.
- 4. Barricade any unsafe areas.
- 5. Assess how to set up by-pass pumping into the next manhole down the main flow that is damaged.
- 6. Summon Public Works staff and contractors to make repairs.

- Is traffic control required?
- Has the break occurred within a Provincial road? If so, notify the Ministry of Highways or Argo Road Maintenance.
- Has there been damage to the environment? If so, contact the following:
 - Director of Operations.
 - Provincial Emergency Program.
 - Regional Waste Manager.



10.0 High Lift Station Electrical Fire

In the event of a collapse or a major joint separation, the following contingency plan is to be put into action.

At the time that the High Lift Station Electrical Fire is discovered, the following procedures will be followed:

- 1. Summon the power utility to disconnect the power and summon the Fire Department to extinguish the fire.
- 2. If the power is disconnected then the fire can be extinguished.
- 3. Assess whether or not the electrical fire has resulted in any damage to the environment or property damage. If so, make the necessary arrangements to minimize the damage.
- 4. Summon an electrical contractor to assess the cause of the electrical fire and to repair the High lift Station.
- 5. Assess whether or not there is any information in the O & M Manual that would provide any insight into the problem.
- 6. Assess whether or not the station can be restarted.
- 7. Summon Public Works staff and/or contractors or the power utility for assistance as required.

- Has there been any damage to the environment? If so, notify the Director of Operations and advise that the Provincial Emergency Program ("PEP") and the Ministry of Environment
- Has there been any property damage? If so, notify the Director of Operations (or alternate) to deal with potential liability issues.
- Is there power to the lift station? If not, is it a localized or an area wide outage? Who needs to be summoned to restore the power supply?
- What is the rate of flow coming into the pump station?
- How much storage capacity can be utilized in the collection system before damage to the environment or property may result?
- As a temporary measure, should the water supply to the neighborhoods be temporarily turned off in order to limit the amount of in-flow into the station?
- Will hydro vac trucks / tank trucks be required to haul sewage? If so, make the appropriate arrangements.
- Will arrangements be necessary with neighboring municipalities to accept sewage transported by truck?



11.0 Influent Screen Failure

In the event of an Influent Screen Failure at the wastewater treatment plant, the following contingency plan is to be put into action.

At the time that the Influent Screen Failure at the wastewater treatment plant is discovered, the following procedures will be followed:

- 1. Summon Public Works to switch the Influent Screen to the back-up Drum Screen.
- 2. Check to see if the back-up generator is operating.
- 3. If both screens happen to be broken, a 6" self-priming pump would be required outside the Main Influent Lift Station in the manhole outside, upstream and bypass the Main Influent Station and pumped directly into the Equalization Basin #1.
- 4. Assess whether the Influent Screens can be repaired and schedule a trash bin to be emptied every two (2) weeks as a minimum.
- 5. Assess whether or not there is any information in the O & M Manual that would provide any insight into the problem.
- 6. Flushing device will clean screens, ensure after screen replacement that the flushing device is operational
- 7. Summon Public Works staff and contractors to make repairs.

- Has there been any damage to the environment? If so, notify the Director of Operations and advise that the Provincial Emergency Program ("PEP") and the Ministry of Environment
- Has there been any property damage? If so, notify the Director of Operations (or alternate) to deal with potential liability issues.
- Is there power to the Influent Screen? If not, is it a localized or an area wide outage? Who needs to be summoned to restore the power supply?
- What is the rate of flow coming into the Wastewater Treatment Plant?
- How much storage capacity can be utilized in the collection system before damage to the environment or property damage may result?



12.0 Contact Pond Failure

In the event of a Contact Pond Failure at Topping Lake, the following contingency plan is to be put into action.

At the time that the Contact Pond Failure at Topping Lake is discovered, the following procedures will be followed:

- 1. Assess the extent of the damage, leak or failure.
- 2. Do not disturb any physical evidence that may exist.
- 3. Arrange for any temporary measures that may be required such as supporting, ditching, damming, etc.
- 4. Notify the Director of Operations.
- 5. Notify the RCMP if the damage is the result of accident, vandalism or criminal activity.
- 6. Summon a qualified Geo-Technical Engineer to review the design drawings and provide recommendations.
- 7. Notify the CAO, Mayor, and Council.
- 8. Notify the appropriate insurance company for the Town (ie. liability or boiler and machinery insurance).

- Is there any immediate down slope risk to life or property? If so, notify the effected parties immediately.
- Given the location of the leak, does the O & M Manual refer to any alternate operating modes that will minimize the leak or risk of total failure? (ie. Lowering the level in the Contact Ponds.) If so, follow the instructions in the O & M Manual carefully.

13.0 Topping Lake Aeration Building Failure

In the event of Topping Lake Pump House Failure, the following contingency plan is to be put into action.

At the time Topping Lake Pump House Failure at Topping Lake is discovered, the following procedures will be followed:

- 1. Assess whether or not the failure has resulted in any damage to the environment or property damage. If so, make the necessary arrangements to minimize the damage.
- 2. Assess the cause of the failure. Is it electrical or mechanical in nature?
- 3. Assess whether or not there is any information in the O & M Manual that would provide any insight into the problem.
- 4. Assess whether or not the blower(s) can be restarted.
- 5. Take dissolved oxygen (DO) readings in the aeration cells. Begin to monitor and record any reduction in the DO readings.
- 6. Assess whether or not the station can be restarted.
- 7. Summon Public Works staff, electrical contractor and/or power utility for assistance as required.

Considerations:

- Is the failure due to loss of power from the power utility?
- Will it be necessary to notify the public requesting them to minimize discharge into the sewer system?
- Will hydro vac trucks / tank trucks be required? If so, make standby arrangements.
- Will arrangements be necessary with neighboring municipalities to accept sewage transported by truck?

Note: Electric Motor & Pump Service in Kelowna maintains a broad inventory of Flygt Pumps for emergency purposes (1-888-837-3677).



14.0 High Lift Diversion Structure Failure

In the event of the Diversion Structure Failure, the following contingency plan is to be put into action.

At the time of the Diversion Structure Failure at wastewater treatment plant is discovered, the following procedures will be followed:

- 1. Assess the extent of the damage, leak, collapse or failure.
- 2. Do not disturb any physical evidence that may exist.
- 3. Arrange for any temporary measures that may be required such as supporting, damming, or by-pass pumping, etc.
- 4. Notify the Director of Operations.
- 5. Notify the RCMP if the damage is the result of accident, vandalism or criminal activity.
- 6. Summon a qualified Geo-Technical Engineer to review the design drawings and provide recommendations.
- 7. Notify the CAO, Mayor, and Council.
- 8. Notify the appropriate insurance company for the Town (ie. liability or boiler and machinery insurance).

- Does the O & M Manual refer to any alternate operating modes that will minimize the leak or risk of total failure? (ie. Bypass pumping into the Equalization Basins.) If so, follow the instructions in the O & M Manual carefully.
- Will it be necessary to notify the public requesting them to minimize discharge into the sewer system?
- Will hydro vac trucks / tank trucks be required? If so, make standby arrangements.
- Will arrangements be necessary with neighboring municipalities to accept sewage transported by truck?



15.0 Equalization Basins Failure

In the event of an Equalization Basin Failure at wastewater treatment plant, the following contingency plan is to be put into action.

At the time that the Equalization Basin Failure at wastewater treatment plant is discovered, the following procedures will be followed:

- 1. Assess the extent of the damage, leak or failure.
- 2. Do not disturb any physical evidence that may exist.
- 3. Arrange for any temporary measures that may be required such as supporting, ditching, damming, etc.
- 4. Assess whether or not the failure has resulted in any damage to the environment or property damage. If so, make the necessary arrangements to minimize the damage.
- 5. Notify the Director of Operations.
- 6. Notify the RCMP if the damage is the result of accident, vandalism or criminal activity.
- 7. Summon a qualified Geo-Technical Engineer to review the design drawings and provide recommendations.
- 8. Notify the CAO, Mayor, and Council.
- 9. Notify the appropriate insurance company for the Town (ie. liability or boiler and machinery insurance).
- 10. Assess how long the repair time will be and whether or not there is sufficient standby storage capacity in the equalization basin and abandoned concrete cells.

- Is there any immediate down slope risk to life or property? If so, notify the effected parties immediately.
- Given the location of the leak, does the O & M Manual refer to any alternate operating modes that will minimize the leak or risk of total failure? (ie. Lowering the level in the Equalization Basins.) If so, follow the instructions in the O & M Manual carefully.
- Has there been damage to the environment? If so, contact the following:
 - Director of Operations.
 - Provincial Emergency Program.
 - Regional Waste Manager.
- Is the available standby storage capacity sufficient to accept the influent flow for the duration of the Equalization Basin repair? If not, consider the following:
 - Will it be necessary to notify the public requesting them to minimize discharge into the sewer system?
 - Will hydro vac trucks / tank trucks be required? If so, make standby arrangements.



• Will arrangements be necessary with neighboring municipalities to accept sewage transported by truck?



APPENDIX A

Operation Certificate PE 13717



Province of British Columbia

MINISTRY OF

ENVIRONMENT,

LANDS AND PARKS



Environmental Protection #201-3547 Skaha Lake Rd. Penticton, British Columbia V2A 7K2 Telephone: (604) 490-8200 Fax: (604) 492-1314

Date: December 14, 1995

File: 76750-40/PE-13717 (01)

REGISTERED MAIL

The Corporation of the Town of Oliver PO Box 638 Oliver BC VOH 1TO

Attention: Tom Szalay, Administrator

Enclosed is a copy of the Operational Certificate No. PE-13717 issued under the provisions of the Waste Management Act. This Operational Certificate supersedes Permit PE-00102 which is cancelled in accordance with Section 16(13) of the Waste Management Act. Your attention is respectfully directed to the terms and conditions outlined in the Operational Certificate. An annual Permit fee will be determined according to the Waste Management Permit Fee Regulation.

This Operational Certificate does not authorize entry upon, crossing over, or use for any purpose of private or Crown lands or works, unless and except as authorized by the owner of such lands or works. The responsibility for obtaining such authority shall rest with the Operational Certificate holder.

This Operational Certificate is issued pursuant to the provisions of the Waste Management Act to ensure compliance with Section 34(3) of that statute, which makes it an offence to discharge waste without proper authorization. It remains the responsibility of the Operational Certificate holder to ensure that all activities conducted under this authorization comply with any other applicable legislation which may be in force from time to time.

The administration of this Operational Certificate will be carried out by staff from our Regional Office located in Penticton, (telephone 490-8200). Plans, data and reports pertinent to the Operational Certificate are to be submitted to the Environmental Protection office, Suite 201, 3547 Skaha Lake Road, Penticton, British Columbia, V2A 7K2. - 30th Street, Vernon, British Columbia, V1T 9G3.

This decision may be appealed by any person(s) who considers themselves aggrieved by this decision, in accordance with Part 5 of the Waste Management Act. Written notice of intent to appeal must be received by the Regional Waste Manager within twenty-one (21) days of the date of notification of this decision.

Yours truly,

T.R. Forty, P.Eng. Assistant Regional Waste Manager Okanagan Sub-Region

Enclosure



Environmental Protection #201 - 3547 Skaha Lake Road Penticton British Columbia, V2A 7K2 Telephone: (604) 490-8200

MINISTRY OF ENVIRONMENT, LANDS AND PARKS

OPERATIONAL CERTIFICATE

PE 13717

Under the Provisions of the Waste Management Act

TOWN OF OLIVER

P.O. Box 638

Oliver, British Columbia

V0E 1T0

is authorized to discharge reclaimed wastewater to the ground by irrigation, from a municipal sewage collection and aerated lagoon sewage treatment facility located at Oliver, British Columbia, subject to the conditions listed below. Contravention of any of these conditions is a violation of the Waste Management Act and may result in prosecution.

1. SPECIFIC AUTHORIZED DISCHARGES AND RELATED REQUIREMENTS

The discharge of effluent to which this sub-section is applicable is from a municipal sewage treatment facility located approximately as shown on the attached Site Plan A and Site Plan B. The reference number (S.E.A.M. site number) for this discharge is E222150.

1.1 Discharge Quantity

- 1.1.1 The maximum authorized rate of effluent to be discharged from the aerated lagoon sewage treatment system to the reclaimed wastewater storage reservoir, averaged on a monthly basis:
 - 1995 1950 m³ per day 1996 - 2000 m³ per day 1997 - 2050 m³ per day 1998 - 2100 m³ per day 1999 - 2150 m³ per day 2000 - 2200 m³ per day

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OPERATIONAL CERTIFICATE NO.: PE 13717

1.1.2 There is no maximum authorized rate of reclaimed wastewater to be discharged from the storage reservoir for beneficial use as irrigation water.

1.2 Discharge Quality

1.2.1 It is recommended that to ensure reclaimed wastewater is adequately renovated prior to irrigation, the characteristics of the effluent discharged from the aerated lagoon treatment system to the reclaimed wastewater storage reservoir not exceed:

5 Day Biochemical Oxygen Demand, 45 mg/L; and

Total Suspended Solids - 60 mg/L.

1.3 Permit Fee Calculations for Reclaimed Wastewater Discharge to Land

1.3.1 The characteristics of the reclaimed wastewater discharged from the storage reservoir and beneficially used for irrigation, for the purposes of permit fee calculations, the following discharge factors have been assumed:

5 Day Biochemical Oxygen Demand, 10 mg/L; and

Total Suspended Solids - 10 mg/L.

1.4 Authorized Works

The works authorized are: sewage collection system, sewage treatment plant concrete tankage for emergency containment, influent screen, flow equalization basin, pumping station, pressure forcemain to aerated lagoons, aerated lagoon treatment system, reclaimed wastewater storage reservoir sized to provide a minimum retention time of 60 days prior to spray irrigation, post storage chlorination, pressure forcemain to the golf course and related irrigation supply mains and sprinkler irrigation equipment, infiltration basin, and other related appurtenances, approximately as shown on the attached Site Plan A.

1.5 Source of Discharge

The source of discharge and sewage collection system services the Town of Oliver and surrounding area.

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1.6 Location of Works

The location of the sewage collection, flow equalization basin and effluent pumping station is: Block 47 of District Lot 2450s, Similkameen Division of Yale District.

The location of the effluent aerated lagoon treatment facilities, reclaimed wastewater storage reservoir, chlorination and withdrawal facilities is: District Lot 763s, and Block B, District Lot 682s, Similkameen Division of Yale District. The location of the potential infiltration basin sites: Block K, Plan 1789 (Town Sand Pit) and Lot 2, Plan 5881 (Town Gravel Pit).

1.7 Location of Discharge

The location where reclaimed wastewater may be irrigated is described generally as Oliver and the surrounding area.

1.8 Irrigation Plan

Submit for review, and obtain written authorization from the Regional Waste Manager, an "Irrigation Plan" of all new areas of land to be irrigated prior to commencement of irrigation with reclaimed wastewater. Areas for effluent irrigation are as indicated in the Oliver Waste Management Plan and as indicated on Site Plan A.

2. <u>GENERAL REQUIREMENTS</u>

2.1 Maintenance of Works, Emergency Procedures and Noncompliance Reporting

Inspect the pollution control works regularly and maintain them in good working order. In the event of an emergency or any condition which prevents continuing operation of the approved method of pollution control or results in noncompliance with the terms and conditions of this Operational Certificate, immediately notify the Regional Waste Manager and take appropriate remedial action.

2.2 Bypasses

The discharge of effluent which has bypassed the designated treatment works is prohibited, unless the consent of the Regional Waste Manager is obtained and confirmed in writing.

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2.3 **Process Modifications**

Notify the Regional Waste Manager, and his written consent obtained, prior to implementing changes to any process that may affect the quality and/or quantity of the discharge.

2.4 Alternate Water Supply

Provide alternate water supplies if any privately owned well is adversely affected by the land disposal scheme as determined by the Regional Waste Manager.

2.5 Plans - New Works

- 2.5.1 Plans of modifications and/or extensions to the existing works shall be signed and sealed by a Professional Engineer licensed to practise in the Province of British Columbia.
- 2.5.2 Copies of all "as-built" plans and drawings for the effluent treatment system, signed and sealed by a Professional Engineer licensed to practise in the Province of British Columbia, shall be submitted to the Regional Waste Manager on completion of construction.
- 2.5.3 Plans and specifications of any proposed new works, modifications or additions to the works authorized in this Operational Certificate, including the infiltration basin plans, and with the exception of the sewage collection system, shall be submitted to the Regional Waste Manager, and his written consent obtained before construction commences. The works shall be constructed in accordance with such plans.
- 2.5.4 Retain a copy of all "as-built", plans of modifications and/or extensions to the sewage collection system for perusal by the Regional Waste Manager, or his designate, upon request.
- 2.5.5 Plans for modifications of, and/or extensions to, the existing reclaimed wastewater irrigation system shall be approved by a person qualified in the design of irrigation systems.
- 2.5.6 Design and construct the irrigation works in accordance with best current agricultural practice and:

The "Pollution Control Guidelines for Municipal Effluent Application to Land", dated January 1983, and any amendments thereto, issued by the Ministry of Environment of British Columbia.

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The "B.C. Sprinkler Irrigation Manual" 1989 issue, prepared by the B.C. Ministry of Agriculture and Fisheries.

The "Health and Safety Criteria for the Use of Reclaimed Wastewater", 1991, developed by the Ministry of Health and the Ministry of Environment.

3. GENERAL REQUIREMENTS - ALL DISCHARGES

3.1 Operation and Maintenance

Develop and maintain both an Operational and Maintenance Manual for the sewage collection, sewage treatment and reclaimed wastewater utilization. A copy of the Operational and Maintenance Manuals shall be retained at the treatment facility for inspection by the Regional Waste Manager or their designate.

3.2 Facility Classification

Maintain the wastewater treatment facility classification as authorized in Section 1.4 with the "British Columbia Water and Wastewater Operators Certification Program Society" (BCWWOCPS). The new aerated lagoon treatment facility is presently classified as a Level II facility.

3.3 Operator Certification

- 3.3.1 All operators in training (OIT) working at this Level II facility classified by the BCWWOCPS shall be required to successfully pass an OIT examination within three (3) months of commencement of employment at the facility. The OIT certificate shall be valid for fifteen (15) months from the date of issue. Prior to the expiry date of the OIT certificate, but not sooner than twelve (12) months from the date when the OIT commenced facility operation, the OIT shall successfully complete a Class I certification examination in order to continue to operate at the facility.
- 3.3.2 The facility is currently classified by the BCWWOCPS at Level II. Designate at least one operator to be the "Chief Operator" of the facility by **December 1, 1996**. The "Chief Operator" shall be certified at a Class II level, at a minimum.

After December 1, 1996, no person shall have "Direct Responsible Charge", as defined by the BCWWOCPS, of a municipal wastewater

T.R. Forty, P.Eng Assistant Regional Waste Manager

Date issued: December 14, 1995 Amendment Date: (most recent) Page: 5 of 18 treatment facility classified at Level II or higher unless they possess a valid operator's certificate not more than one level below the classification level of the facility. "Direct Responsible Charge" is the "Chief Operator" of the facility, the identifiable senior person who is in charge of the plant.

- 3.3.3 Should the facility be reclassified by the BCWWOCPS at Level III, designate a "Chief Operator", certified at a Class III level by **December 1, 1998**.
- 3.3.4 Should the facility be reclassified by the BCWWOCPS at Level IV, designate a "Chief Operator", certified at a Class IV level by December 1, 1998.

3.4 Water Conservation

Establish a water conservation program to encourage a reduction in the volume of domestic and industrial wastewaters discharged to the sewage collection system.

3.5 Sewage Collection System - Groundwater Infiltration, Inflow and Cross Connections

Inspect and maintain the sewage collection system works so as to minimize the possibility of cross connections between the storm sewer and the sanitary sewer systems, to minimize infiltration of groundwater, to minimize inflow of water from basement sump pumps and roof drains, and minimize exfiltration of the collected sewage from the sewage collection system to the ground.

3.6 Influent Wastes Bylaw

Subject to being declared a Sewage Control Area under Section 17 of the Waste Management Act, and in order to minimize the potential effect of heavy metals or other toxic materials in the effluent and/or sludge, prepare, implement and/or amend an Influent Wastes Bylaw, Building Bylaw, or other similar bylaws, to regulate the input of such wastes to the sewage collection system. Devices to process household putrescible waste for disposal to the sewage collection system shall be prohibited.

3.7 Contingency Plan

Prepare a Contingency Plan that will address the appropriate course of action to be taken in any particular preconceived emergency situation. The Contingency Plan shall include chlorine leaks and any potential point of concern in the collection, treatment and disposal systems. Attention is to be given to public

T.R. Forty, P.Eng. Assistant Regional Waste Manager

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3.8 Sludge Management Plan

The rationale of sludge management, including frequency of withdrawal of sludge from the sewage treatment plant and the location(s) used for disposal and/or utilization shall be developed into a Sludge Management Plan. The Sludge Management Plan shall be prepared and submitted to the Regional Waste Manager for approval on or before December 31, 1996.

3.9 Odours

Should odours become objectionable, additional works shall be provided when so directed in writing by the Regional Waste Manager.

3.10 Fencing

Erect a fence around the sewage treatment facility, storage reservoir and such other areas as required by the Regional Waste Manager. The height and type of fencing shall meet the approval of the Regional Waste Manager.

3.11 Surface Water Diversionary Works

Surface water shall be intercepted and diverted away from the effluent treatment facilities to the greatest extent possible.

3.12 Signage

- 3.12.1 A suitable sign erected at the main entrance to the site shall have the appropriate emergency phone numbers for use by the general public and others.
- 3.12.2 Prominent "NO TRESPASSING", signs shall be erected around agricultural and silvicultural sites irrigated with reclaimed wastewater, warning persons of the possible health hazard during the irrigation season and advising that the water used for irrigation is NOT POTABLE. The wording shall be in language or symbols readily comprehensible by the general public. eg. "NO TRESPASSING - RECLAIMED WASTEWATER - DO NOT DRINK"

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4. <u>GENERAL REQUIREMENTS - EFFLUENT STORAGE RESERVOIR</u>

4.1 Leakage

Operate and maintain the reclaimed wastewater storage reservoir to minimize fluid leakage. Leakage shall not aggravate or produce soil or bedrock instability or erosion elsewhere or contaminate ground or surface water.

5. GENERAL REQUIREMENTS - EFFLUENT IRRIGATION

5.1 Disinfection - Chlorination

- 5.1.1 Adequate chlorination shall be maintained and provide not less than one hour's contact time at average flow rates in the reclaimed wastewater discharging from the chlorination facility to the irrigation system.
- 5.1.2 Reclaimed wastewater utilized for irrigation shall conform to the effluent irrigation guidelines developed by the B.C. Ministry of Health. Fecal coliforms shall not exceed 200 MPN per 100 mL for agricultural, silvicultural and low public use lands, or exceed 2.2 MPN per 100 mL for high public use lands.

5.2 Annual Irrigation

- 5.2.1 The authorized discharge period for irrigation is during the period March 15 to October 31, inclusive.
- 5.2.2 With the written authorization of the Regional Waste Manager, the irrigation schedule may be extended on a weekly basis beyond these limits. Any extension will be considered only upon receipt of a substantiated written request.

5.3 Buffer Zones

- 5.3.1 The requirement for formal buffer zones surrounding lands irrigated with reclaimed wastewater is no longer in effect, however, a buffer zone may be specified by the Regional Waste Manager.
- 5.3.2 Reclaimed wastewater applied by irrigation shall not be applied to the ground any closer than 15 metres from the edge of flowing streams or bodies of water.
- 5.3.3 There shall be no reclaimed wastewater irrigated within 30 metres of any well or inground reservoir for domestic supply.

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5.4 Surface Runoff

There shall be no surface runoff of irrigated reclaimed wastewater from the irrigated lands.

5.5 Surfacing Reclaimed Wastewater

Irrigation shall be managed in such a fashion as to preclude surfacing of irrigation tail water down slope of the point of irrigation.

5.6 Spray Irrigation Drift

The reclaimed wastewater irrigation system shall be managed in such a fashion as to preclude aerosol drift from leaving the irrigated lands.

5.7 Irrigation Rates

- 5.7.1 Irrigation rates shall not exceed the rates given in "B.C. Sprinkler Irrigation Manual", dated 1989, prepared by the B.C. Ministry of Agriculture and Fisheries.
- 5.7.2 Soils of the irrigated lands shall be monitored to prevent saturation, erosion, and instability.

5.8 Agricultural Products Lag Time

- 5.8.1 A three day lag time is required before uninspected livestock intended for human consumption are permitted on areas irrigated with reclaimed wastewater. No lag time is required if livestock are subjected to the federal meat inspection program.
- 5.8.2 A six day lag time is required before dairy cattle are permitted in areas irrigated with reclaimed wastewater.
- 5.8.3 A three day lag time, after irrigation has ceased, is required before a crop intended for animal feed is harvested.

T.R. Forty, P.Eng.

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6. MONITORING REQUIREMENTS

6.1 Influent Sampling Program - (Equalization Basin)

- 6.1.1 Install and maintain a suitable sampling facility at the equalization basin outlet, (S.E.A.M. site number E222152), and obtain a grab sample of the plant influent semi-annually (a proportional continuous sampler may be used).
- 6.1.2 Obtain analyses of the influent sample for the following:

total phosphorus and ortho phosphorus, expressed as P in mg/L;

6.2 Effluent Sampling Program - (Cell #3, prior to storage reservoir)

- 6.2.1 Install and maintain a suitable sampling facility on the outlet of the aerated treatment lagoon, Cell #3, (S.E.A.M. site number E222151), and obtain a grab sample of the effluent before it is discharged to the storage reservoir, for analysis by a suitably accredited laboratory, a proportional continuous sampler may be used, provided that prior written approval has been obtained from the Regional Waste Manager.
- 6.2.2 Obtain analyses of the effluent sample for the following:

total suspended solids (non-filterable residue), (monthly analysis), mg/L;

5-day biochemical oxygen demand, (monthly analysis), mg/L;

total phosphorus, ortho phosphorus and total dissolved phosphorus, (quarterly analysis during 1996, and semi-annually analysis, thereafter), all expressed as mg/L P; and

total nitrogen, ammonia nitrogen, nitrate nitrogen, nitrite nitrogen, and organic nitrogen, (quarterly analysis during 1996, and semiannually analysis thereafter), all expressed as mg/L N.

6.2.3 Occasional full chemical analysis of the main cations and anions and other characteristics may be required at the discretion of the Regional Waste Manager.

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6.3 Effluent Irrigation Sampling Program - (Chlorine Contact Chamber, prior to Irrigation)

- 6.3.1 Install a suitable sampling facility after the chlorine contact chamber, prior to irrigating, (S.E.A.M. site number E222150) and obtain a grab sample of the reclaimed wastewater during the irrigation season.
- 6.3.2 Obtain analyses of the sample, parameters and frequency as follows:

faecal coliforms, M.P.N./100ml, on a monthly basis;

total coliforms, M.P.N./100ml, on a monthly basis;

total phosphorus, mg/L, on a monthly basis;

total nitrogen, mg/L, on a monthly basis; and

chlorine residual, mg/L, on a weekly basis.

6.3.3 Occasional full chemical analysis of the main cations and anions and other characteristics may be required at the discretion of the Regional Waste Manager.

6.4 Effluent Irrigation Monitoring Program

- 6.4.1 Provide and maintain a suitable flow measuring device to measure total volume of reclaimed wastewater irrigated annually and record the areas where it is utilized.
- 6.4.2 Provide and maintain a suitable flow measuring device to measure the amount of fresh water make-up from Okanagan River to the equalization basin in m³/day, and totalize this make up water volume on an annual basis in m³/year.
- 6.4.3 Provide and maintain a suitable flow measuring device and record once per day the reclaimed wastewater volume irrigated over a 24-hour period. Record the flows for each calendar month and for each calendar year.

6.5 Storage Reservoir Level Monitoring Program

6.5.1 Provide a suitable staff gauge or other similar device as approved by the Regional Waste Manager in the storage reservoir and take weekly measurements of the water level in the storage reservoir on a year round basis.

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6.6 Sampling and Analytical Requirements

- 6.6.1 Proper care should be taken in sampling, storing and transporting the samples to adequately control temperature and avoid contamination, breakage, etc.
- 6.6.2 Occasional full chemical analysis of the main cations and anions and other characteristics may be required at the discretion of the Regional Waste Manager.
- 6.6.3 Analyses are to be carried out in accordance with procedures described in the second edition of "A Laboratory Manual for the Chemical Analysis of Waters, Wastewaters, Sediments and Biological Materials, (March 1994 Permittee Edition)", or by suitable alternative procedures as authorized by the Regional Waste Manager.

The above manual may be purchased from Queens Printer Publications Centre, 2nd Floor, 563 Superior Street, Victoria, B.C., V8V 4R6, 1-800-663-6105. The manual may also be reviewed at any Environmental Protection Program Office.

- 6.6.4 Sampling and flow measurement shall be carried out in accordance with the procedures described in "Field Criteria for Sampling Effluents and Receiving Waters", April 1989, 17 pp., or by other suitable alternative procedures as authorized by the Regional Waste Manager.
- 6.6.5 The Permittee is required to follow the terms and conditions of the <u>Quality Assurance Regulation</u> (EQDA). Ten percent of the samples collected shall be duplicated to provide data quality assurance. Quality control information generated by the Permittee lab while analyzing parameters required by this Permit shall also be provided with the data required to be reported.

6.7 Sludge Sampling and Monitoring Program

Develop and maintain a record keeping system for measuring and recording the depth of sludge collecting in the lagoons and volume of sludge removed from the treatment lagoons during desludging operations, the location where the sludge was discharged, and the amount of sludge discharged at each location. The Regional Waste Manager is to be notified in writing at least two weeks prior to the commencement of desludging operations. Analysis of the sludge may be required by the Regional Waste Manager.

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6.8 Groundwater Monitoring Program

A Groundwater Monitoring Program, shall be submitted to the Regional Waste Manager. The Groundwater Monitoring Program shall be designed by a Professional Engineer or a Hydrogeological Technologist licensed to practice in the Province of British Columbia, to establish with acceptable scientific accuracy, the groundwater flow pattern and nutrient removal capability of the soil to ensure reasonable notice of impending high phosphorus or nitrate levels that may adversely affect surface water, groundwater or domestic waterwells. The sampling, measurement frequency and analyses shall be conducted in accordance with the Groundwater Monitoring Program upon its written authorization by the Regional Waste Manager. The Groundwater Monitoring Program to be submitted to the Regional Waste Manager by December 31, 1997.

6.9 Soils Assessment Program

A ground assessment of any new areas to be irrigated, as shown in the "Irrigation Plan", shall be performed by a suitably qualified professional, using best current climate and soils data to substantiate that the land is capable of accepting reclaimed wastewater for irrigation purposes. This assessment is to include any suggested restrictions or recommendations that the suitably qualified professional deems necessary. This Soils Assessment shall be submitted to the Regional Waste Manager for review prior to the initial commencement of irrigation annually. Further review and ongoing soils assessments may be required by the Regional Waste Manager.

7. <u>REPORTING</u>

7.1 General Reporting

- 7.1.1 Maintain the monitoring data required in Section 6 for inspection.
- 7.1.2 The influent/effluent water quality analyses and flow data is to be submitted to the Regional Waste Manager such that they are received by the Regional Waste Manager within 30 days of the results being sent out by the testing agency.
- 7.1.3 Monitoring data shall be submitted in an electronic and/or printed format satisfactory to the Regional Waste Manager.

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7.2 Annual Reporting

- 7.2.1 Submit an Annual Report which includes a summary of the results of all sampling and monitoring programs as specified in this permit, data interpretation and trend analyses by a suitably qualified professional.
- 7.2.2 This report is to be in a format which is suitable for review by the public and/or other government agencies.
- 7.2.3 The first report is due on or before 60 days of the end of a calendar year for that year's monitoring. Raw data are to be attached as appendices to the report.
- 7.2.4 Maintain and submit records of the following as a part of the annual report:
 - 7.2.4.1 Records of reclaimed wastewater balance, that is, the flows to and from the storage reservoir. This balance, must also include the freshwater make-up.
 - 7.2.4.2 Records of the duration, intensity, property owner, acreage, location, and type of reclaimed wastewater irrigation.
 - 7.2.4.3 Records of efforts to reduce infiltration, inflow and cross connections for inspection by the Regional Waste Manager or his designate.
 - 7.2.4.4 Records of efforts to administer the Influent Wastes By-law(s) for inspection by the Regional Waste Manager or his designate. Include as an attachment, any amendments to the Influent Wastes By-law(s) that have been made during the past year.
 - 7.2.4.5 Copy of the Contingency Plan.
 - 7.2.4.6 Copy of the Sludge Management Plan.
 - 7.2.4.7 Copy of the Annual Flow Summaries.
 - 7.2.4.8 Copy of the Annual Irrigation Summaries.

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APPENDIX A

Requirements of Reclaimed Wastewater Users

The holder of this Operational Certificate (The reclaimed wastewater supplier) shall be responsible for ensuring that the contractual agreement with the Reclaimed Wastewater User is in accordance with the Operational Certificate. A copy of this Appendix is to be provided to each user prior to the commencement of irrigation <u>EACH YEAR</u>.

1 GENERAL REQUIREMENTS

1.1 Plans - New Works

- 1.1.1 Plans for modifications and/or extensions to the existing reclaimed wastewater irrigation system shall be approved by a person qualified in the design of irrigation systems.
- 1.1.2 Design and construct the irrigation works in accordance with best current agricultural practice and the "Pollution Control Guidelines for Municipal Effluent Application to Land", dated January 1983, and any amendments thereto, issued by the Ministry of Environment of British Columbia, and also in accordance with the "B.C. Sprinkler Irrigation Manual", dated 1989, prepared by the B.C. Ministry of Agriculture and Fisheries.

1.2 Construction Criteria

- 1.2.1 All reclaimed water user valves, shall be of a type or secured in a manner that permits operation by only personnel authorized by each wastewater user. All piping, valves and outlets should be marked to differentiate reclaimed wastewater from domestic water. All reclaimed wastewater controllers, valves, etc., shall be affixed with reclaimed wastewater warning signs.
- 1.2.2 Use or installation of hose-bibbs on any irrigation system presently operating, or designated to operate with reclaimed wastewater, regardless of the hose-bibb construction or identification, is not permitted.
- 1.2.3 There shall be at least a 3 metre horizontal and a 0.3 metre vertical separation (with domestic water pipeline above the reclaimed water pipeline) between all pipelines transporting reclaimed water and those transporting domestic water.

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1.2.4 There shall be no connection between a potable water supply, irrigation water or industrial well, and piping containing reclaimed wastewater, except through an air gap separation or reduced pressure principle device.

1.3 Fencing

The Reclaimed Wastewater User MAY be required by the Regional Waste Manager to erect a fence around the disposal area to restrict public access. The height and type of fencing shall meet the approval of the Regional Waste Manager.

1.4 Signage

- 1.4.1 Prominent "NO TRESPASSING", signs shall be erected around agricultural and silvicultural sites irrigated with reclaimed wastewater, warning persons of the possible health hazard during the irrigation season and advising that the water used for irrigation is NOT POTABLE. The wording shall be in language or symbols readily comprehensible by the general public. eg. "NO TRESPASSING - RECLAIMED WASTEWATER - DO NOT DRINK"
- 1.4.2 Warning signs shall be posted in sufficient numbers and size and at strategic locations to advise the public that reclaimed water is being used. Additional signage may be required as directed by the Regional Waste Manager.

2 <u>GENERAL REQUIREMENTS - RECLAIMED WASTEWATER IRRIGATION</u>

2.1 Buffer Zones

- 2.1.1 The requirement for formal buffer zones surrounding lands irrigated with reclaimed wastewater is no longer in effect, however, a buffer zone may be specified by the Regional Waste Manager.
- 2.1.2 Reclaimed wastewater applied by irrigation shall not be applied to the ground any closer than 15 metres from the edge of flowing streams or bodies of water.
- 2.1.3 There shall be no reclaimed wastewater irrigated within 30 metres of any well or inground reservoir for domestic supply.

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2.2 Surface Runoff

- 2.2.1 There shall be no surface runoff of irrigated reclaimed wastewater from the irrigated lands.
- 2.2.2 The maximum ground slope shall not exceed 20% without the written consent of the Regional Waste Manager.

2.3 Surfacing Reclaimed Wastewater

- 2.3.1 Irrigation shall be managed in such a fashion as to preclude surfacing of irrigation tail water down slope of the point of irrigation.
- 2.3.2 Irrigation shall be managed as to prevent ponding.

2.4 Spray Irrigation Drift

- 2.4.1 Reclaimed wastewater shall be confined to the area designated and approved for reclamation. The reclaimed wastewater irrigation system shall be managed in such a fashion as to prevent aerosol drift from leaving the irrigated lands.
- 2.4.2 Precautions shall be taken to ensure that reclaimed water will not have contact with any facility or area not designated for reclamation, such as passing vehicles, buildings, domestic water facilities, fruit and vegetable gardens, or food handling facilities.
- 2.4.3 Drinking water facilities shall be protected from direct or wind blown reclaimed wastewater spray.

2.5 Irrigation Rates

- 2.5.1 Irrigation rates shall not exceed the rates given in "B.C. Sprinkler Irrigation Manual", dated 1989, prepared by the B.C. Ministry of Agriculture and Fisheries.
- 2.5.2 Soils of the irrigated lands shall be monitored periodically or as otherwise directed by the Regional Waste Manager or the Town of Oliver, to prevent saturation, erosion, and instability.

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2.6 Agricultural Products Lag Time

- 2.6.1 A three day lag time is required before uninspected livestock intended for human consumption are permitted on areas irrigated with reclaimed wastewater. No lag time is required if livestock are subjected to the federal meat inspection program.
- 2.6.2 A six day lag time is required before dairy cattle are permitted in areas irrigated with reclaimed wastewater.
- 2.6.3 A three day lag time, after irrigation has ceased, is required before a crop intended for animal feed is harvested.

2.7 Insect and Vector Control

Adequate measures shall be taken to prevent the breeding of insects and other vectors of health significance, and the creation of odors, slimes or unsightly deposits.

2.8 Irrigation of Public Areas

- 2.8.1 Irrigation on golf courses or cemeteries shall only be practised when the public are not present.
- 2.8.2 Golf score cards shall indicate that reclaimed wastewater is used for irrigation on the golf course lands.

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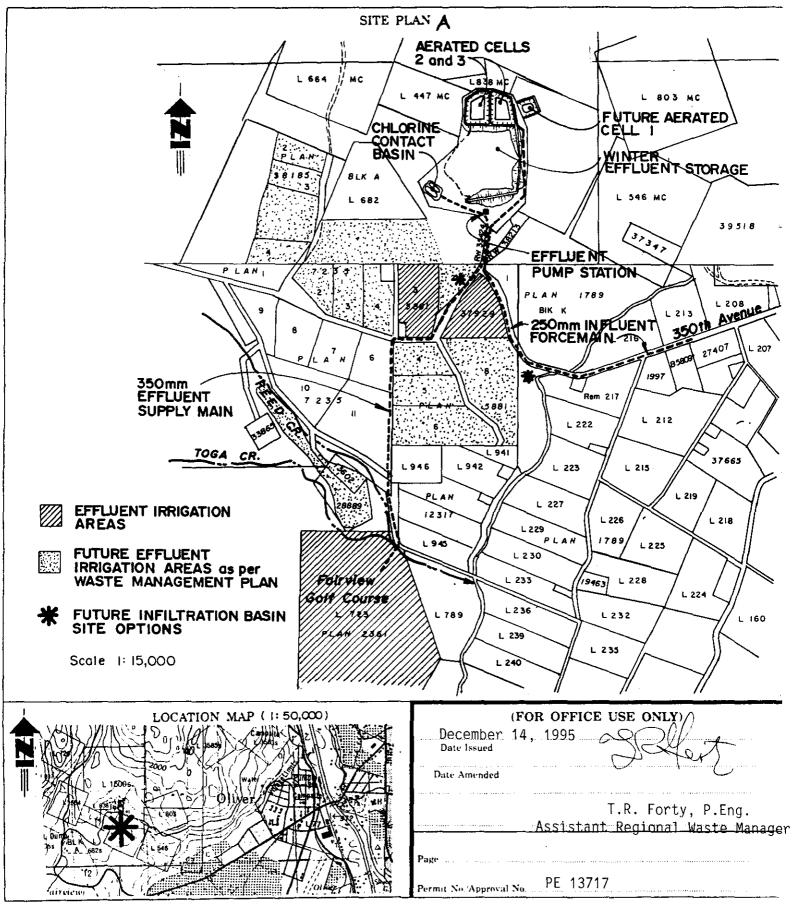
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Province of British Columbia

Ministry of Environment, Lands and Parks





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